

Introduction to Nuclear Fusion as An Energy Source



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Lecture 6

2024 spring semester

Wednesday 9:10-12:00

Materials:

<https://capst.ncku.edu.tw/PGS/index.php/teaching/>

Online courses:

<https://nckucc.webex.com/nckucc/j.php?MTID=ma76b50f97b1c6d72db61de9eaa9f0b27>

Note!



- **Midterm** **4/17 (One double-sided A4 cheating sheet is allowed.)**
- **Final exam** **6/12**

Course Outline



- **Magnetic confinement fusion (MCF)**
 - Gyro motion, MHD
 - 1D equilibrium (z pinch, theta pinch)
 - Drift: ExB drift, grad B drift, and curvature B drift
 - Tokamak, Stellarator (toroidal field, poloidal field)
 - Magnetic flux surface
 - 2D axisymmetric equilibrium of a torus plasma: Grad-Shafranov equation.
 - Stability (Kink instability, sausage instability, Safety factor Q)
 - Central-solenoid (CS) start-up (discharge) and current drive
 - CS-free current drive: electron cyclotron current drive, bootstrap current.
 - Auxiliary Heating: ECRH, Ohmic heating, Neutral beam injection.

Ideal MHD



- **Continuity eq:** $\frac{\partial \rho_m}{\partial t} + \nabla \cdot (\rho_m \vec{v}) = 0$
- **Momentum eq:** $\rho_m \left[\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla) \vec{v} \right] = \vec{j} \times \vec{B} - \nabla p$
- **Ohm's law:** $\vec{E} + \vec{v} \times \vec{B} \approx 0$
- **Equation of state:** $\frac{d}{dt} \left(\frac{P}{\rho_m^\gamma} \right) = 0$
- **Maxwell's eqs:**
 - $\nabla \cdot \vec{E} \approx 0$
 - $\nabla \cdot \vec{B} = 0$
 - $\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$
 - $\nabla \times \vec{B} = \mu_0 \vec{j}$
 - $\nabla \cdot \vec{j} = 0$
- **Requirement:**
 - High collisionality – fluid model
 - Small gyro radius – low frequency
 - Small resistivity – a perfect conductor

When forces are balanced, the system is in the equilibrium state, or called “Magnetohydrostatics”



- Equilibrium state:

$$\rho_m \left[\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla) \vec{v} \right] = \vec{j} \times \vec{B} - \nabla p \equiv 0$$

$$\vec{j} \times \vec{B} = \nabla p$$

$$\vec{j} \times \vec{B} = \frac{1}{\mu_0} (\nabla \times \vec{B}) \times \vec{B} = \frac{1}{\mu_0} \left[(\vec{B} \cdot \nabla) \vec{B} - \frac{1}{2} \nabla B^2 \right] = \nabla p$$

$$\nabla \times \vec{B} = \mu_0 \vec{j}$$

$$\nabla \left(p + \frac{B^2}{2\mu_0} \right) = \frac{1}{\mu_0} (\vec{B} \cdot \nabla) \vec{B}$$

Magnetic
pressure

Magnetic
tension

← Forces caused by
curvature of the field lines

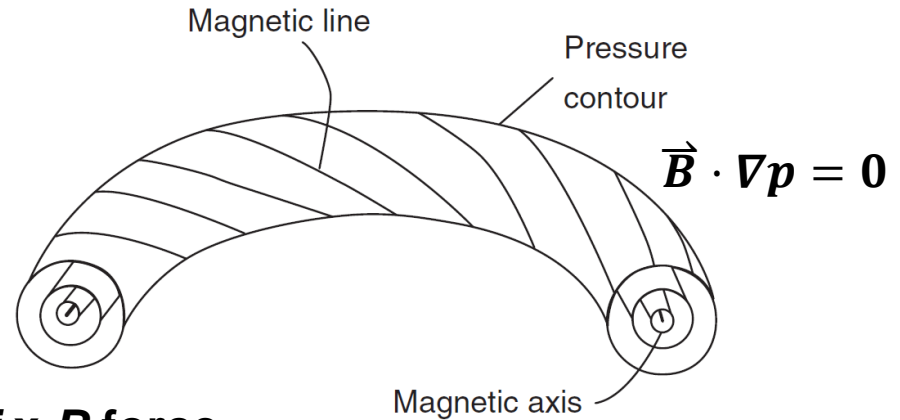
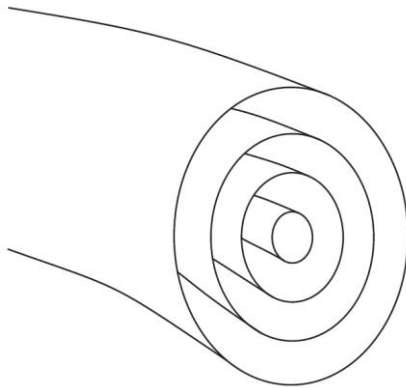
$$\vec{j} \perp \nabla p \quad \vec{B} \perp \nabla p \quad \Rightarrow \quad \vec{j} \cdot \nabla p = 0 \quad \vec{B} \cdot \nabla p = 0$$

- The surfaces with $p = \text{constant}$ are both magnetic surfaces (i.e., they are made up of magnetic field lines) and current surfaces (i.e., they are made of current flow lines).

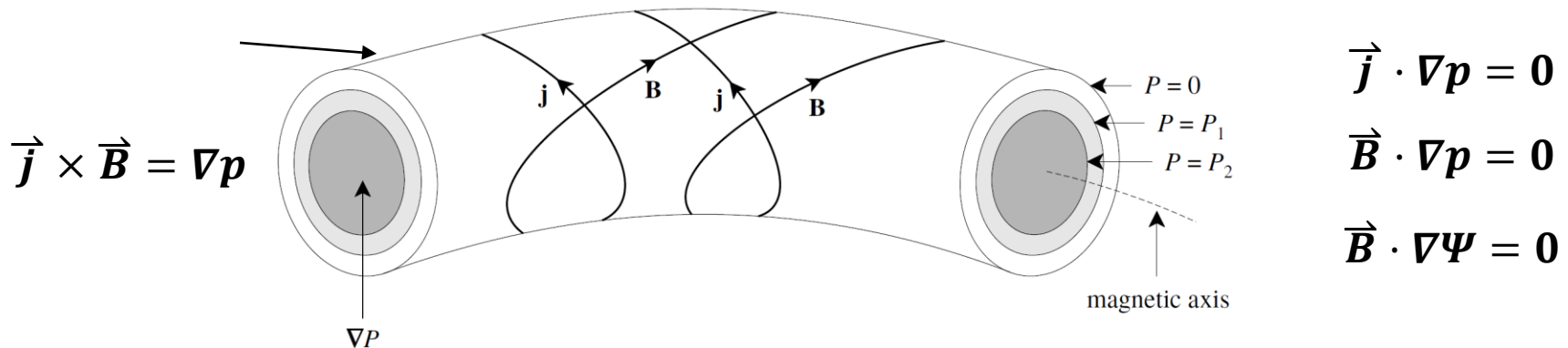
Magnetic lines lying on pressure contour



- Contours of constant pressure
- Magnetic lines lying on pressure contour

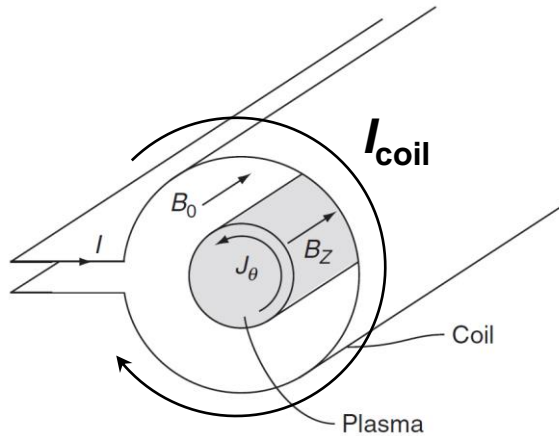


- Pressure gradient is balanced by the $j \times B$ force



- A magnetic (or flux) surface is one that is everywhere tangential to the field, i.e., the normal to the surface is everywhere perpendicular to B .

Theta pinch – current in the azimuthal direction



- **Symmetry:** $\partial_\theta = \partial_z = 0$
 $\vec{B} = B_z \hat{z}$
- **All quantities are only functions of the radius r .**

$$\nabla \cdot \vec{B} = 0$$

$$\frac{1}{r} \frac{\partial}{\partial r} (r B_r) + \frac{1}{r} \frac{\partial B_\theta}{\partial \theta} + \frac{\partial B_z}{\partial z} = 0$$

$$\frac{\partial B_z}{\partial z} = 0$$

$$\nabla \times \vec{B} = \mu_0 \vec{j}$$

$$(\nabla \times \vec{B})_r = \frac{1}{r} \frac{\partial B_z}{\partial \theta} - \frac{\partial B_\theta}{\partial z} = 0$$

$$(\nabla \times \vec{B})_\theta = \frac{\partial B_r}{\partial z} - \frac{\partial B_z}{\partial r} = -\frac{\partial B_z}{\partial r}$$

$$(\nabla \times \vec{B})_z = \frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) - \frac{1}{r} \frac{\partial B_r}{\partial \theta} = 0$$

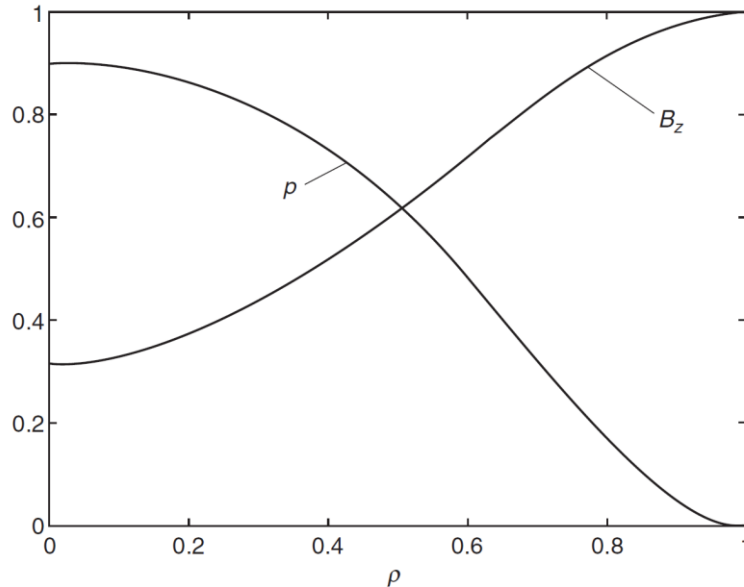
$$j_\theta = -\frac{1}{\mu_0} \frac{\partial B_z}{\partial r}$$

$$\nabla \left(P + \frac{B^2}{2\mu_0} \right) = \frac{1}{\mu_0} (\vec{B} \cdot \nabla) \vec{B} = 0$$

$$P + \frac{B_z^2}{2\mu_0} = \frac{B_0^2}{2\mu_0}$$

$$\vec{j} \times \vec{B} = \nabla p \quad j_\theta B_z = \frac{dp}{dr}$$

Theta pinch is an excellent option for producing radial pressure balance in a fusion plasma



$$\frac{2\mu_0 p(r)}{B_0^2} = 1 - \left[1 - \hat{\beta}(1 - \rho^2)\right]^2$$

$$\frac{B_z(r)}{B_0} = 1 - \hat{\beta}(1 - \rho^2)$$

$$\frac{a\mu_0 j_\theta(r)}{B_0} = -4\hat{\beta}\rho(1 - \rho^2)$$

$$\hat{\beta} = \frac{\beta_0}{1 + \sqrt{1 - \beta_0}} \quad \beta_0 = \frac{2\mu_0 p_0}{B_0^2} \quad \rho = \frac{r}{a}$$

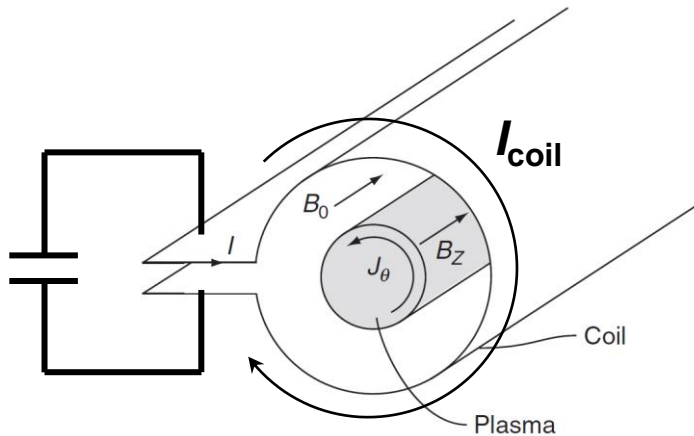
$$\beta \equiv \beta_t = \frac{2\mu_0 \langle p \rangle}{B_0^2} = \frac{4\mu_0}{a^2 B_0^2} \int_0^a p r dr = 2 \int_0^1 \left(1 - \frac{B_z^2}{B_0^2}\right) \rho d\rho = \hat{\beta} \left(\frac{2}{3} - \frac{\hat{\beta}}{5}\right)$$

$$\beta_0 \rightarrow 0 \Rightarrow \hat{\beta} \approx \frac{\beta_0}{2}, \beta \approx \frac{\beta_0}{3}$$

$$\beta_0 \rightarrow 1 \Rightarrow \hat{\beta} \rightarrow 1, \beta \approx \frac{7}{15}$$

$$0 < \beta < 1$$

Theta pinches provide good radial confinement but NOT axially



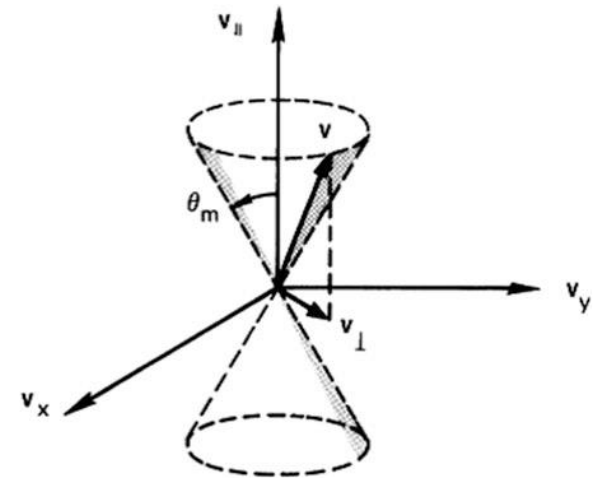
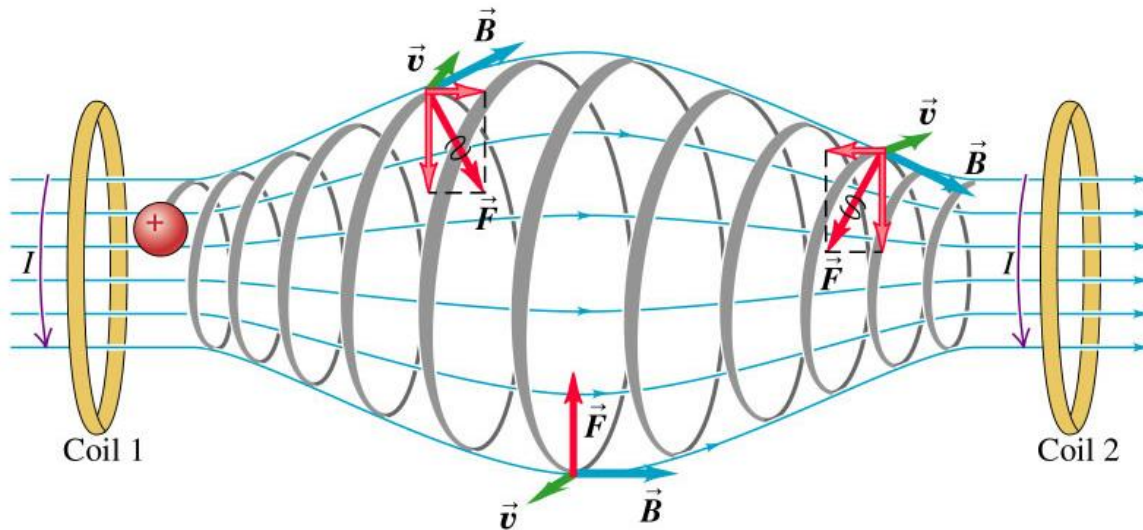
- The gas is initially preionized.
- The coil current is provided by a capacitor bank. The typical pulse length is 10-50 μs .
- The rapidly rising magnetic field acts like a piston, imparting a large impulse of momentum and energy to the particles as they are reflected.
- This energy is ultimately converted to heat after repeated reflections off the converging piston.
- $T_i \sim 1\text{-}4 \text{ keV}$, $n \sim 1\text{-}2 \times 10^{22} \text{ m}^{-3}$, $\beta_0 \sim 0.7\text{-}0.9$, $\beta \sim 0.05$.
- The plasma simply flowed out the end of the device along field lines in a characteristic time $\tau = L/V_{Ti} \sim 10 \mu\text{s}$ for $L = 5 \text{ m}$.

Main issue: end loss.

Charged particles can be partially confined by a magnetic mirror machine



- Charged particles with small v_{\parallel} eventually stop and are reflected while those with large v_{\parallel} escape.



$$\frac{1}{2}mv^2 = \frac{1}{2}mv_{\parallel}^2 + \frac{1}{2}mv_{\perp}^2 \quad \text{Invariant: } \mu \equiv \frac{1}{2} \frac{mv_{\perp}^2}{B}$$

$$v'_{\perp}{}^2 = v_{\perp 0}{}^2 + v_{\parallel 0}{}^2 \equiv v_0^2$$

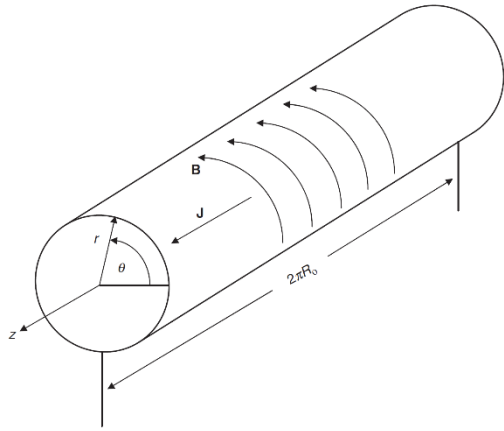
$$\frac{B_0}{B'} = \frac{v_{\perp 0}{}^2}{v'_{\perp}{}^2} = \frac{v_{\perp 0}{}^2}{v_0^2} \equiv \sin^2 \theta$$

$$\frac{B_0}{B_m} \equiv \frac{1}{R_m} = \sin^2 \theta_m$$

- Large v_{\parallel} may occur from collisions between particles.

Those confined charged particle are eventually lost due to collisions.

Z pinch – current in the axial direction. The radial confinement of the plasma is provided by the tension force



- **Symmetry:** $\partial_\theta = \partial_z = 0$
 $\vec{B} = B_\theta \hat{\theta}$
- **All quantities are only functions of the radius r .**

$$\nabla \cdot \vec{B} = 0$$

$$\frac{1}{r} \frac{\partial}{\partial r} (r B_r) + \frac{1}{r} \frac{\partial B_\theta}{\partial \theta} + \frac{\partial B_z}{\partial z} = 0$$

$$\frac{1}{r} \frac{\partial B_\theta}{\partial \theta} = 0$$

$$\nabla \times \vec{B} = \mu_0 \vec{j}$$

$$(\nabla \times \vec{B})_r = \frac{1}{r} \frac{\partial B_z}{\partial \theta} - \frac{\partial B_\theta}{\partial z} = 0$$

$$(\nabla \times \vec{B})_\theta = \frac{\partial B_r}{\partial z} - \frac{\partial B_z}{\partial r} = 0$$

$$(\nabla \times \vec{B})_z = \frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) - \frac{1}{r} \frac{\partial B_r}{\partial \theta} = \frac{1}{r} \frac{\partial}{\partial r} (r B_\theta)$$

$$j_z = \frac{1}{\mu_0 r} \frac{\partial}{\partial r} (r B_\theta)$$

$$\vec{j} \times \vec{B} = \nabla p \quad j_z B_\theta = - \frac{dp}{dr}$$

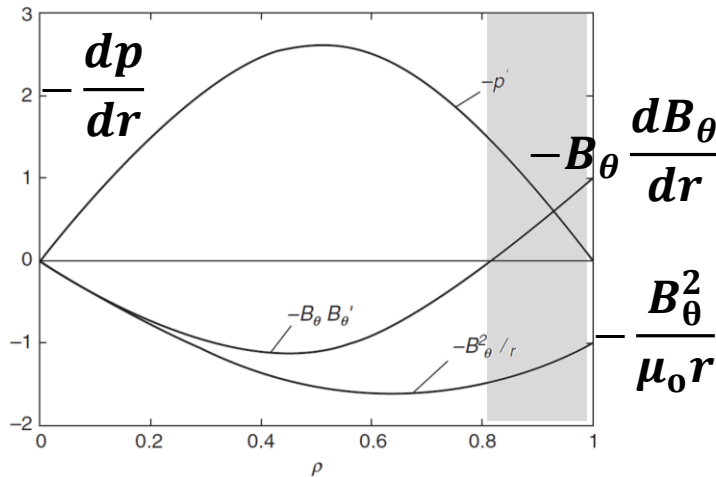
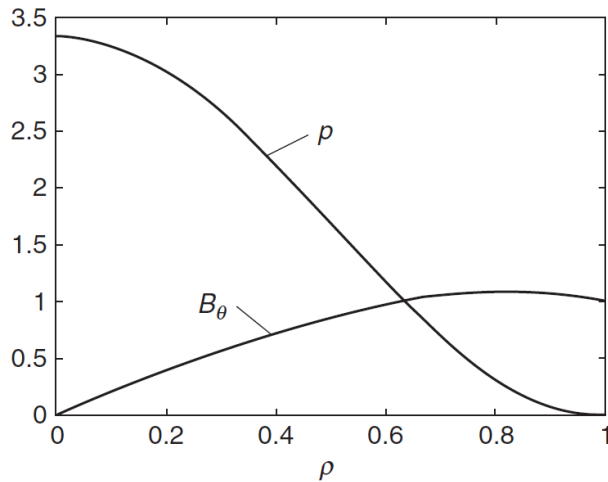
$$\frac{dp}{dr} + \frac{B_\theta}{\mu_0 r} \frac{\partial}{\partial r} (r B_\theta) = 0$$

$$\frac{d}{dr} \left(p + \frac{B_\theta^2}{2\mu_0} \right) + \frac{B_\theta^2}{\mu_0 r} = 0$$

Magnetic pressure

Magnetic tension

Z pinch – there is no flexibility in achieving small to moderate β



$$\frac{d}{dr} \left(p + \frac{B_{\theta}^2}{2\mu_0} \right) + \frac{B_{\theta}^2}{\mu_0 r} = 0$$

$$\frac{2\mu_0 p(r)}{B_{\theta a}^2} = \frac{2}{3} (5 - 2\rho^2)(1 - \rho^2)^2$$

$$\frac{B_{\theta}(r)}{B_{\theta a}} = 2\rho \left(1 - \frac{\rho^2}{2} \right)$$

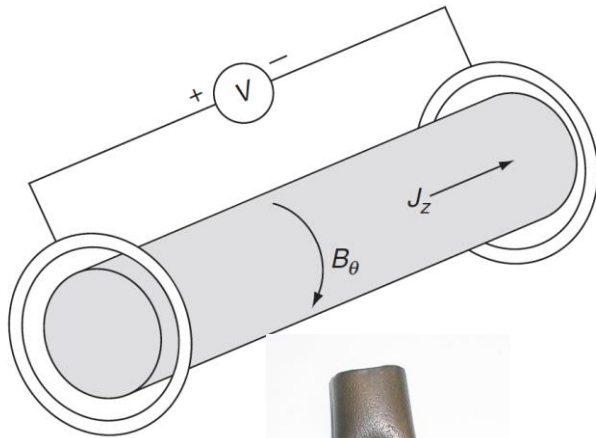
$$\frac{a\mu_0 j_z(r)}{B_{\theta a}} = 4(1 - \rho^2)$$

$$B_{\theta a} \equiv B_{\theta}(a) = \frac{\mu_0 I}{2\pi a}$$

$$\beta \equiv \beta_p = \frac{2\mu_0 \langle p \rangle}{B_{\theta a}^2} = \frac{4\mu_0}{a^2 B_{\theta a}^2} \int_0^a p r dr = 1$$

Bennett pinch relation: $\beta = 1$

Huge instabilities occur in a z pinch

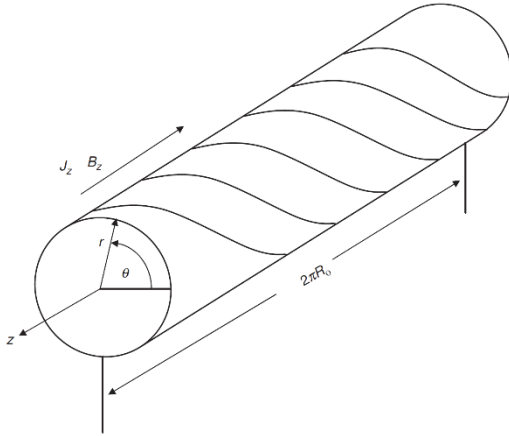


- A capacitor bank is discharged across two electrodes located at each end of a cylindrical quartz or Pyrex tube.
- The gas is ionized by the high voltage and produces a z current flowing along the plasma.
- Disastrous instabilities occurs often leading to a complete quenching of the plasma after 1-2 us.



Main issue: unstable.

General screw pinch – linear superposition of the theta pinch and the z pinch



- Nonzero field: $\vec{B} = B_\theta \hat{\theta} + B_z \hat{z}$

$$\vec{j} = j_\theta \hat{\theta} + j_z \hat{z}$$

$$\nabla \cdot \vec{B} = 0$$

$$\frac{1}{r} \frac{\partial}{\partial r} (r B_r) + \frac{1}{r} \frac{\partial B_\theta}{\partial \theta} + \frac{\partial B_z}{\partial z} = 0$$

$$\frac{1}{r} \frac{\partial B_\theta}{\partial \theta} + \frac{\partial B_z}{\partial z} = 0$$

$$\nabla \times \vec{B} = \mu_0 \vec{j}$$

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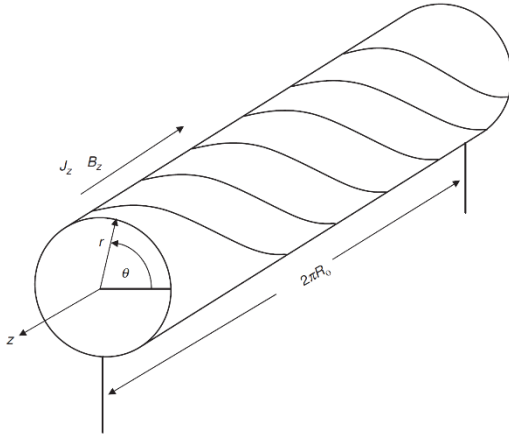
$$j_\theta = -\frac{1}{\mu_0} \frac{\partial B_z}{\partial r} \quad j_z = \frac{1}{\mu_0 r} \frac{\partial}{\partial r} (r B_\theta)$$

$$\vec{j} \times \vec{B} = \nabla p \quad j_\theta B_z - j_z B_\theta = -\frac{dp}{dr}$$

$$-\frac{B_z}{\mu_0} \frac{\partial B_z}{\partial r} - \frac{B_\theta}{\mu_0 r} \frac{\partial}{\partial r} (r B_\theta) = -\frac{dp}{dr}$$

$$\frac{d}{dr} \left(p + \frac{B_\theta^2 + B_z^2}{2\mu_0} \right) + \frac{B_\theta^2}{\mu_0 r} = 0$$

General screw pinch – linear superposition of the theta pinch and the z pinch



- Nonzero field: $\vec{B} = B_\theta \hat{\theta} + B_z \hat{z}$

$$\vec{j} = j_\theta \hat{\theta} + j_z \hat{z}$$

$$\nabla \cdot \vec{B} = 0$$

$$\frac{1}{r} \frac{\partial}{\partial r} (r B_r) + \frac{1}{r} \frac{\partial B_\theta}{\partial \theta} + \frac{\partial B_z}{\partial z} = 0$$

$$\frac{1}{r} \frac{\partial B_\theta}{\partial \theta} + \frac{\partial B_z}{\partial z} = 0$$

$$\nabla \times \vec{B} = \mu_0 \vec{j}$$

$$(\nabla \times \vec{B})_r = \frac{1}{r} \frac{\partial B_z}{\partial \theta} - \frac{\partial B_\theta}{\partial z} = 0$$

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$$(\nabla \times \vec{B})_z = \frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) - \frac{1}{r} \frac{\partial B_r}{\partial \theta} = \frac{1}{r} \frac{\partial}{\partial r} (r B_\theta)$$

$$j_\theta = -\frac{1}{\mu_0} \frac{\partial B_z}{\partial r} \quad j_z = \frac{1}{\mu_0 r} \frac{\partial}{\partial r} (r B_\theta)$$

$$\vec{j} \times \vec{B} = \nabla p \quad j_\theta B_z - j_z B_\theta = -\frac{dp}{dr}$$

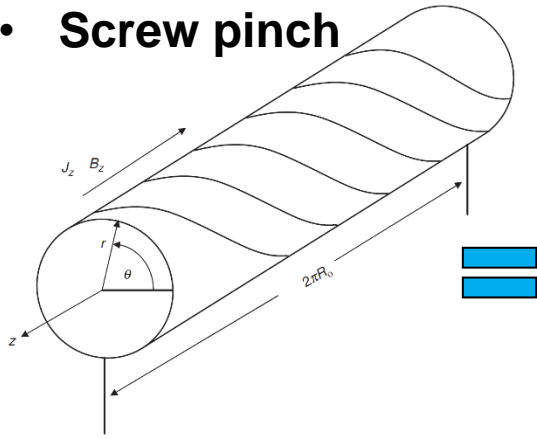
$$-\frac{B_z}{\mu_0} \frac{\partial B_z}{\partial r} - \frac{B_\theta}{\mu_0 r} \frac{\partial}{\partial r} (r B_\theta) = -\frac{dp}{dr}$$

$$\frac{d}{dr} \left(p + \frac{B_\theta^2 + B_z^2}{2\mu_0} \right) + \frac{B_\theta^2}{\mu_0 r} = 0$$

General screw pinch is flexible with varies range of β



• Screw pinch

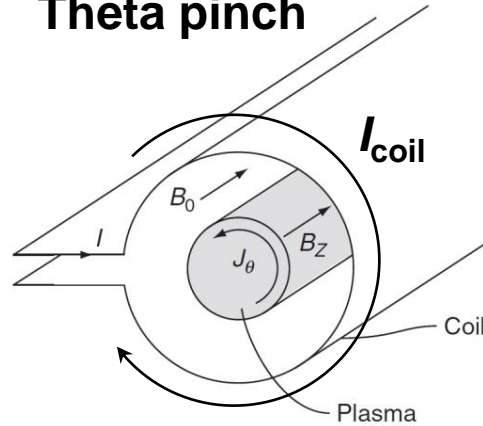


$$\vec{B} = B_\theta \hat{\theta} + B_z \hat{z}$$

$$\vec{j} = j_\theta \hat{\theta} + j_z \hat{z}$$

$$\frac{d}{dr} \left(p + \frac{B_\theta^2 + B_z^2}{2\mu_0} \right) + \frac{B_\theta^2}{\mu_0 r} = 0$$

• Theta pinch

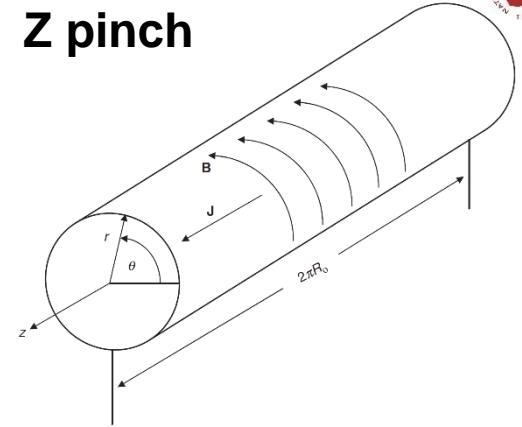


$$\vec{B} = B_z \hat{z}$$

$$\vec{j} = j_\theta \hat{\theta}$$

$$p + \frac{B_z^2}{2\mu_0} = \frac{B_0^2}{2\mu_0}$$

• Z pinch



$$\vec{B} = B_\theta \hat{\theta}$$

$$\vec{j} = j_z \hat{z}$$

$$\frac{d}{dr} \left(p + \frac{B_\theta^2}{2\mu_0} \right) + \frac{B_\theta^2}{\mu_0 r} = 0$$

$$\int_0^a \pi r^2 dr \left[\frac{d}{dr} \left(p + \frac{B_\theta^2 + B_z^2}{2\mu_0} \right) + \frac{B_\theta^2}{\mu_0 r} \right] = 0$$

$$\langle p \rangle = \frac{B_{\theta a}^2}{2\mu_0} + \frac{1}{2\mu_0} (B_0^2 - \langle B_z^2 \rangle)$$

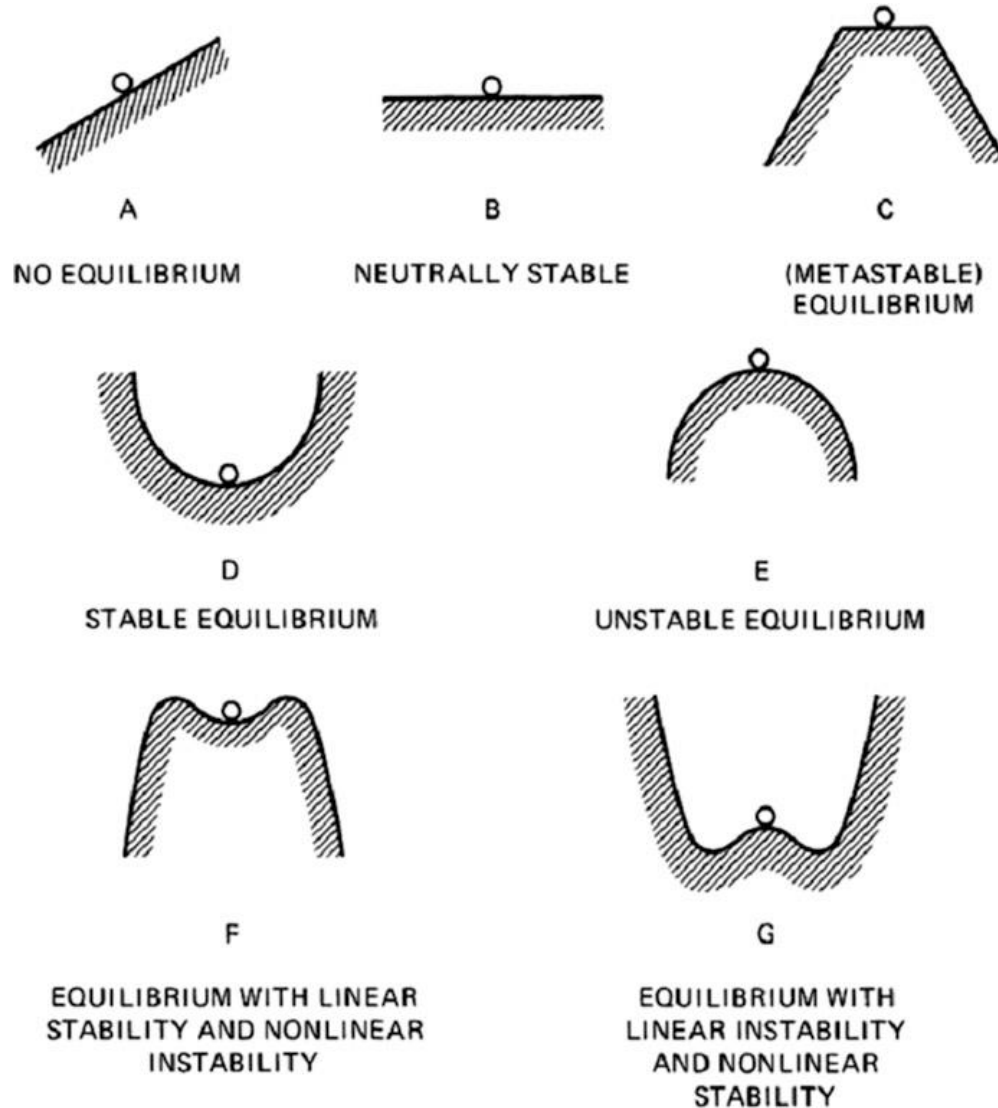
$$\beta_t = \frac{2\mu_0 \langle p \rangle}{B_0^2}$$

$$\beta_p = \frac{2\mu_0 \langle p \rangle}{B_{\theta a}^2}$$

$$\beta = \frac{\beta_t \beta_p}{\beta_t + \beta_p} = \frac{2\mu_0 \langle p \rangle}{B_0^2 + B_{\theta a}^2}$$

$$0 \leq \langle \beta \rangle \leq 1$$

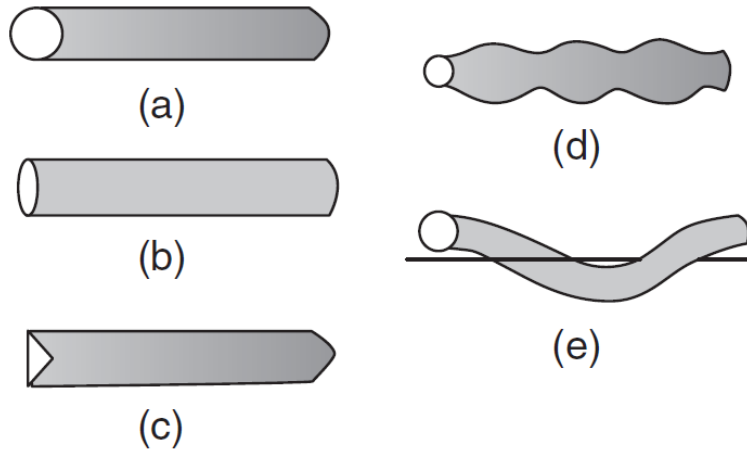
An equilibrium state may not be stable



A cylindrical plasma column may not be stable

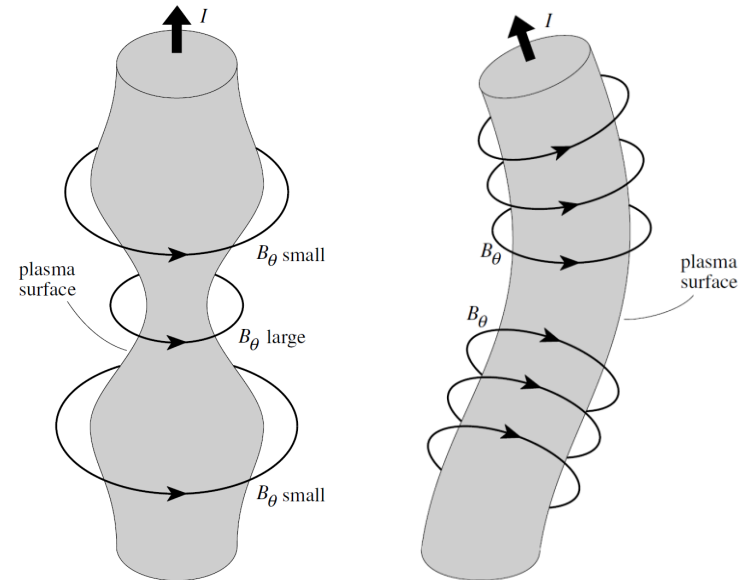


- Instabilities of theta pinch



- (a) Unperturbed
- (b) $m=2, k=0$
- (c) $m=3, k=0$
- (d) $m=0, k \neq 0$
- (e) $m=1, k \neq 0$

- Instabilities of z pinch



**Sausage
instability
($m=0$)**

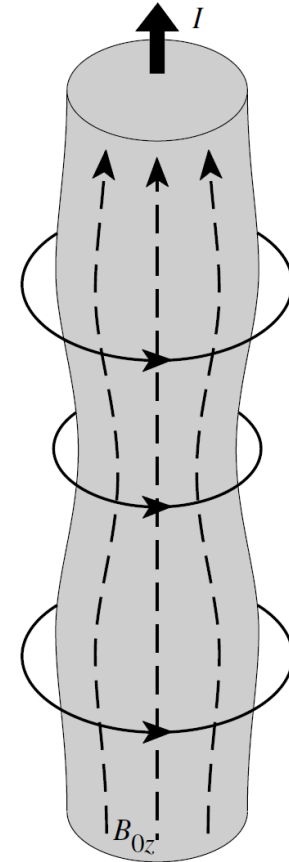
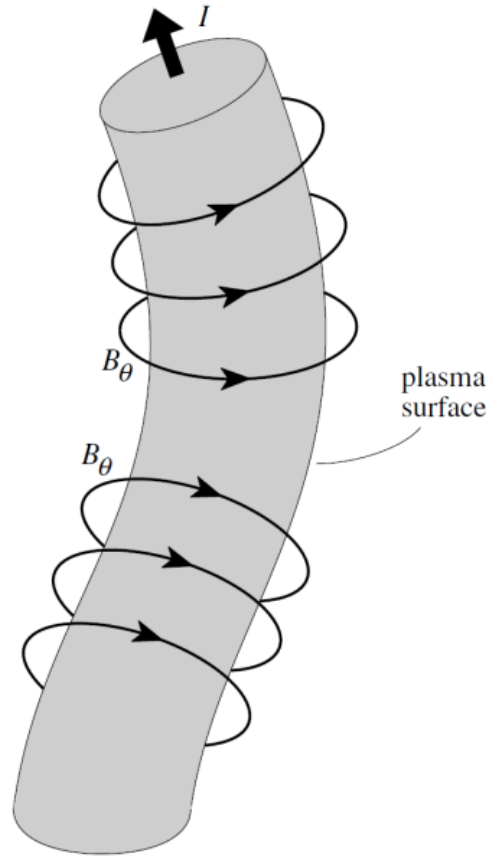
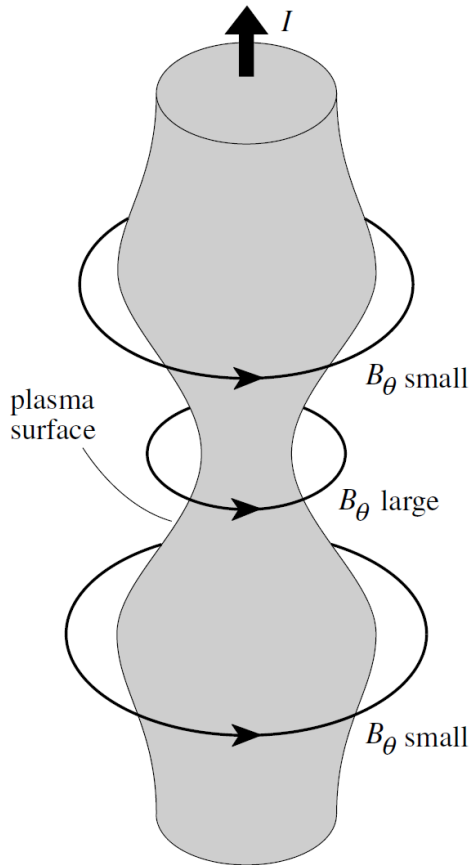
**Kink
instability
($m=1$)**

$$\zeta(\vec{r}) = \zeta(r) \exp(im\theta + ikz)$$

A cylindrical plasma column is stable when the safety factor is greater than unity



- Sausage instability ($m=0$)
- Kink instability

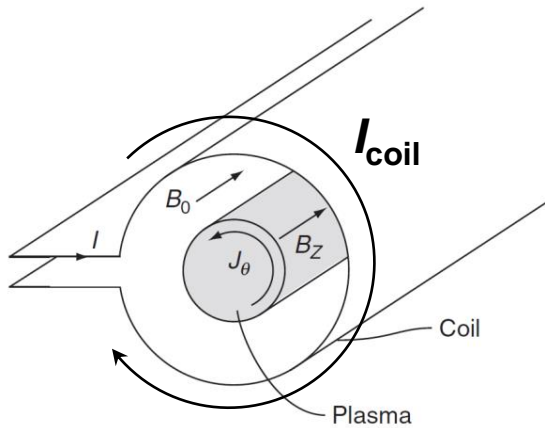


- MHD Safety factor: $q(r) = \frac{rB_z(r)}{R_0B_\theta(r)}$ Kruskal–Shafranov limit

Theta pinch is stable while z pinch is unstable



- **Theta pinch**

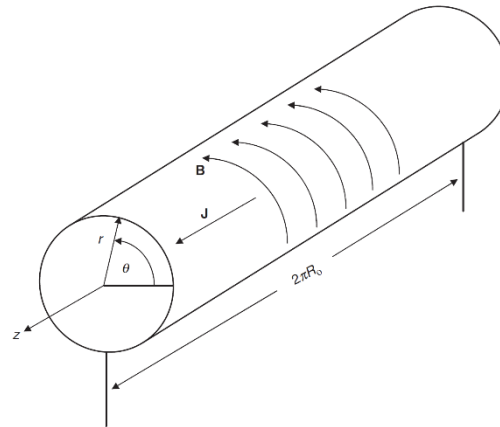


$$\vec{B} = B_z \hat{z}$$

$$q_\theta = \infty$$

Stable

- **Z pinch**



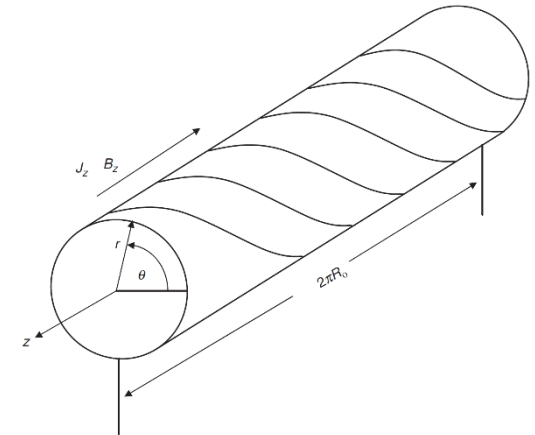
$$\vec{B} = B_\theta \hat{\theta}$$

$$q_z = 0$$

Unstable

$$q(r) = \frac{r B_z(r)}{R_0 B_\theta(r)}$$

- **Screw pinch**



$$\vec{B} = B_\theta \hat{\theta} + B_z \hat{z}$$

$$\vec{j} = j_\theta \hat{\theta} + j_z \hat{z}$$

q can be controlled.

Stable/Unstable

Course Outline

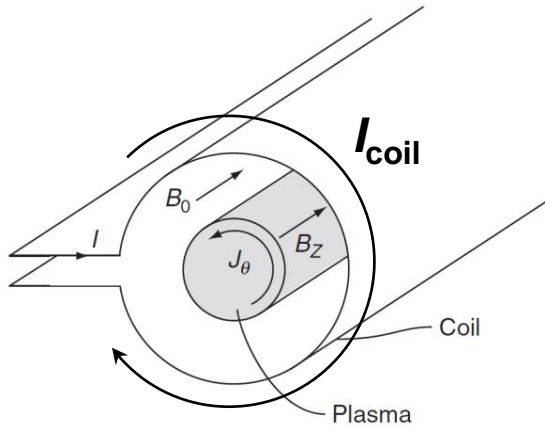


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Theta pinch is stable while z pinch is unstable



- **Theta pinch**

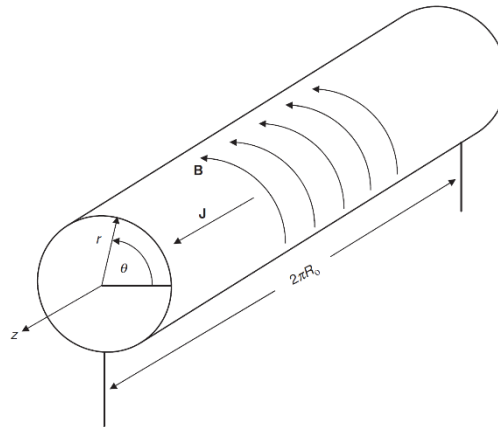


$$\vec{B} = B_z \hat{z}$$

$$q_\theta = \infty$$

Stable

- **Z pinch**



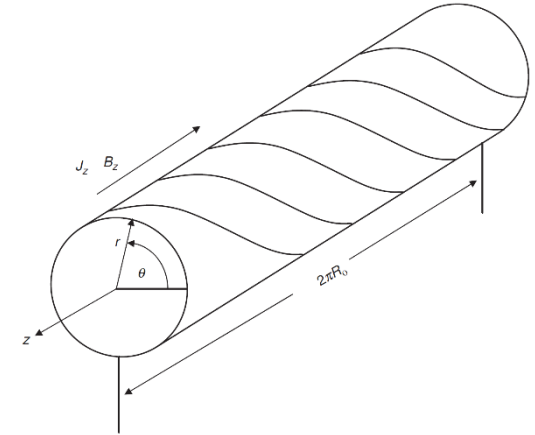
$$\vec{B} = B_\theta \hat{\theta}$$

$$q_z = 0$$

Unstable

$$q(r) = \frac{r B_z(r)}{R_0 B_\theta(r)}$$

- **Screw pinch**



$$\vec{B} = B_\theta \hat{\theta} + B_z \hat{z}$$

$$\vec{j} = j_\theta \hat{\theta} + j_z \hat{z}$$

q can be controlled.

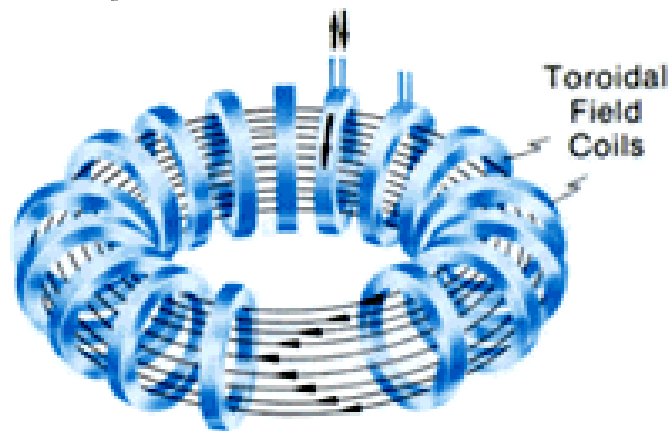
Stable/Unstable

Plasma can be confined in a doughnut-shaped chamber with toroidal magnetic field



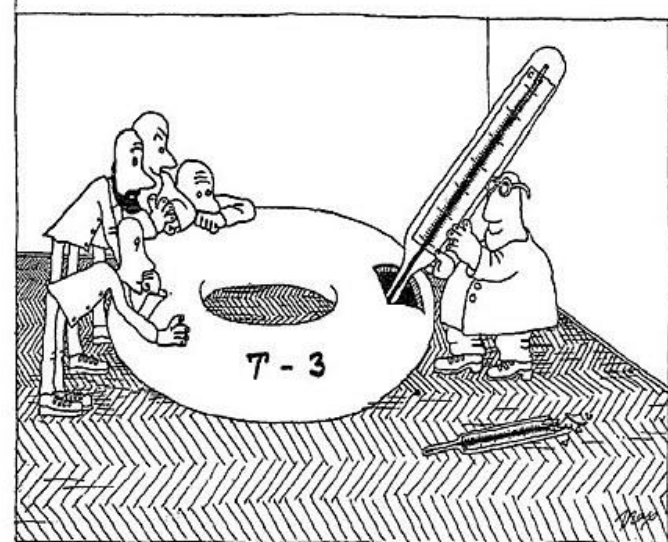
- Tokamak - "toroidal chamber with magnetic coils" (тороидальная камера с магнитными катушками)

Relatively Constant Electric Current



Nature

Constant Toroidal Field



Measurement of the Electron Temperature by Thomson Scattering in Tokamak T3

by

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M. J. FORREST
P. D. WILCOCK
UKAEA Research Group,
Culham Laboratory,
Abingdon, Berkshire

V. V. SANNIKOV
I. V. Kurchatov Institute,
Moscow

$$T_e = 100 \sim 1 \text{ keV}$$

$$n_e = 1\text{-}3 \times 10^{13} \text{ cm}^{-3}$$

Electron temperatures of 100 eV up to 1 keV and densities in the range $1\text{-}3 \times 10^{13} \text{ cm}^{-3}$ have been measured by Thomson scattering on Tokamak T3. These results agree with those obtained by other techniques where direct comparison has been possible.

<https://www.iter.org/mach/tokamak>

https://en.wikipedia.org/wiki/Tokamak#cite_ref-4

Drawing from the talk "Evolution of the Tokamak" given in 1988 by B.B. Kadomtsev at Culham.

N. J. Peacock, et al., Nature **224**, 488 (1969)

Quick summary of different drifts



- ExB drift: $\vec{v}_E = \frac{\vec{E} \times \vec{B}}{B^2}$

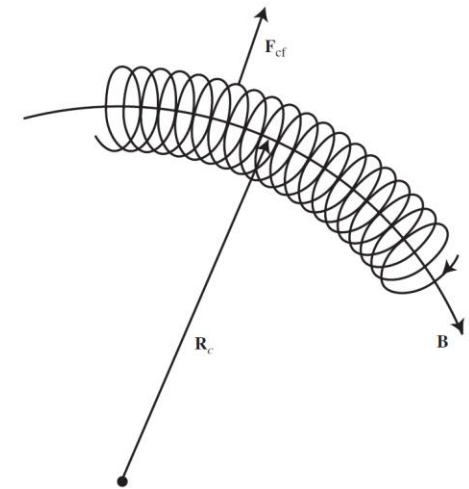
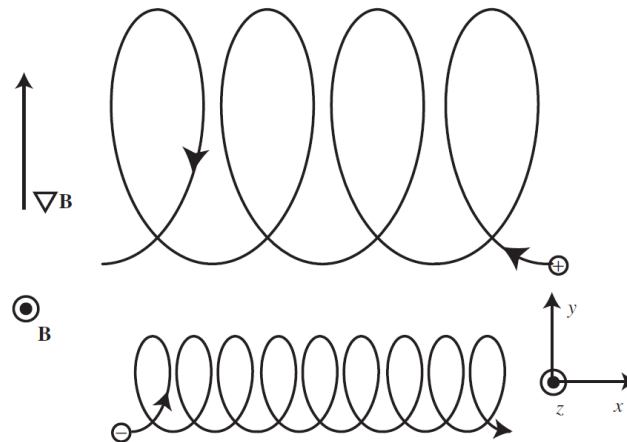
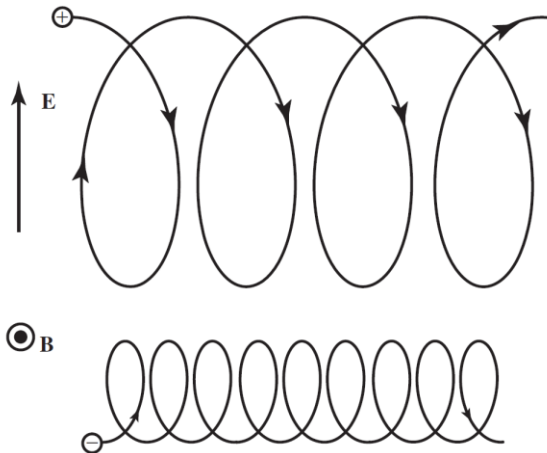
Independent to charge

- Grad-B drift: $\vec{v}_\nabla = \frac{mv_\perp^2}{2q} \frac{\vec{B} \times \nabla B}{B^3}$

Depended on charge

- Curvature drift: $\vec{v}_R = \frac{mv_{||}^2}{q} \frac{\vec{R}_c \times \vec{B}}{R_c^2 B^2}$

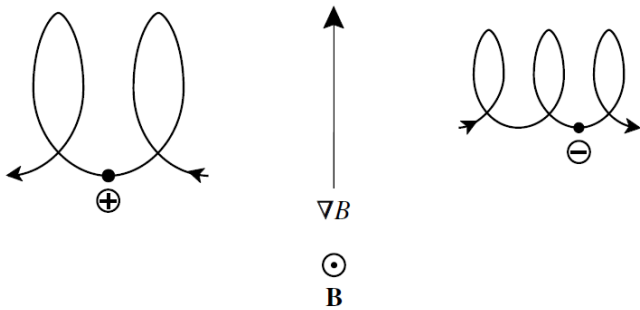
Depended on charge



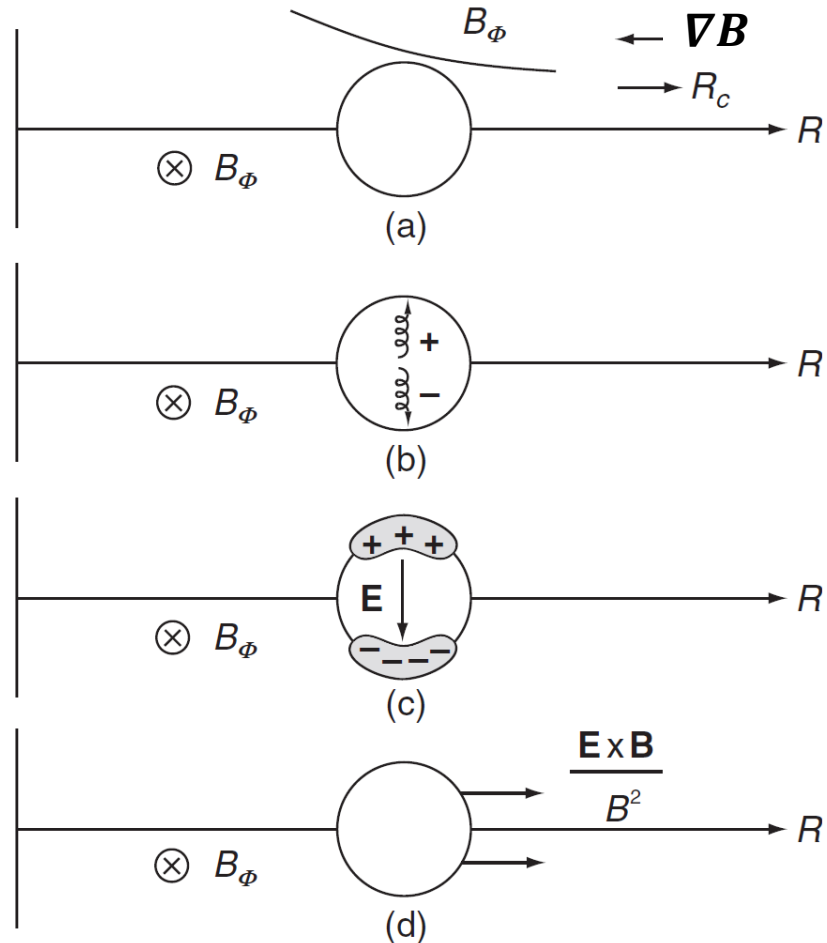
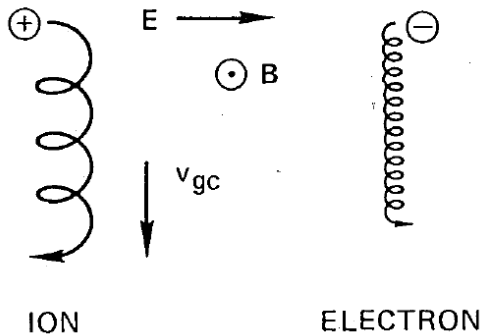
Charged particles drift across field lines



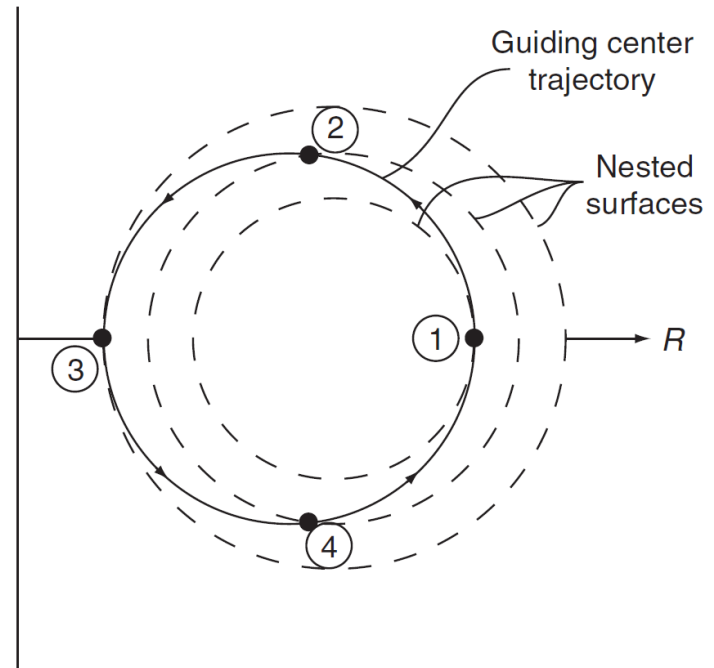
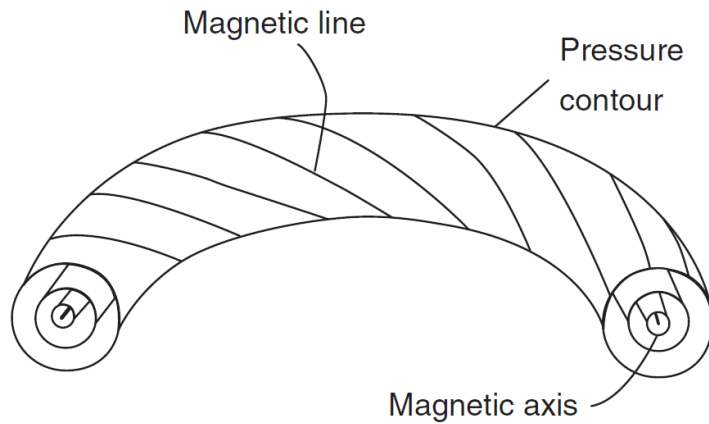
- Grad-B drift**



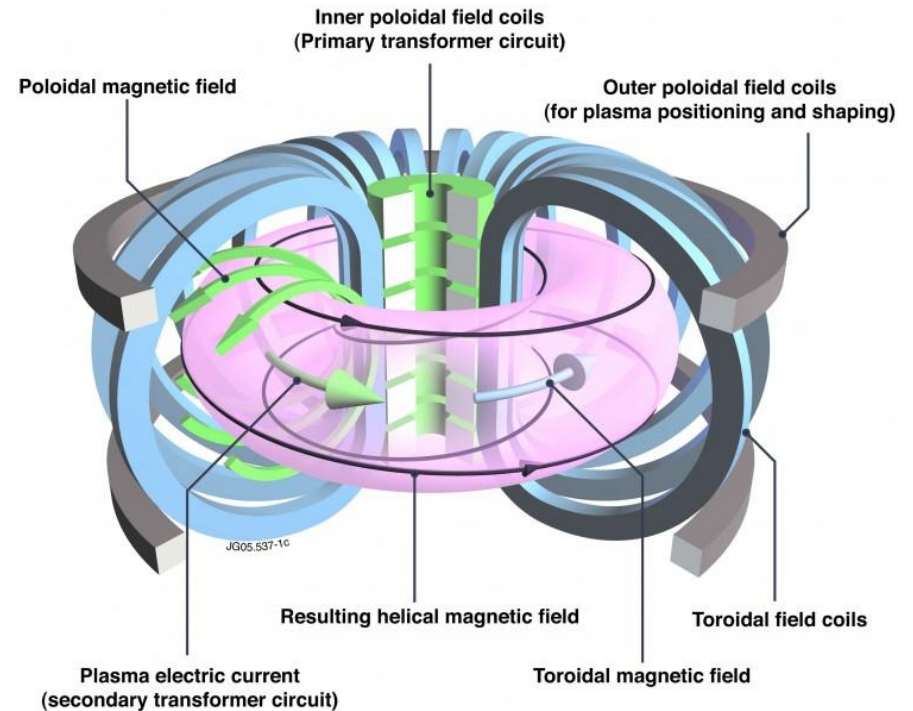
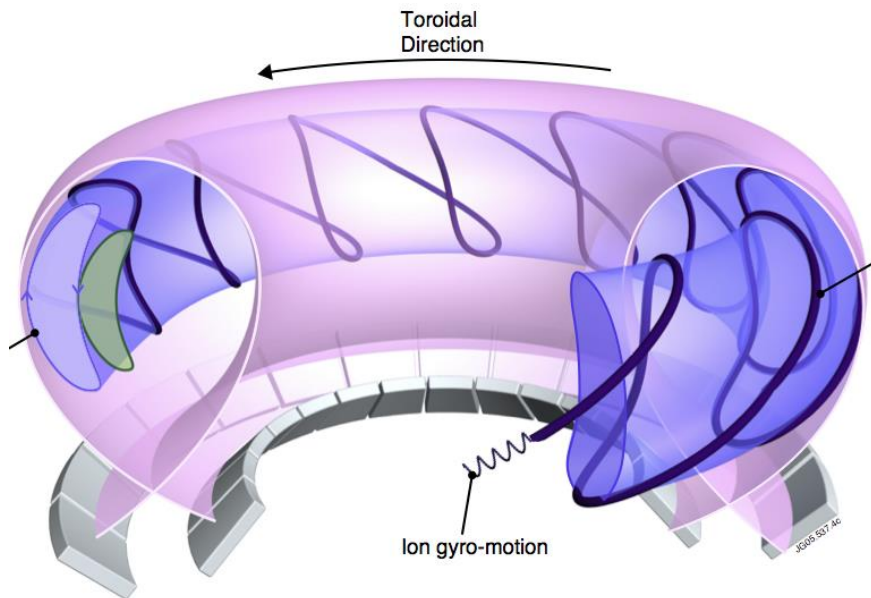
- ExB drift**



The particle drifts back to the original position if a small poloidal field is superimposed on the toroidal field



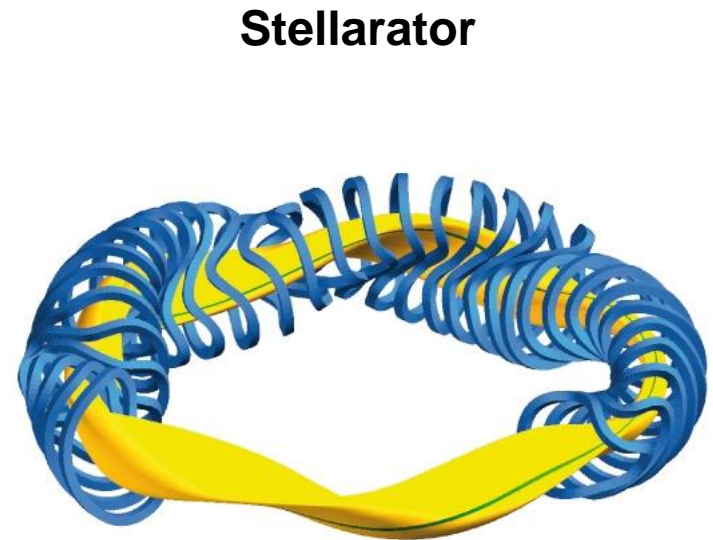
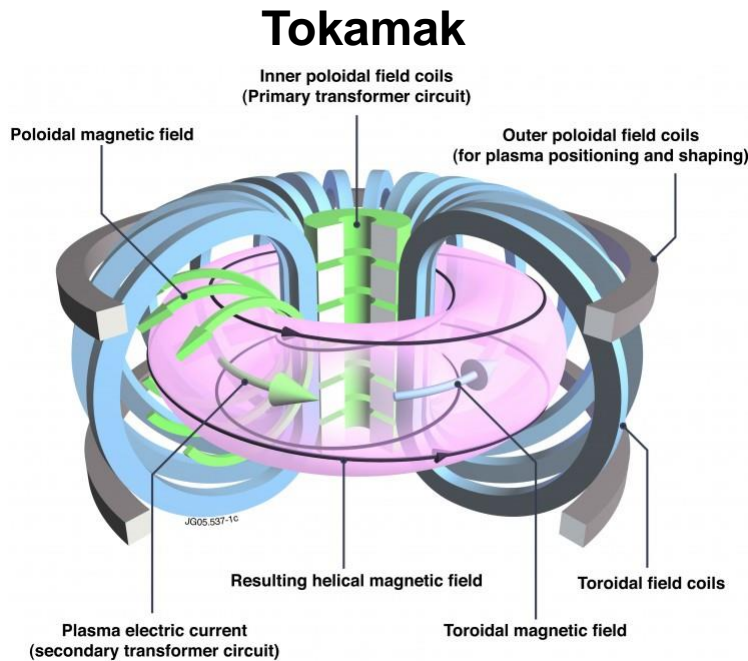
A poloidal magnetic field is required to reduce the drift across field lines



A poloidal magnetic field is required to reduce the drift across field lines



Stellarator uses twisted coil to generate poloidal magnetic field

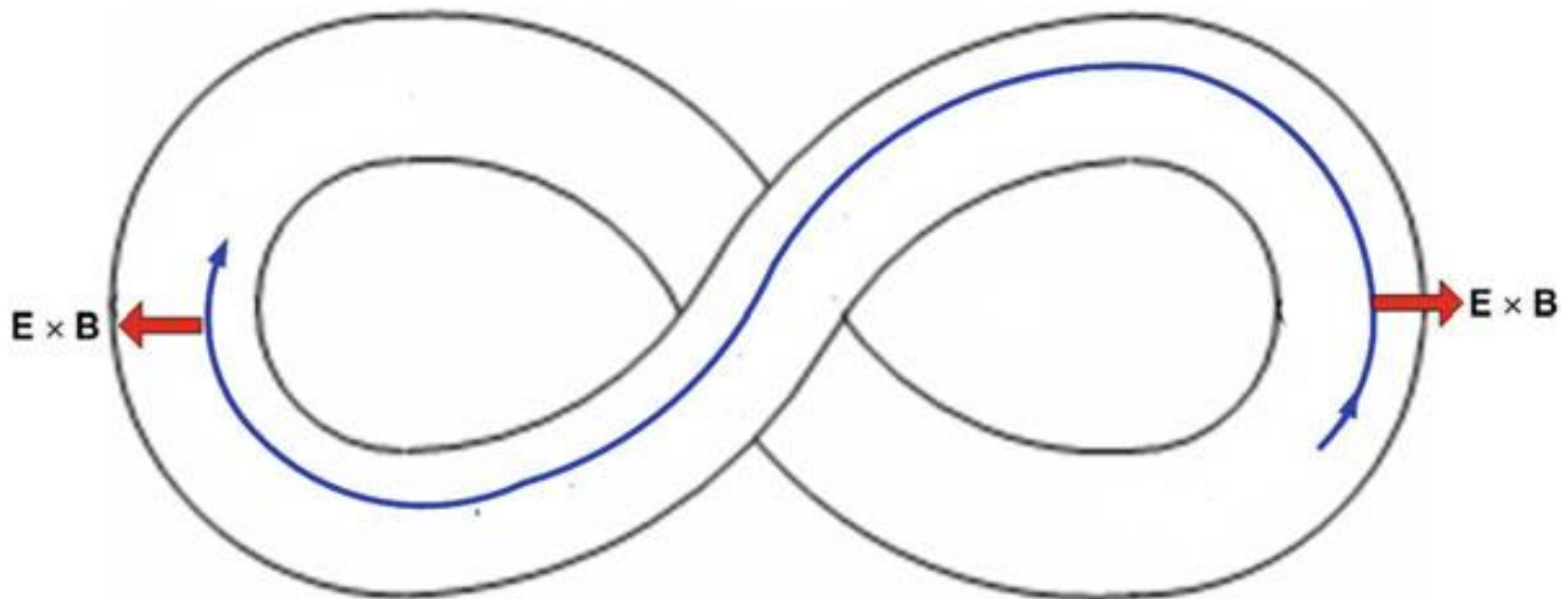


Stellarator



- **Figure eight shape**
- **Oval shape (racetrack)**
- **Torsatron**
- **Heliotron**
- **Heliac (Helical Axis stellarator)**
- **Helias (W7-x)**

A figure-8 stellarator solved the drift issues



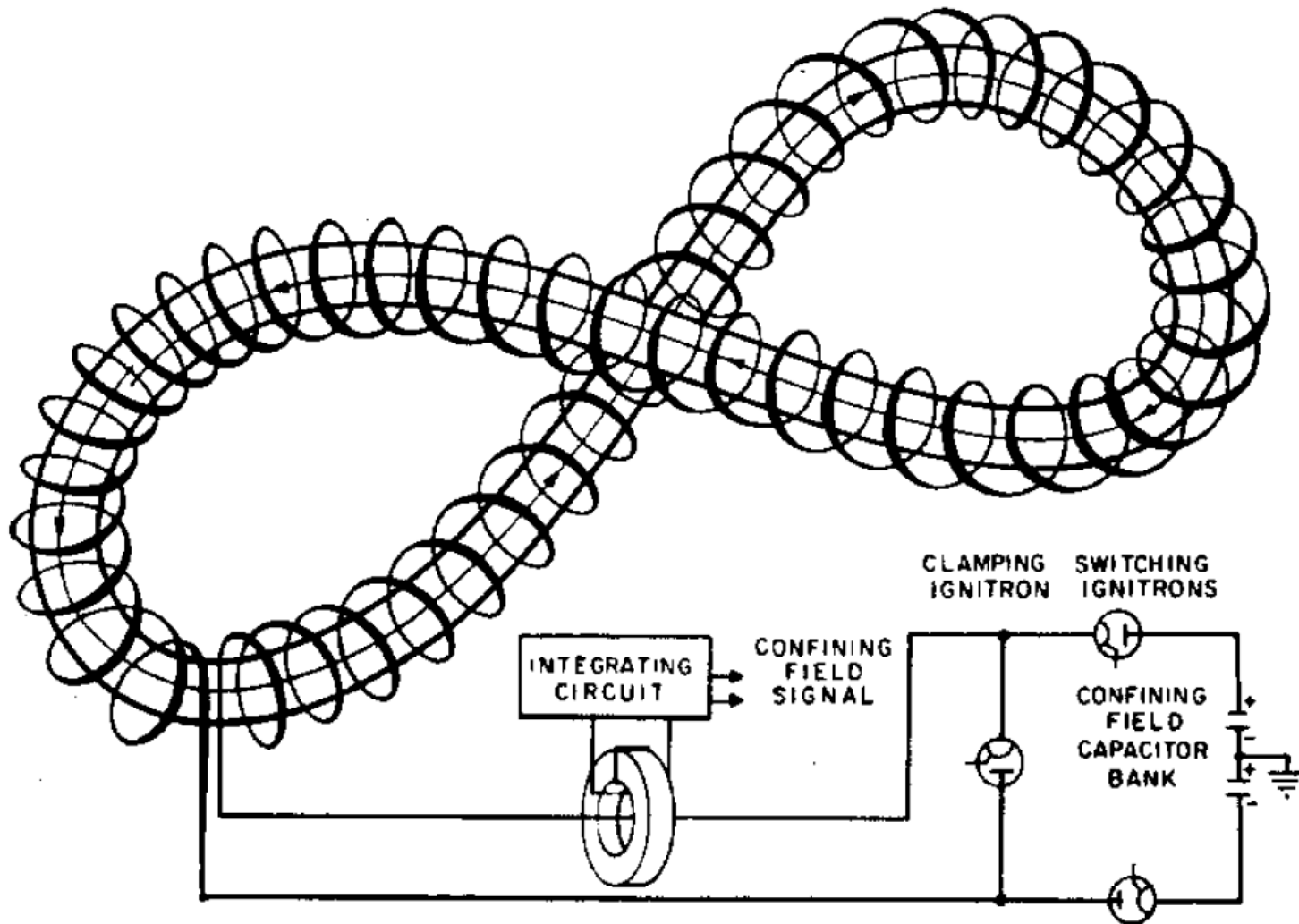
A figure-8 stellarator solved the drift issues



Lyman Spitzer, Jr. came out the idea during a long ride on a ski lift at Garmisch-Partenkirchen

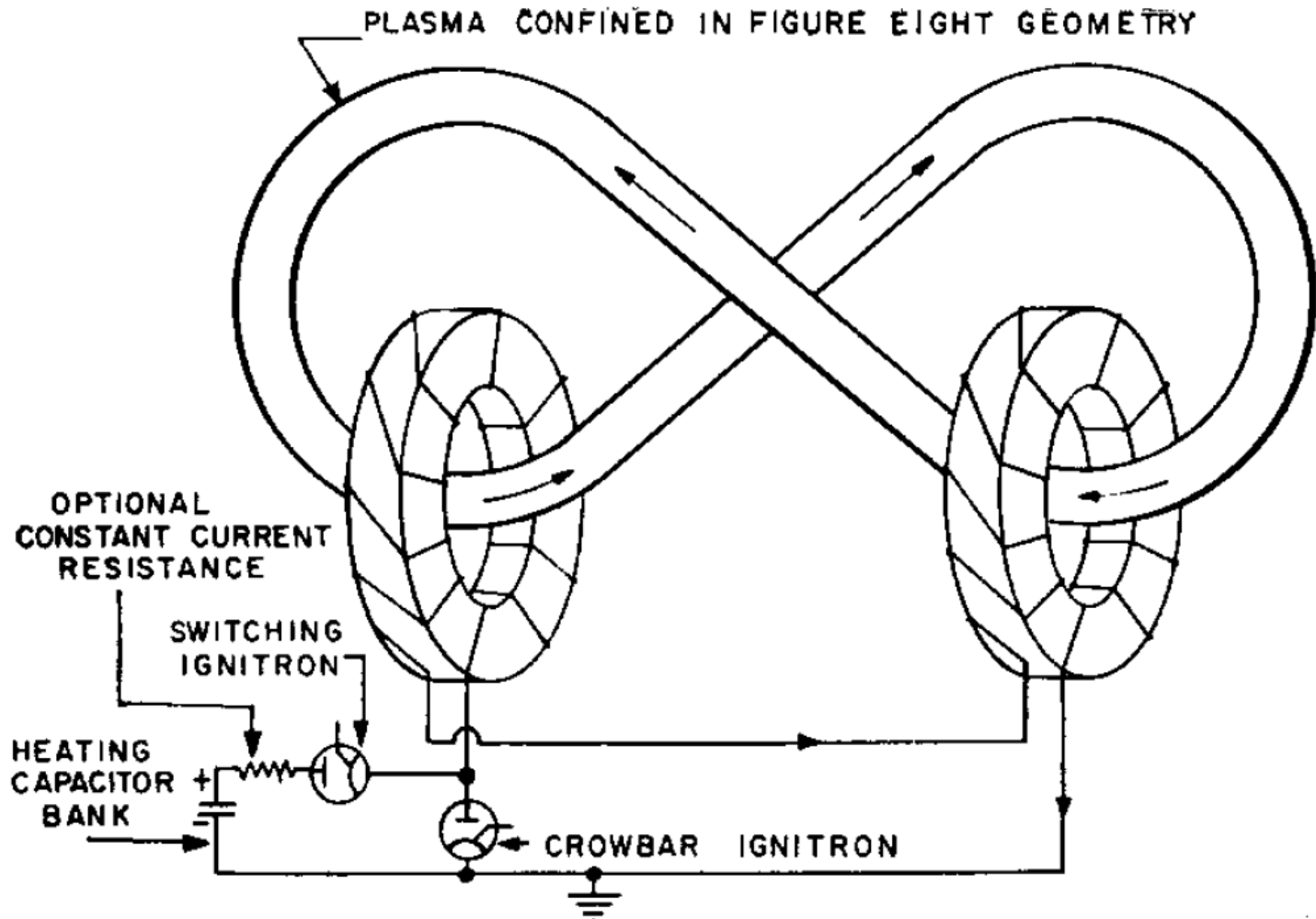


Concept of figure-8 stellarator



T. Coor, et al., Phys. Fluids 1, 411 (1958)

Figure-8 stellarator with ohmic heating apparatus



Schematic diagram of B-1 stellarator

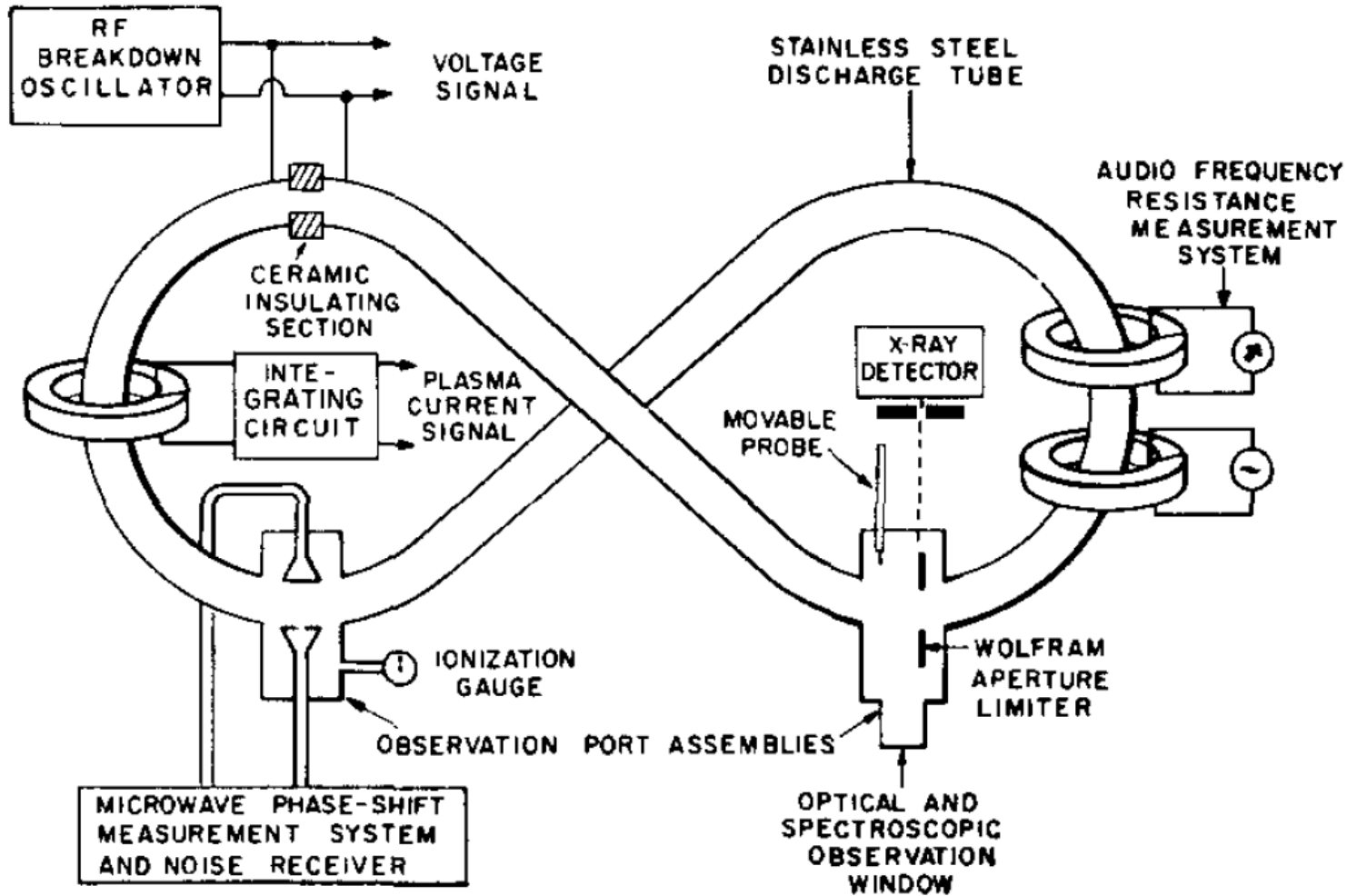
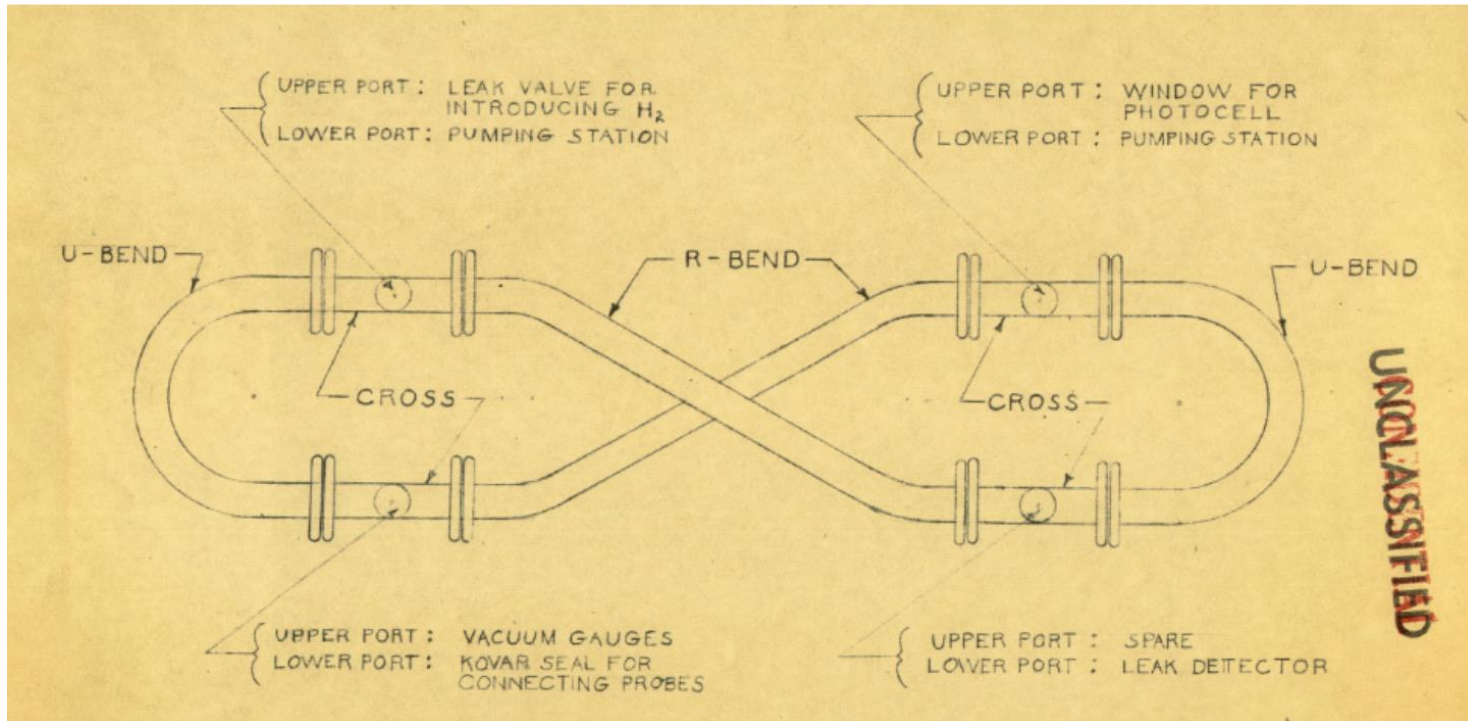
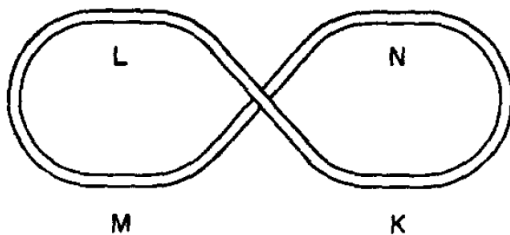


Figure-eight (Princeton Model A) – 1953-1958



- **Top view**



- **Side view**

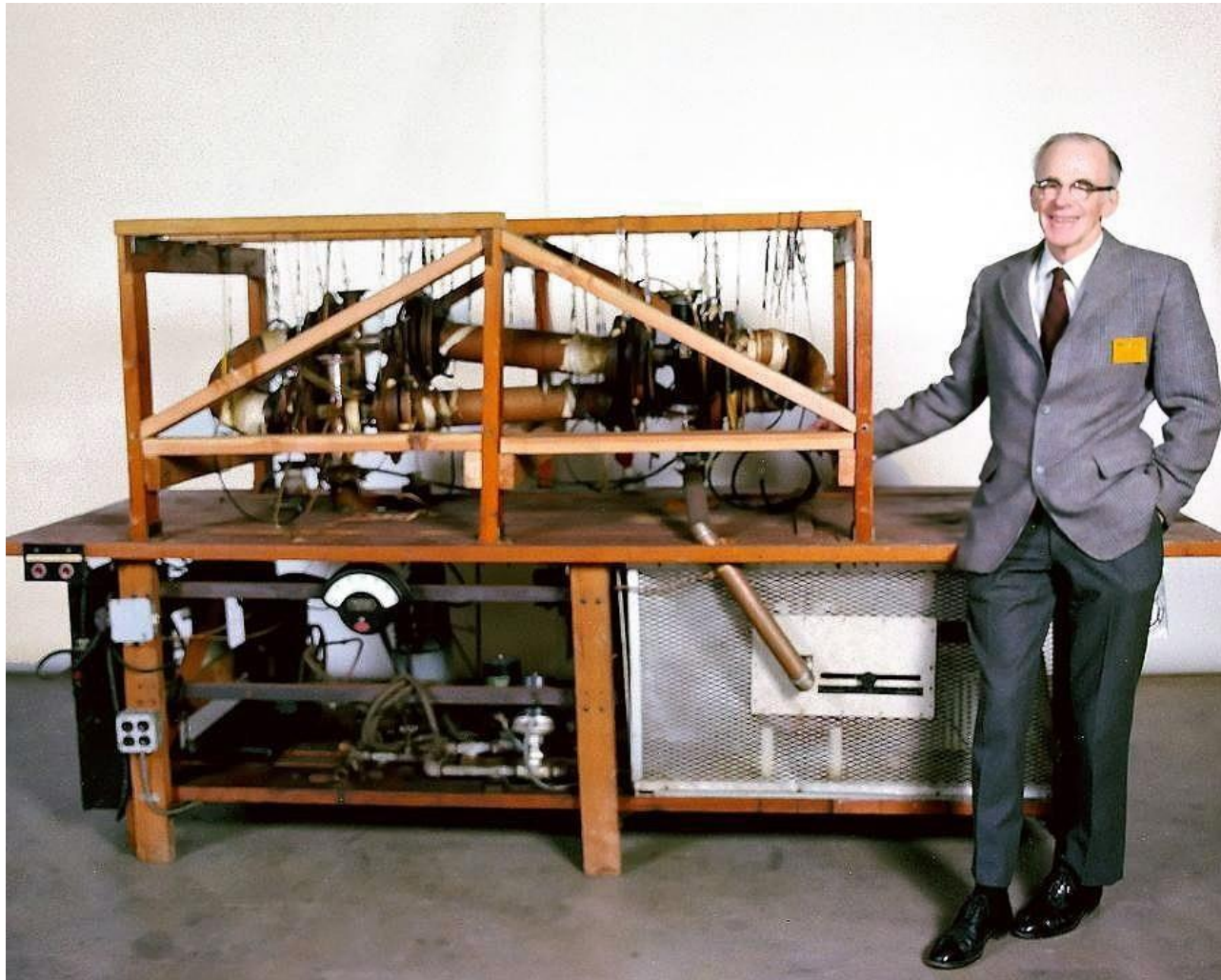


C. H. Willis, NJ Project Matterhorn (1953)
 L. Spitzer, Jr., Phys. Fluids 1, 253 (1958)

Model A stellarator

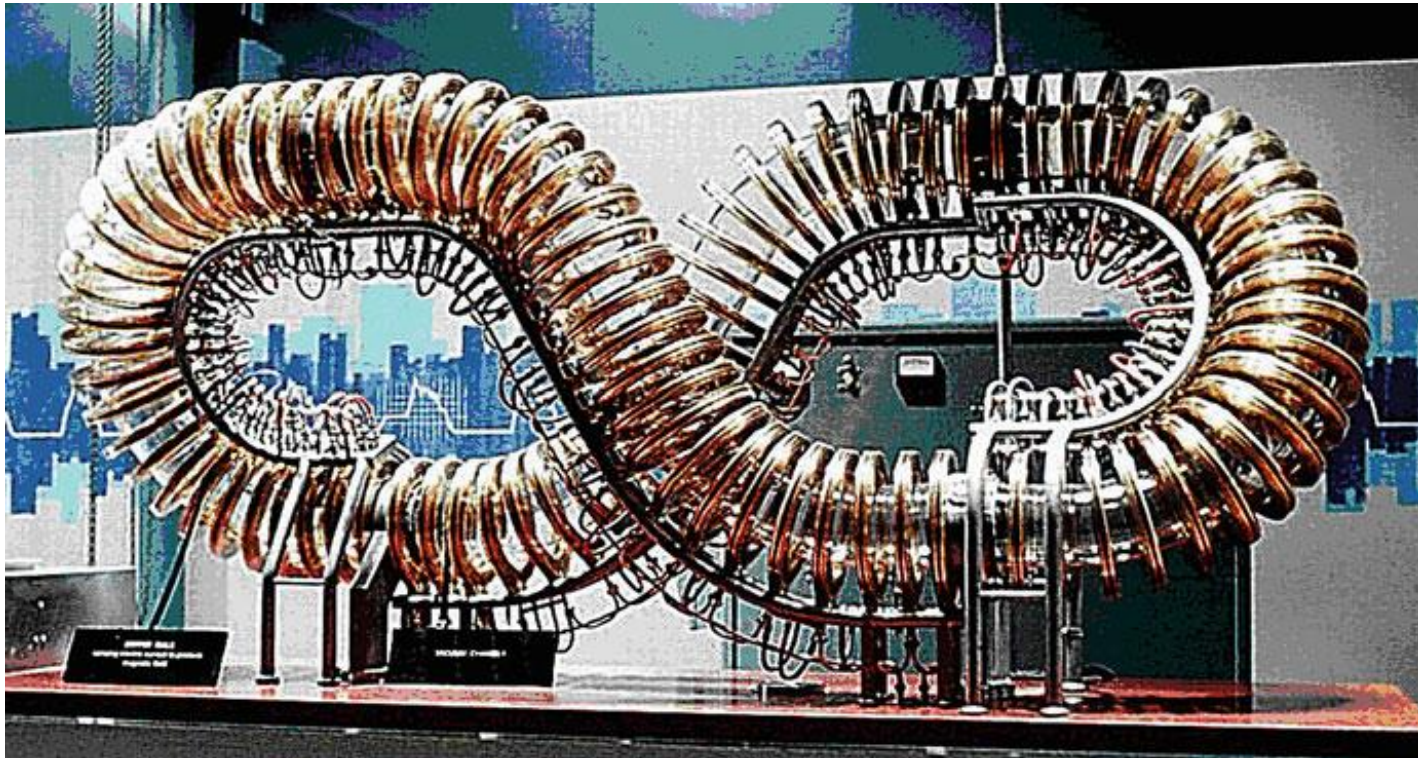


Model A stellarator



https://www.autoevolution.com/news/stellarator-reactors-the-once-forgotten-all-american-approach-to-nuclear-fusion-209478.html#agal_2

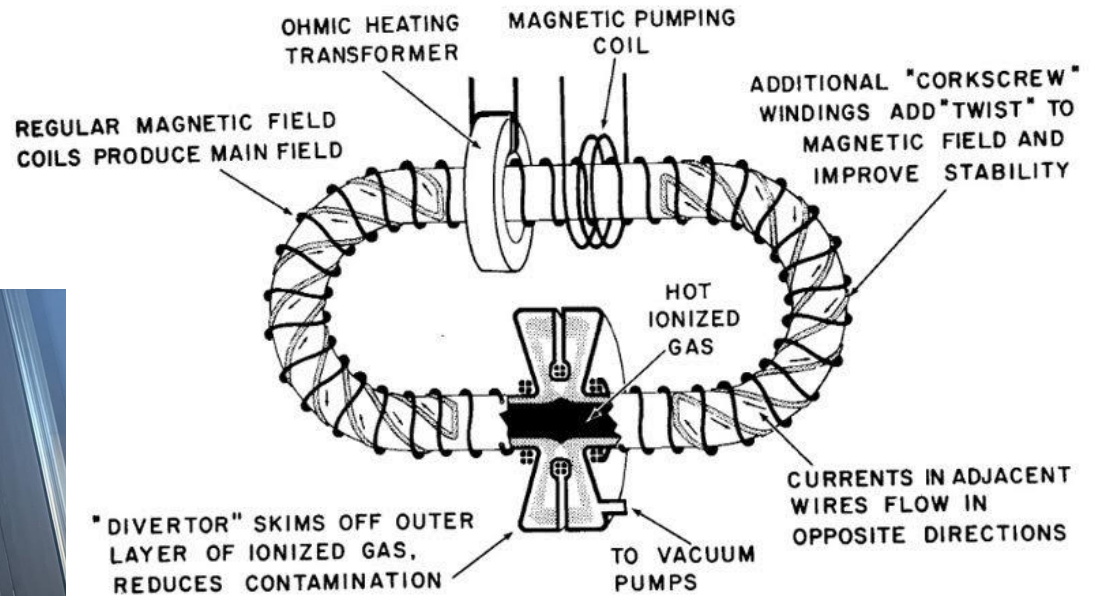
Exhibit model of a figure-8 stellarator for the Atoms for Peace conference in Geneva in 1958



Racetrack Stellarator (Project Matterhorn)

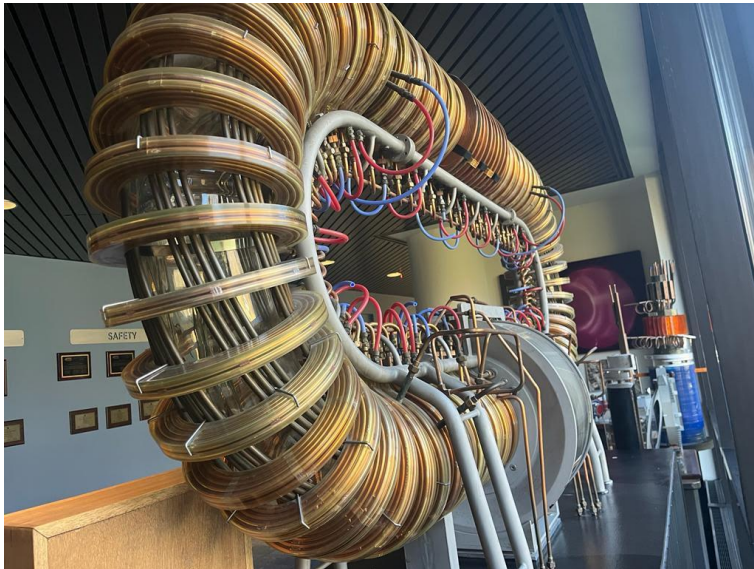
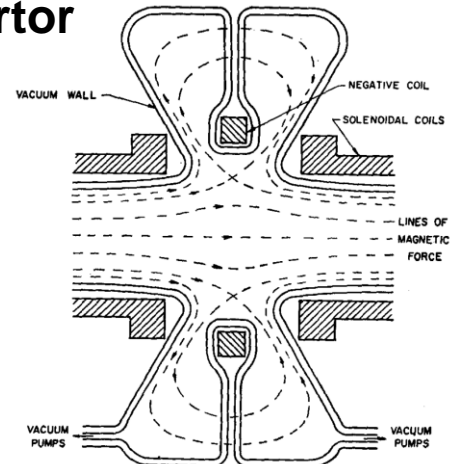


FIG. 4: SCHEMATIC "RACETRACK" STELLARATOR

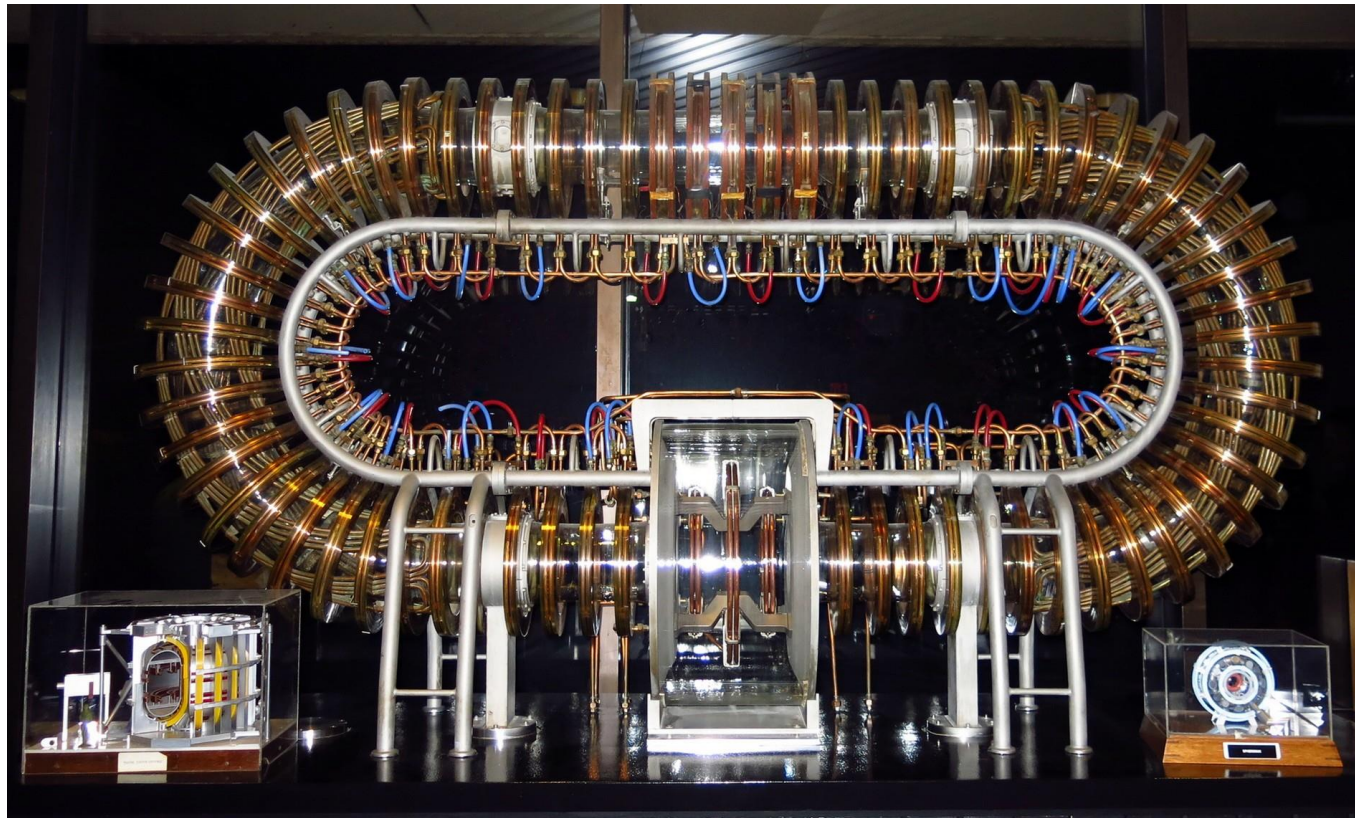


SEPTEMBER 19, 1958 ★ 9

- **Divertor**



Racetrack Stellarator



https://www.autoevolution.com/news/stellarator-reactors-the-once-forgotten-all-american-approach-to-nuclear-fusion-209478.html#agal_2

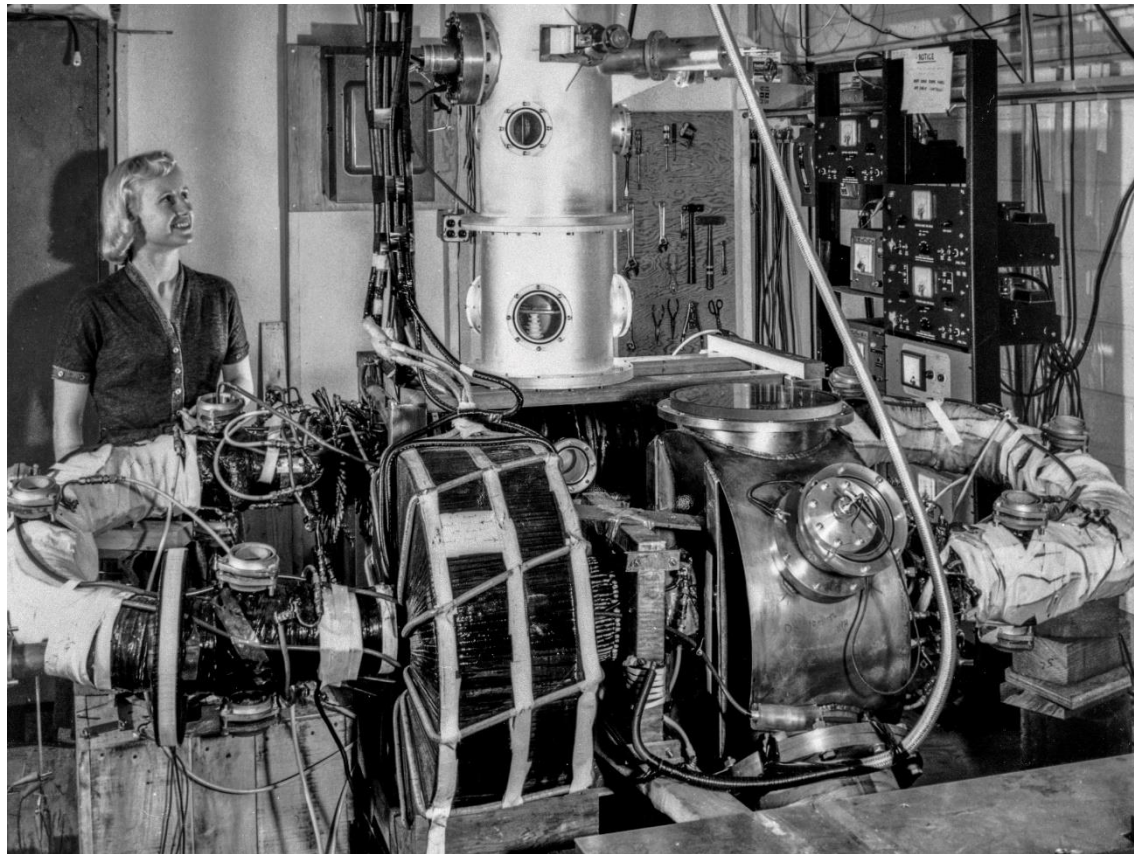
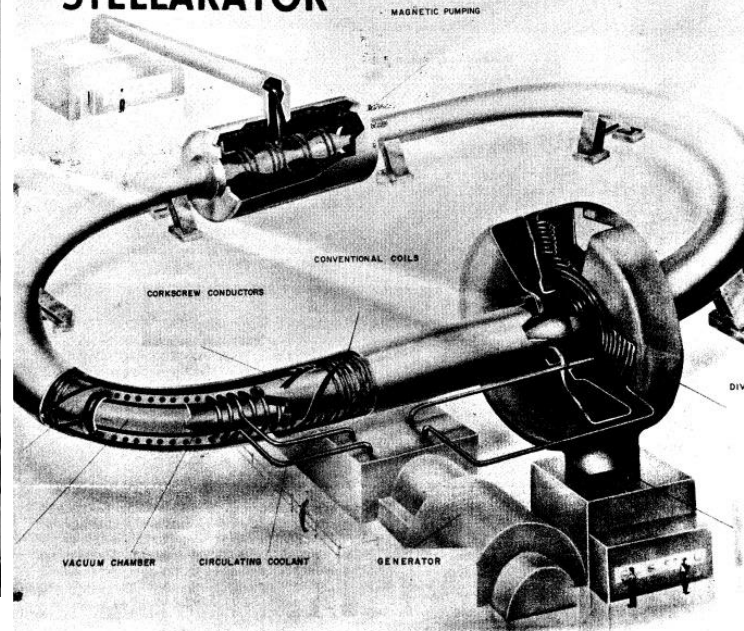
B-65 stellarator



PRINCETON ALUMNI WEEKLY

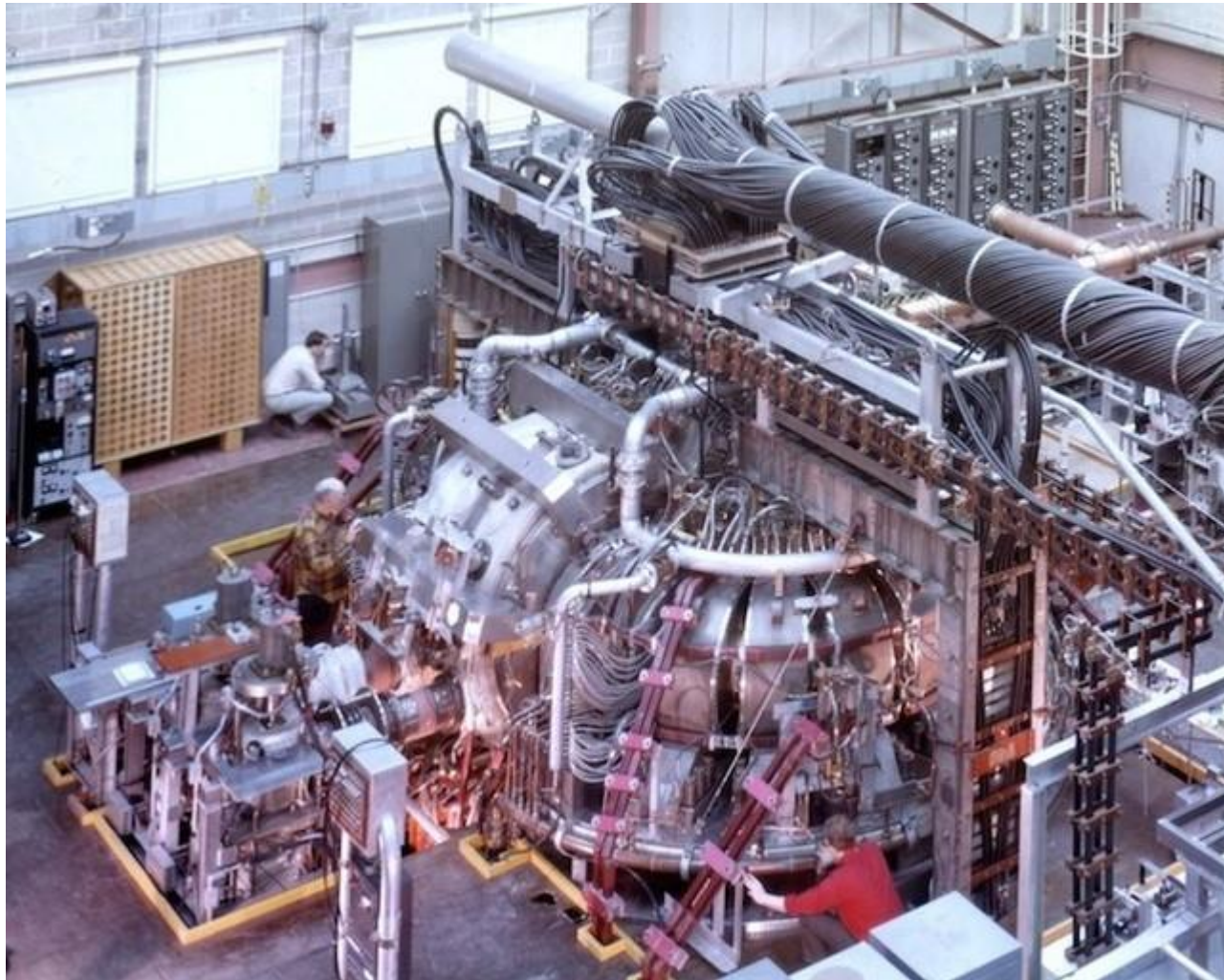
Vol. LIX • SEPTEMBER 19, 1958 • No. 1

STELLARATOR



<https://www.pppl.gov/timeline>
Elizabeth Paul, An introduction to stellarators,
Princeton Alumni Weekly, Sep. 19, 1958

Racetrack (Princeton Model C) – 1962-1969

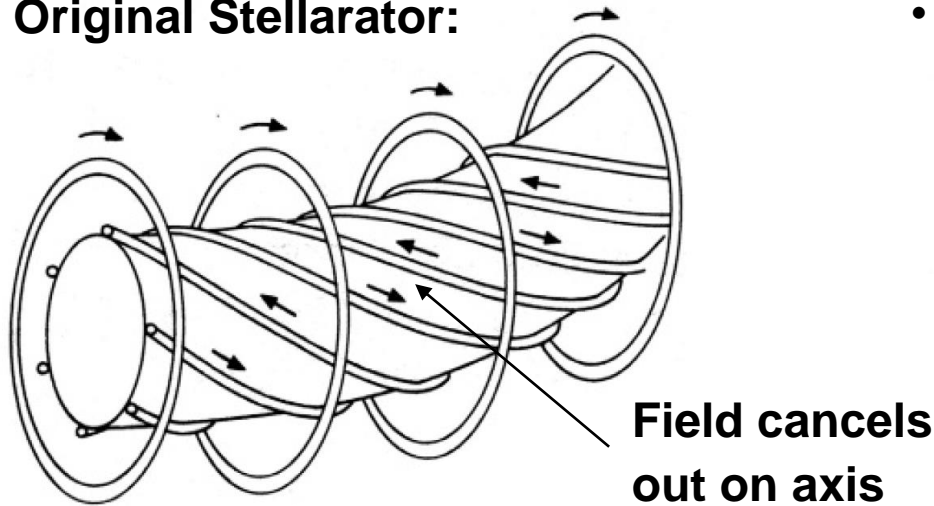


https://www.autoevolution.com/news/stellarator-reactors-the-once-forgotten-all-american-approach-to-nuclear-fusion-209478.html#agal_2

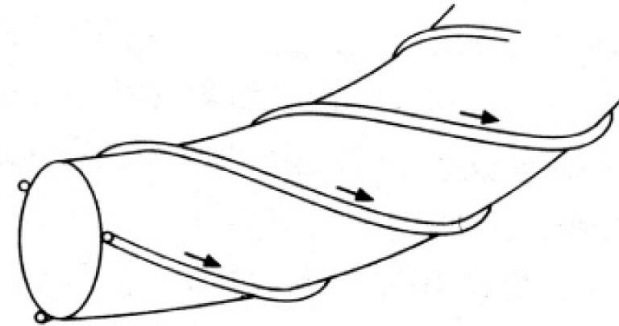
Different types of stellarators



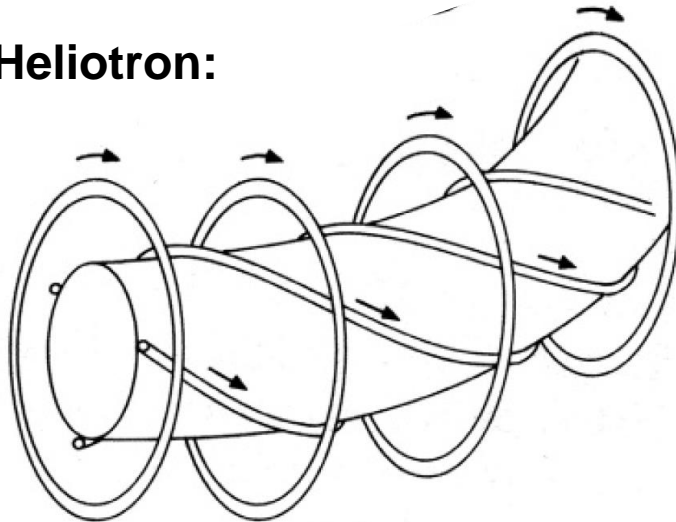
- **Original Stellarator:**



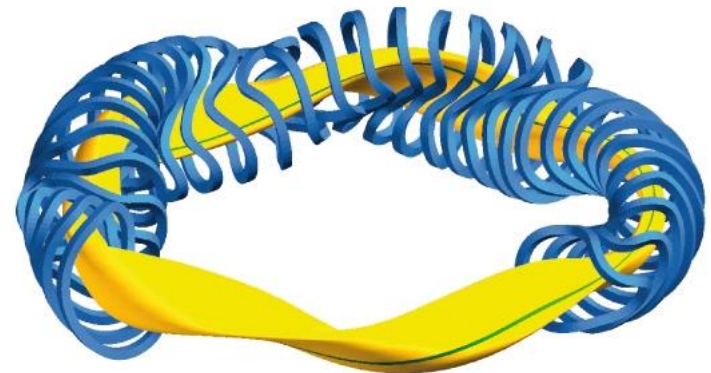
- **Torsatron:**



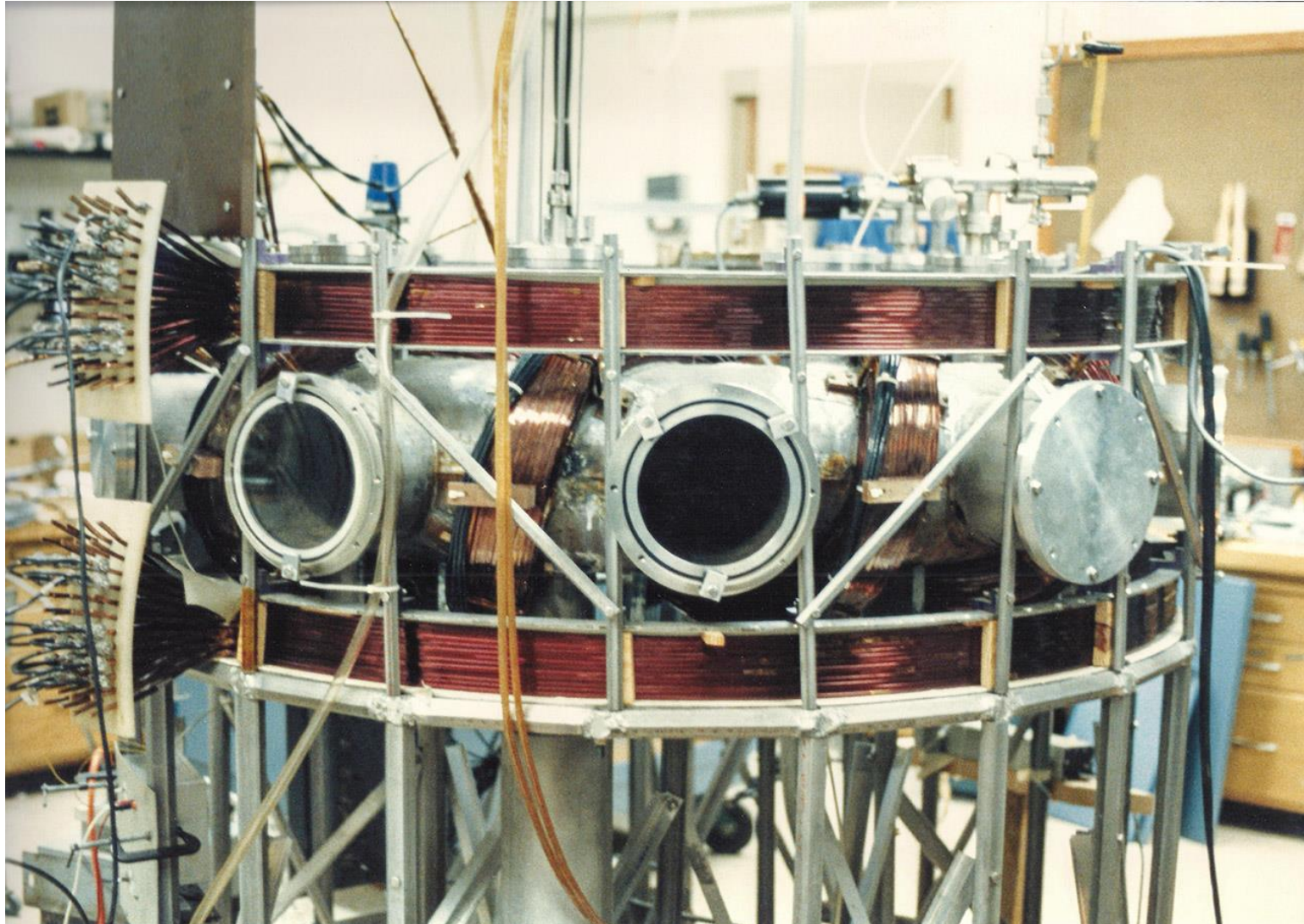
- **Heliotron:**



- **Helias:**



Auburn torsatron — winding of both helical and poloidal coils can be seen

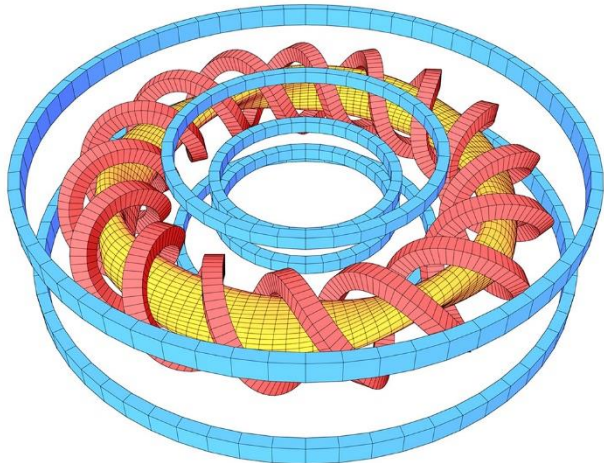
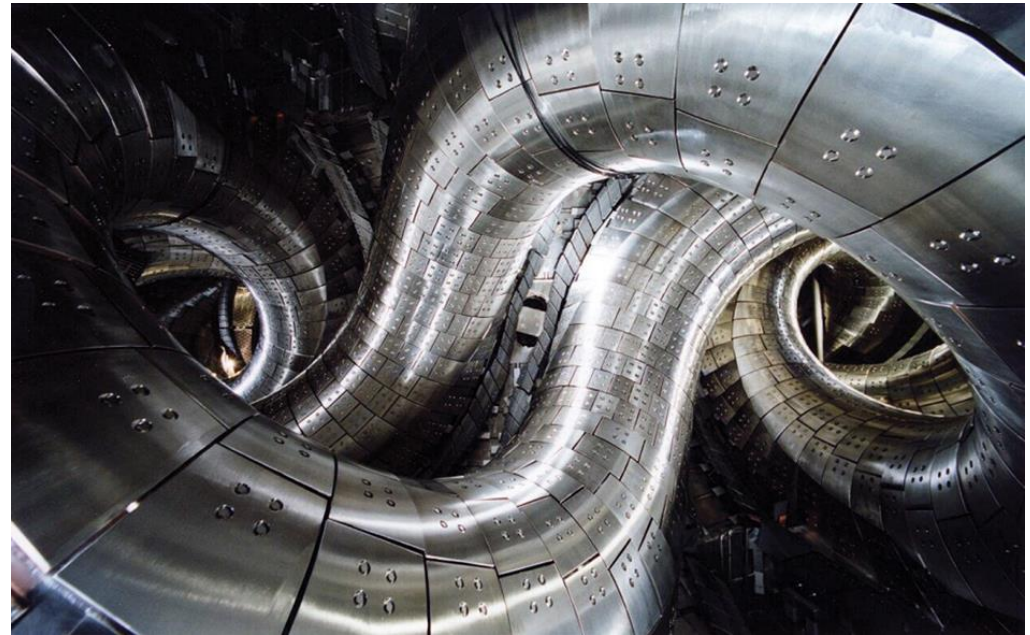
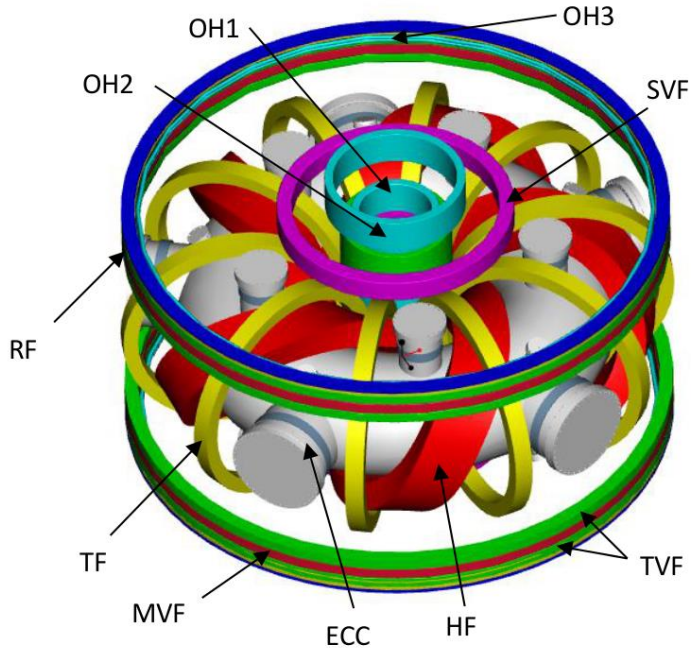


Construction of a pair of helical magnetic coils for the Advanced Toroidal Facility torsatron



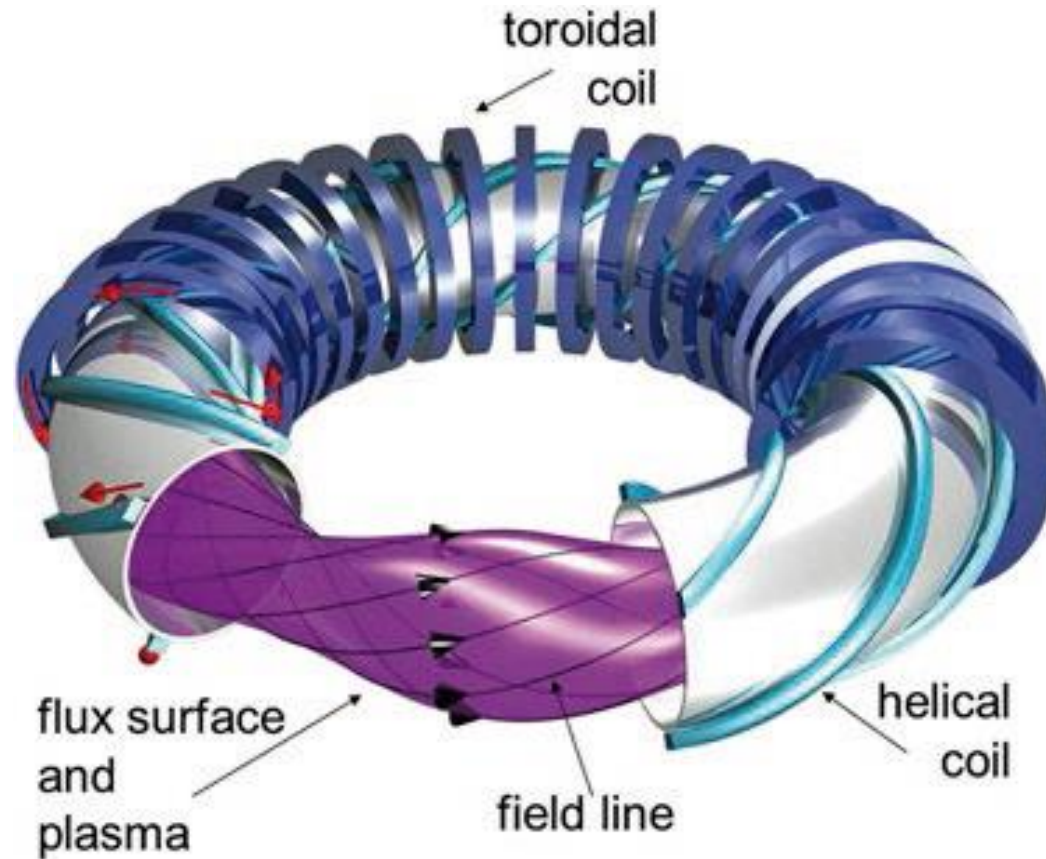
<https://www.energyencyclopedia.com/en/glossary/torsatron>

LHD stellarator in Japan (Heliotron)

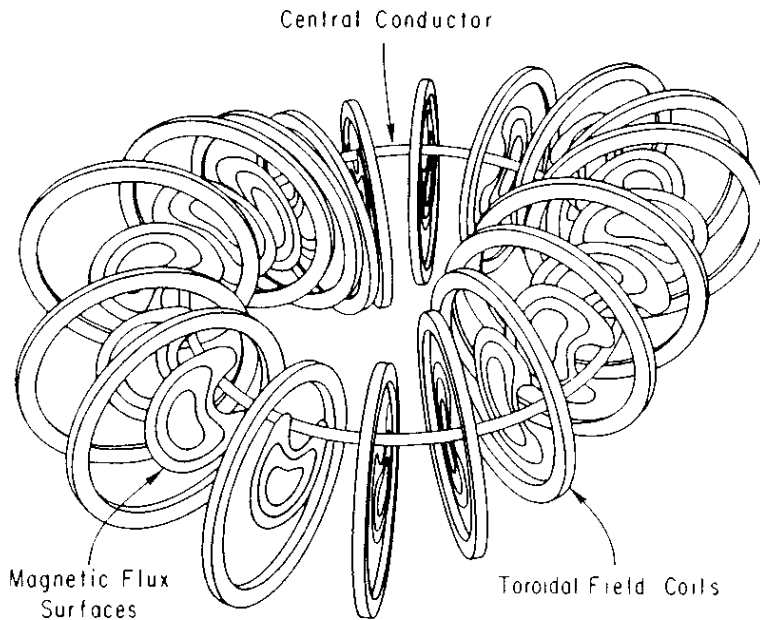


https://en.wikipedia.org/wiki/Compact_Toroidal_Hybrid
<https://www.energyencyclopedia.com/en/glossary/heliotron>
https://en.wikipedia.org/wiki/Large_Helical_Device

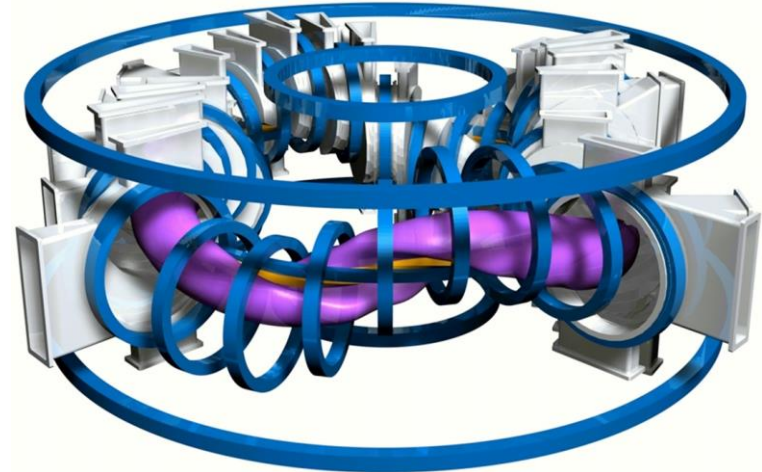
Twisted magnetic field lines can be provided by toroidal coils with helical coils



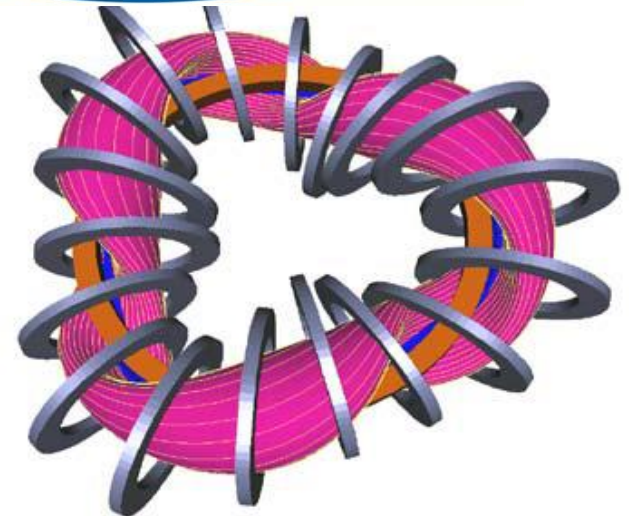
Heliac (Helical Axis stellarator)



- **TJ-II (Spain's National Fusion Laboratory):**



- **H-1 (Australian Plasma Fusion Research Facility):**

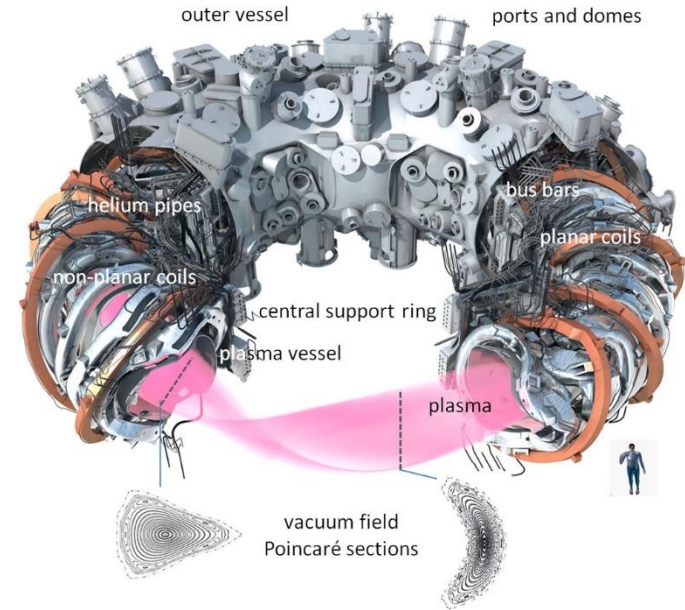
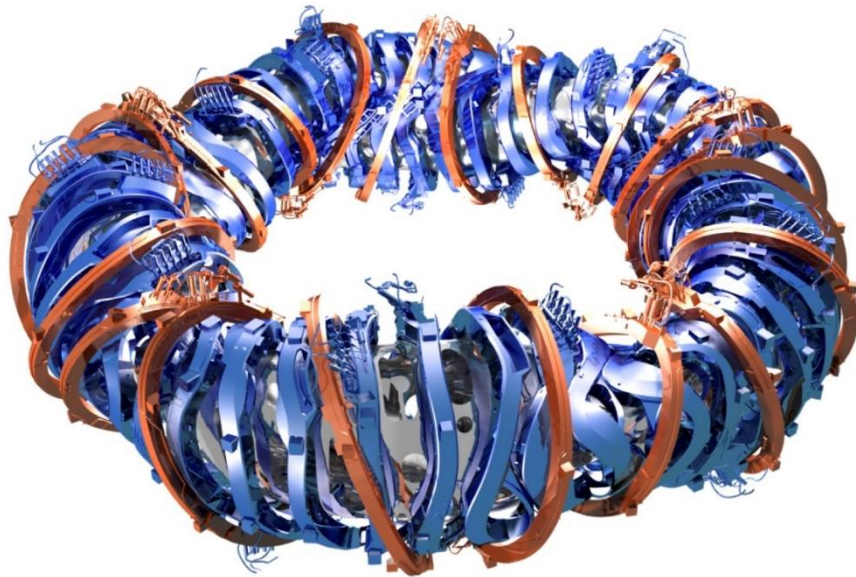


A. H. Boozer, Phys. Plasmas, 5, 1647 (1998)

<https://wiki.fusion.ciemat.es/wiki/TJ-II>

B. D. Blackwell, et. al, 23rd IAEA Fusion Energy Conference, 2010

Wendelstein 7-X is a (Helias) stellarator built by Max Planck Institute for Plasma Physics (IPP)



- **Wendelstein 7-x is now installing new diverters.**



Advantages of Stellarator



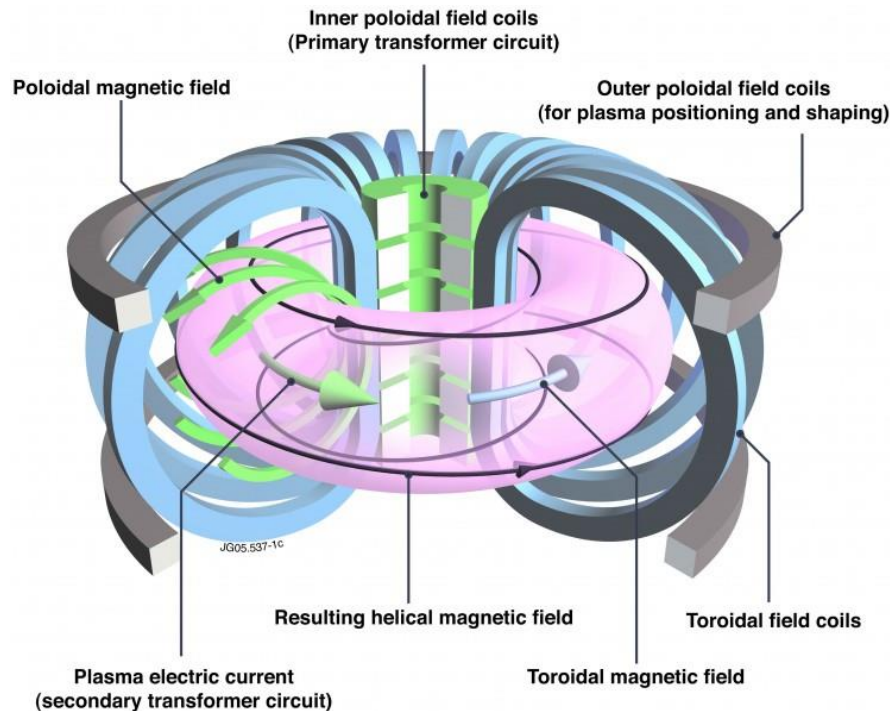
- **No need to drive plasma current. It is intrinsically steady state.**
- **With zero net current, one potentially dangerous class of MHD instabilities, the current-driven kink modes, is eliminated.**
- **Magnetic configuration is set by external coils, not by currents in the plasma. Stellarators do not suffer violent disruptions.**
- **Potential for greater range of designs and optimization of fusion performance.**

Disadvantages of Stellarator



- **Complicated coil configurations. It's difficult to design. The precision requirement is high. It is expensive to build coils for stellarators.**
- **Achieving good particle confinement in stellarators is more difficult than that in tokamaks.**
- **Divertors and heat load geometry in stellarators is more complicated than those in tokamaks.**

2D axisymmetric equilibrium of a torus plasma: Grad-Shafranov equation



$$\vec{j} \times \vec{B} = \nabla p$$



$$\vec{j} \perp \nabla p \quad \vec{B} \perp \nabla p$$



$$\vec{j} \cdot \nabla p = 0 \quad \vec{B} \cdot \nabla p = 0$$

$$\nabla \times \vec{B} = \mu_0 \vec{j} \quad \Rightarrow \quad \nabla \cdot \vec{j} = 0$$

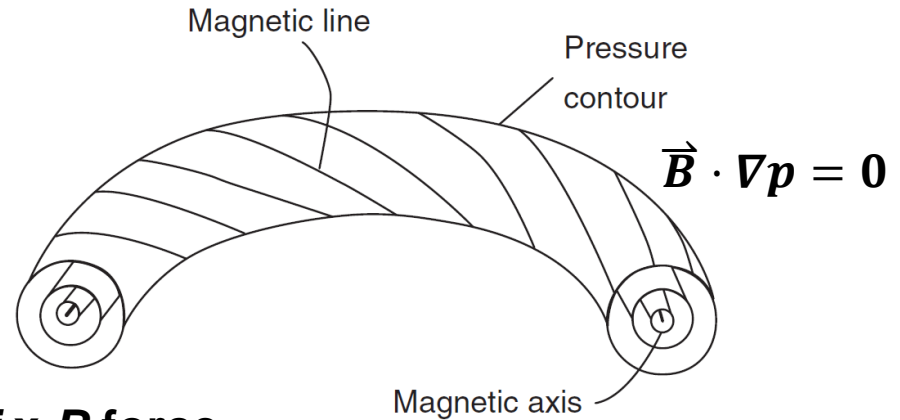
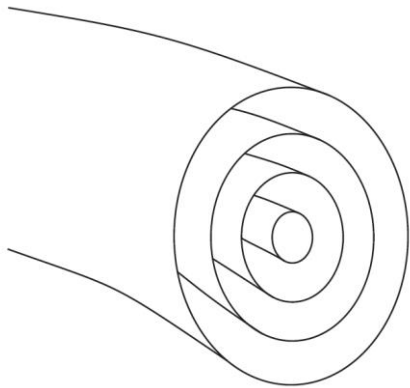
$$\nabla \cdot \vec{B} = 0$$

- The surfaces with $p = \text{constant}$ are both magnetic surfaces (i.e., they are made up of magnetic field lines) and current surfaces (i.e., they are made of current flow lines).

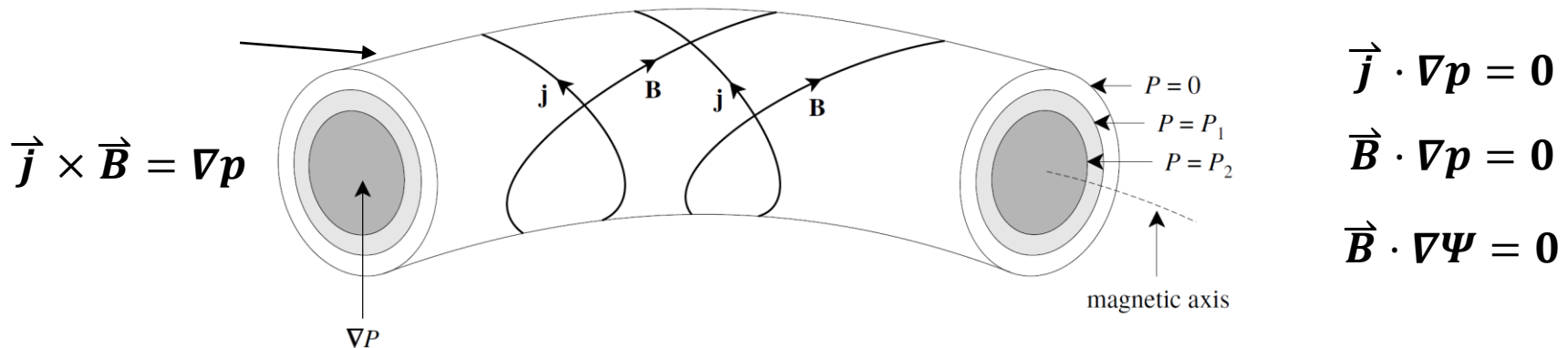
Magnetic lines lying on pressure contour



- Contours of constant pressure
- Magnetic lines lying on pressure contour



- Pressure gradient is balanced by the $\vec{j} \times \vec{B}$ force



- A magnetic (or flux) surface is one that is everywhere tangential to the field, i.e., the normal to the surface is everywhere perpendicular to \vec{B} .

Derivation of Grad-Shafranov equation



$$\vec{j} \times \vec{B} = \nabla p \quad \nabla \times \vec{B} = \mu_0 \vec{j}$$

$$\nabla \cdot \vec{j} = 0 \quad \nabla \cdot \vec{B} = 0$$

$$\vec{B} = (B_R, B_\phi, B_z) \quad \text{Axisymmetric: } \frac{\partial}{\partial \phi} = 0$$

$$\nabla \cdot \vec{B} = 0$$

$$\frac{1}{R} \frac{\partial}{\partial R} (R B_R) + \frac{1}{R} \frac{\partial B_\phi}{\partial \phi} + \frac{\partial B_z}{\partial z} = 0$$

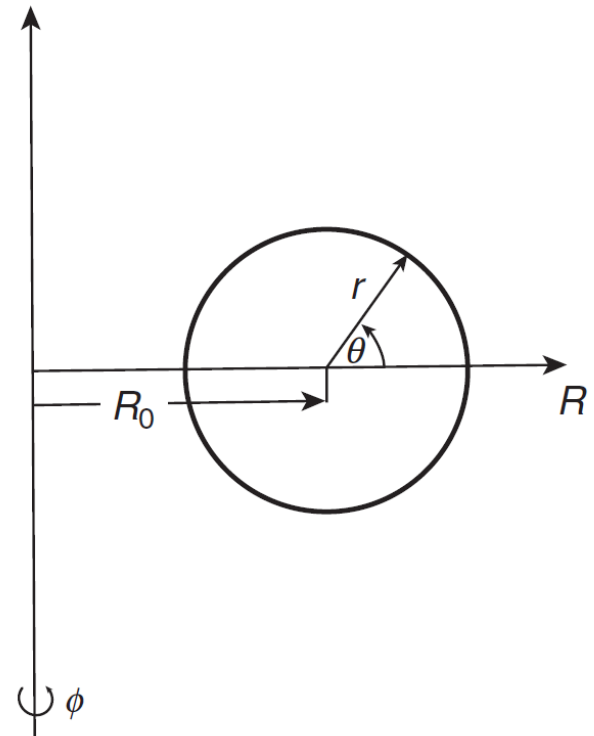
$$\frac{1}{R} \frac{\partial}{\partial R} (R B_R) + \frac{\partial B_z}{\partial z} = 0$$

- Represent the magnetic field using a vector potential A :

$$\vec{B} = \nabla \times \vec{A} = \hat{R} \left(\frac{1}{R} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) + \hat{\phi} \left(\frac{\partial A_R}{\partial z} - \frac{\partial A_z}{\partial R} \right) + \hat{z} \left(\frac{1}{R} \frac{\partial}{\partial R} (R A_\phi) - \frac{1}{R} \frac{\partial A_R}{\partial \phi} \right)$$

$$= \hat{R} \left(-\frac{\partial A_\phi}{\partial z} \right) + \hat{\phi} \left(\frac{\partial A_R}{\partial z} - \frac{\partial A_z}{\partial R} \right) + \hat{z} \left(\frac{1}{R} \frac{\partial}{\partial R} (R A_\phi) \right)$$

$$\equiv \hat{R} B_R + \hat{\phi} B_\phi + \hat{z} B_z \quad B_R = -\frac{\partial A_\phi}{\partial z} \quad B_z = \frac{1}{R} \frac{\partial}{\partial R} (R A_\phi)$$



Pressure can be written as a function of flux



$$\frac{1}{R} \frac{\partial}{\partial R} (RB_R) + \frac{\partial B_z}{\partial z} = 0$$

$$B_R = -\frac{\partial A_\phi}{\partial z}$$

$$B_z = \frac{1}{R} \frac{\partial}{\partial R} (RA_\phi)$$

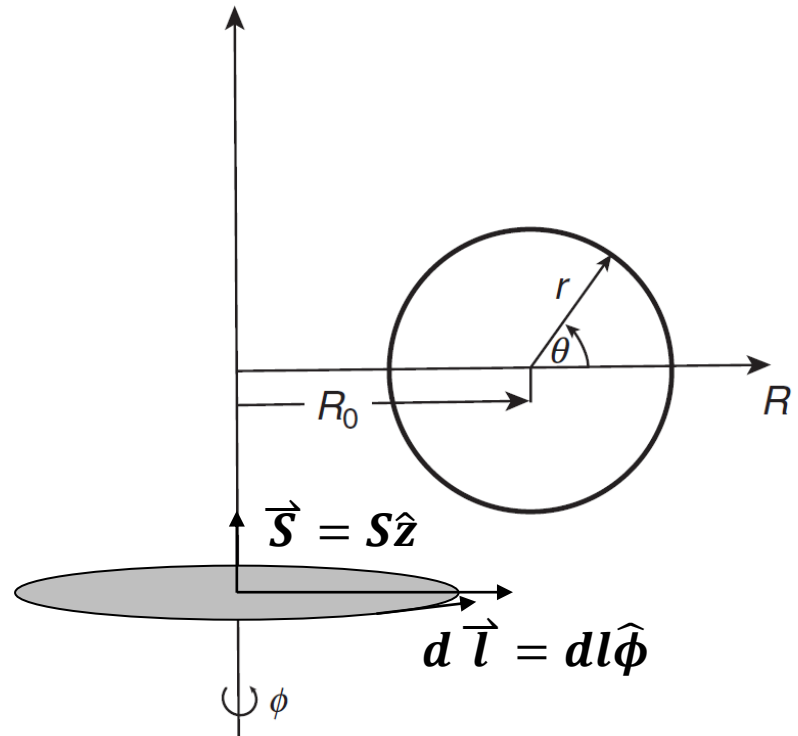
$$\psi \equiv \frac{1}{2\pi} \int \vec{B} \cdot d\vec{S} = \frac{1}{2\pi} \int (\nabla \times \vec{A}) \cdot d\vec{S}$$

$$= \frac{1}{2\pi} \int \vec{A} \cdot 2\pi R \cdot d\vec{l} = \int \vec{A} \cdot \hat{\phi} R dl = RA_\phi$$

$$B_R = -\frac{1}{R} \frac{\partial \psi}{\partial z} \quad B_z = \frac{1}{R} \frac{\partial \psi}{\partial R}$$

$$\vec{B} \cdot \nabla \psi = B_R \frac{\partial \psi}{\partial R} + B_\phi \frac{1}{R} \frac{\partial \psi}{\partial \phi} + B_z \frac{\partial \psi}{\partial z} = B_R \frac{\partial \psi}{\partial R} + B_z \frac{\partial \psi}{\partial z}$$

$$= \left(-\frac{1}{R} \frac{\partial \psi}{\partial z} \right) \frac{\partial \psi}{\partial R} + \left(\frac{1}{R} \frac{\partial \psi}{\partial R} \right) \frac{\partial \psi}{\partial z} = 0$$



$$\vec{B} \cdot \nabla \psi = 0$$

$$\vec{B} \cdot \nabla p = 0$$

for $\nabla p \neq 0$:

$$p = p(\psi)$$

Derivation of Grad-Shafranov equation



- Let's see the $\hat{\phi}$ component of the force-balance equation:

$$(\vec{j} \times \vec{B} = \nabla p)_{\phi} \quad j_z B_R - j_R B_z = \frac{1}{R} \frac{\partial p}{\partial \phi} \equiv 0$$

- Ampère's law:

$$\nabla \times \vec{B} = \mu_0 \vec{j}$$

$$\begin{aligned} \nabla \times \vec{B} &= \hat{R} \left(\frac{1}{R} \frac{\partial B_z}{\partial \phi} - \frac{\partial B_{\phi}}{\partial z} \right) + \hat{\phi} \left(\frac{\partial B_R}{\partial z} - \frac{\partial B_z}{\partial R} \right) + \hat{z} \left(\frac{1}{R} \frac{\partial}{\partial R} (R B_{\phi}) - \frac{1}{R} \frac{\partial B_R}{\partial \phi} \right) \\ &= \hat{R} \left(-\frac{\partial B_{\phi}}{\partial z} \right) + \hat{\phi} \left(\frac{\partial B_R}{\partial z} - \frac{\partial B_z}{\partial R} \right) + \hat{z} \left(\frac{1}{R} \frac{\partial}{\partial R} (R B_{\phi}) \right) \\ &= \hat{R} \mu_0 j_R + \hat{\phi} \mu_0 j_{\phi} + \hat{z} \mu_0 j_z \end{aligned}$$

$$j_R = -\frac{1}{\mu_0} \frac{\partial B_{\phi}}{\partial z} \quad j_z = \frac{1}{\mu_0} \frac{1}{R} \frac{\partial}{\partial R} (R B_{\phi})$$

$$\frac{B_R}{R} \frac{\partial}{\partial R} (R B_{\phi}) + B_z \frac{\partial B_{\phi}}{\partial z} = 0$$

Magnetic field can be decomposed into the poloidal component and the toroidal component



$$\frac{B_R}{R} \frac{\partial}{\partial R} (RB_\phi) + B_z \frac{\partial B_\phi}{\partial z} = 0 \quad \Rightarrow \quad B_R \frac{\partial}{\partial R} (RB_\phi) + B_z \frac{\partial}{\partial z} (RB_\phi) = 0$$

$$F \equiv RB_\phi \quad \Rightarrow \quad B_R \frac{\partial F}{\partial R} + B_z \frac{\partial F}{\partial z} = 0 \quad \Rightarrow \quad \vec{B} \cdot \nabla F = 0$$

$$\left(\frac{\partial}{\partial \phi} = 0 \right)$$

$$\vec{B} \cdot \nabla p = 0$$

$$p = p(\psi)$$

$$B_R = -\frac{\partial A_\phi}{\partial z} = -\frac{1}{R} \frac{\partial \psi}{\partial z}$$

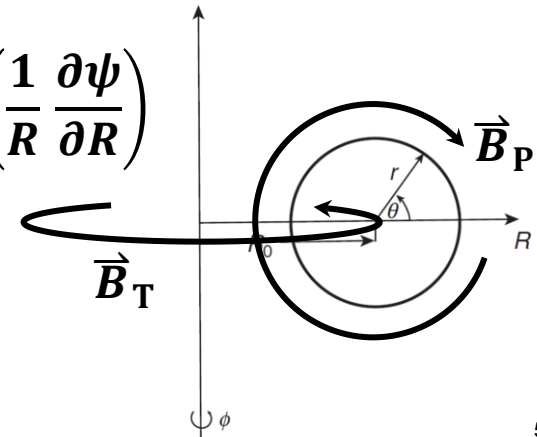
$$B_z = \frac{1}{R} \frac{\partial}{\partial R} (RA_\phi) = \frac{1}{R} \frac{\partial \psi}{\partial R} \quad (\psi = RA_\phi)$$

$$B_\phi = \frac{F(\psi)}{R}$$

$$F = F(\psi)$$

$$\vec{B} = \hat{R}B_R + \hat{\phi}B_\phi + \hat{z}B_z = \hat{R} \left(-\frac{1}{R} \frac{\partial \psi}{\partial z} \right) + \hat{\phi} \left(\frac{F(\psi)}{R} \right) + \hat{z} \left(\frac{1}{R} \frac{\partial \psi}{\partial R} \right)$$

$$\equiv \left(\frac{\nabla \psi}{R} \right) \times \hat{\phi} + \frac{F(\psi)}{R} \hat{\phi}$$



Poloidal
component \vec{B}_P

Toroidal
component \vec{B}_T

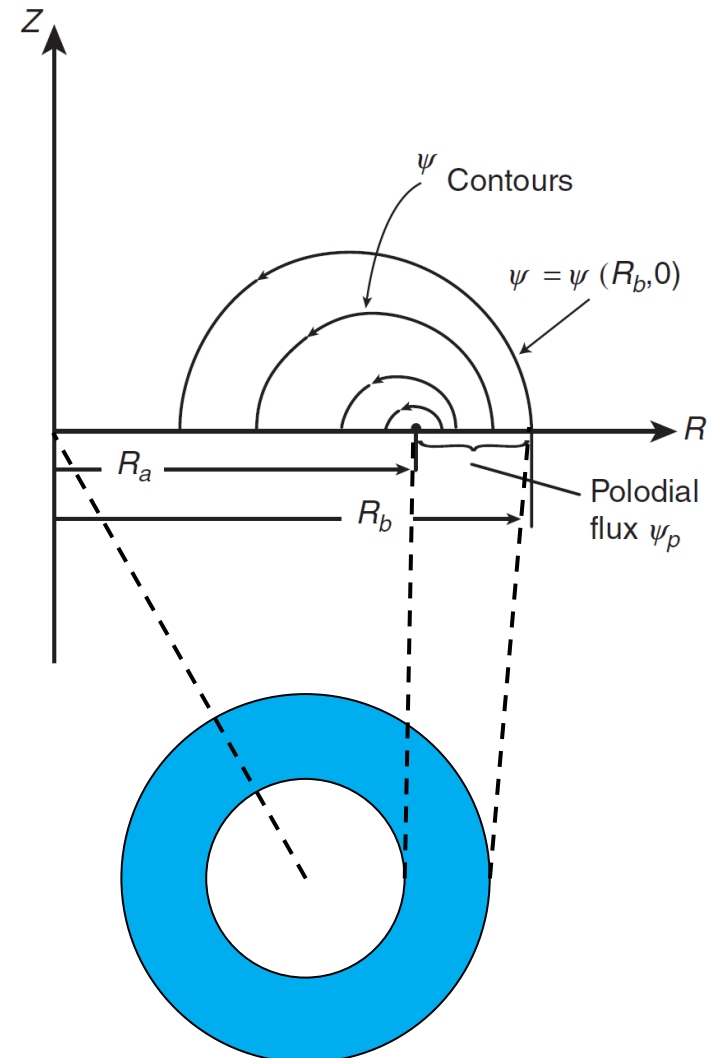
Arbitrary integration constant associated with flux can be chosen such that flux equals to zero on the field axis



- The poloidal flux of the area of a washer-shaped surface lying in the $z = 0$ plane from $R = R_a$ to an arbitrary ψ contour defined by $\psi = \psi(R_b, 0)$:

$$\begin{aligned}\psi_P &\equiv \frac{1}{2\pi} \int \vec{B}_P \cdot d\vec{S} \\ &= \frac{1}{2\pi} \int_0^{2\pi} d\phi \int_{R_a}^{R_b} dR R B_z(R, 0) \\ &= \psi(R_b, 0) - \psi(R_a, 0) \\ &\equiv \psi(R_b, 0)\end{aligned}$$

where $\psi(R_a, 0) \equiv 0$ is chosen.



Derivation of Grad-Shafranov equation



- Let's see the \hat{R} component of the force-balance equation:

$$(\vec{j} \times \vec{B} = \nabla p)_R \quad j_\phi B_z - j_z B_\phi = \frac{\partial p}{\partial R}$$

$$B_R = -\frac{1}{R} \frac{\partial \psi}{\partial z}$$

$$B_z = \frac{1}{R} \frac{\partial \psi}{\partial R}$$

- Ampère's law:

$$\nabla \times \vec{B} = \mu_0 \vec{j}$$

$$B_\phi = \frac{F(\psi)}{R}$$

$$\nabla \times \vec{B} = \hat{R} \left(-\frac{\partial B_\phi}{\partial z} \right) + \hat{\phi} \left(\frac{\partial B_R}{\partial z} - \frac{\partial B_z}{\partial R} \right) + \hat{z} \left(\frac{1}{R} \frac{\partial}{\partial R} (R B_\phi) \right) = \hat{R} \mu_0 j_R + \hat{\phi} \mu_0 j_\phi + \hat{z} \mu_0 j_z$$

$$\mu_0 j_\phi = \frac{\partial B_R}{\partial z} - \frac{\partial B_z}{\partial R} = \frac{\partial}{\partial z} \left(-\frac{1}{R} \frac{\partial \psi}{\partial z} \right) - \frac{\partial}{\partial R} \left(\frac{1}{R} \frac{\partial \psi}{\partial R} \right) = -\frac{1}{R} \frac{\partial^2 \psi}{\partial z^2} - \frac{1}{R} \frac{\partial^2 \psi}{\partial R^2} + \frac{1}{R^2} \frac{\partial \psi}{\partial R}$$

$$\equiv -\frac{1}{R} \Delta^* \psi \quad \text{where } \Delta^* \psi \equiv \frac{\partial^2 \psi}{\partial z^2} + R \frac{\partial}{\partial R} \left(\frac{1}{R} \frac{\partial \psi}{\partial R} \right) = R^2 \nabla \cdot \left(\frac{\nabla \psi}{R^2} \right)$$

$$\mu_0 j_z = \frac{1}{R} \frac{\partial}{\partial R} (R B_\phi) = \frac{1}{R} \frac{\partial F}{\partial R} = \frac{1}{R} \frac{dF}{d\psi} \frac{\partial \psi}{\partial R}$$

Derivation of Grad-Shafranov equation



$$j_{\phi} B_z - j_z B_{\phi} = \frac{\partial p}{\partial R}$$

$$B_{\phi} = \frac{F}{R}$$

$$B_z = \frac{1}{R} \frac{\partial \psi}{\partial R}$$

$$j_{\phi} = -\frac{1}{\mu_0 R} \Delta^* \psi$$

$$j_z = \frac{1}{\mu_0 R} \frac{dF}{d\psi} \frac{\partial \psi}{\partial R}$$

$$\frac{\partial p}{\partial R} = \frac{dp}{d\psi} \frac{\partial \psi}{\partial R}$$

$$-\frac{1}{\mu_0 R} \Delta^* \psi \frac{1}{R} \frac{\partial \psi}{\partial R} - \frac{1}{\mu_0 R} \frac{dF}{d\psi} \frac{\partial \psi}{\partial R} \frac{F}{R} = \frac{dp}{d\psi} \frac{\partial \psi}{\partial R}$$

$$-\Delta^* \psi \frac{1}{\mu_0} \frac{1}{R^2} - \frac{1}{\mu_0} \frac{F}{R^2} \frac{dF}{d\psi} = \frac{dp}{d\psi}$$

$$\text{Grad - Shafranov equation: } \Delta^* \psi = -\mu_0 R^2 \frac{dp}{d\psi} - \frac{1}{2} \frac{dF^2}{d\psi}$$

$$\text{where } \Delta^* \psi = R^2 \nabla \cdot \left(\frac{\nabla \psi}{R^2} \right) \quad \vec{B} = \left(\frac{\nabla \psi}{R} \right) \times \hat{\phi} + \frac{F(\psi)}{R} \hat{\phi}$$

Derivation of Grad-Shafranov equation



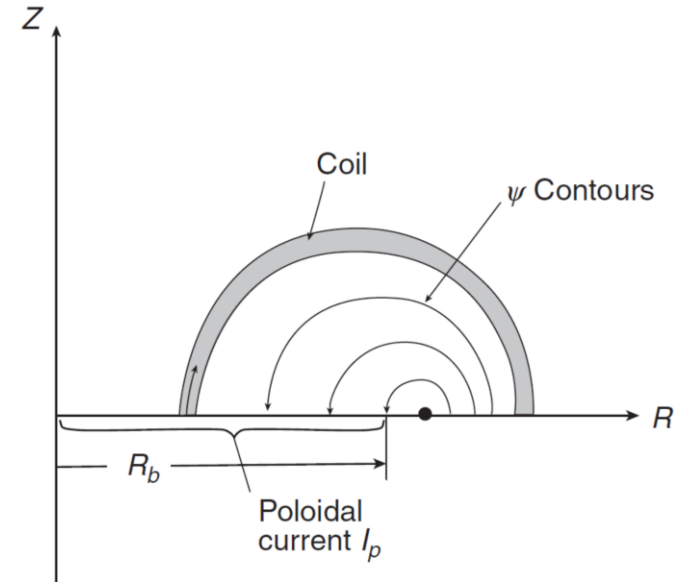
$$\Delta^* \psi = -\mu_0 R^2 \frac{dp}{d\psi} - \frac{1}{2} \frac{dF^2}{d\psi} \quad \text{where } \Delta^* \psi = R^2 \nabla \cdot \left(\frac{\nabla \psi}{R^2} \right) \quad \vec{B} = \left(\frac{\nabla \psi}{R} \right) \times \hat{\phi} + \frac{F(\psi)}{R} \hat{\phi}$$

$$\mu_0 j_\phi = -\frac{1}{R} \Delta^* \psi \quad \mu_0 j_z = \frac{1}{R} \frac{\partial F}{\partial R} \quad F \equiv RB_\phi$$

$$\mu_0 j_R = -\frac{\partial B_\phi}{\partial z} = -\frac{1}{R} \frac{\partial}{\partial z} (RB_\phi) = -\frac{1}{R} \frac{\partial F}{\partial z}$$

$$\begin{aligned} \mu_0 \vec{j} &= \hat{R} \mu_0 j_R + \hat{\phi} \mu_0 j_\phi + \hat{z} \mu_0 j_z = \hat{R} \left(-\frac{1}{R} \frac{\partial F}{\partial z} \right) + \hat{\phi} \left(-\frac{1}{R} \Delta^* \psi \right) + \hat{z} \left(\frac{1}{R} \frac{\partial F}{\partial R} \right) \\ &\equiv \left(\frac{\nabla F}{R} \right) \times \hat{\phi} + \left(-\frac{1}{R} \Delta^* \psi \right) \hat{\phi} \end{aligned}$$

$$\begin{aligned} I_P &= \int \vec{j}_P \cdot d\vec{S} = - \int_0^{2\pi} d\phi \int_0^{R_b} dR R j_z(R, 0) \\ &= -2\pi \int_0^{R_b} dR R \frac{1}{R} \frac{\partial F(R, 0)}{\partial R} = -2\pi F(\psi) \end{aligned}$$



Plasma condition can be obtained by solving Grad-Shafranov equation



$$\Delta^* \psi = -\mu_0 R^2 \frac{dp}{d\psi} - \frac{1}{2} \frac{dF^2}{d\psi} \quad \text{where } \Delta^* \psi = R^2 \nabla \cdot \left(\frac{\nabla \psi}{R^2} \right)$$

- The usual strategy to solve the Grad-Shafranov equation:
 1. Specify two free functions, the plasma pressure $p = p(\psi)$ and the toroidal field function $F = F(\psi)$.
 2. Solve the equation with specified boundary conditions to determine the flux function $\psi(R, z)$.
 3. Calculation the magnetic field using the following equations:

$$B_R = -\frac{1}{R} \frac{\partial \psi}{\partial z} \quad B_\phi = \frac{F(\psi)}{R} \quad B_z = \frac{1}{R} \frac{\partial \psi}{\partial R}$$

4. The pressure profile can then be obtained from $p = p(\psi(R, z))$.

Example of the analytical solution of the Grad-Shafranov equation



$$\Delta^* \psi = -\mu_0 R^2 \frac{dp}{d\psi} - \frac{1}{2} \frac{dF^2}{d\psi}$$

• For $\mu_0 \frac{dp}{d\psi} = -C_2$ $\frac{1}{2} \frac{dF^2}{d\psi} = C_1$

$$\psi(R, z) = -\frac{C_1}{2} z^2 + \frac{C_2}{8} R^4 + C_3 + C_4 R^2 + C_5 (R^4 - 4R^2 z^2)$$

$$C_1 = 1$$

$$C_2 = -8$$

$$C_3 = -20$$

$$C_4 = 20$$

$$C_5 = 0.2$$

$$B_R(R, z) = -\frac{1}{R} (-C_1 z - 8C_5 R^2 z) \quad B_z(R, z) = \frac{1}{R} \left(\frac{C_2}{2} R^3 + 2C_4 R + C_5 (4R^3 - 8Rz^2) \right)$$

