

Pulsed Power system

Prerequisite courses:

Electric Circuits.

Engineering Mathematics / Phys Mathematics (ODE)

① x Po-Yu Chang 張博宇
pchang@mail.ncku.edu.tw.

#1: 65916

② x No office hour, please feel free to stop by my office whenever my door is open & nobody is in my office. Or you may email me to schedule a meeting.

③ x class time : 9:10 ~ 12:00 ²⁰¹⁶ English
→ 9:10 ~ 11:30 ~~class~~ with 10 mins break
11:30 ~ 12:00 ²⁰¹⁷ ~~class~~ Mandarin for ~~pr~~

④ x Assignments : 70% → No roll call.
Presentations : 30%
Pulsed Power by Gennady A. Mesyats.
Foundations of Pulsed Power Technology by Jane Lehr & Prathap Kon

⑤ x References: Pulsed power systems by H. Bluhm.
Circuits analysis by Cunningham and Stuller
Pulse power technology by Richard J. Adler

x Additional References:
→ Pulsed Power by Gennady A. Mesyats
J. C. Martin on Pulsed Power

* Class material: myweb.ncku.edu.tw/~pchang

* Course Outline:

- Introduction to pulsed-power system. - (9/14) → 9/21 ^{p2} 9/12 2018
- Review of circuit analysis - 9/21. ^{9/12} 2018 HW. of KCC circuit

72. Static and dynamic breakdown strength of dielectric material. - (9/28, 10/5) ^{9/19} 2018 ^{9/26} 2018
 → avalanche, townsend condition, Paschen Law.
 * HW?
 [Gas.
 [Liquid
 [Solid.

73 Energy storage. (10/12 - 10/19) ²⁰¹⁷ (10/3, 10/17) ²⁰¹⁸
 [pulsed discharge capacitors
 [Marx Generators. → HW. of explory Max
 [Inductive energy storage. (10/20, 10/27) ²⁰¹⁸

74 Switches. 10/26 - ~~11/2~~ 11/9 ²⁰¹⁷ → calculate capacitor sizing & Paschen's eq.
 [Closing switches → gas switches
 [Opening switches →

75 Pulse-forming networks ~~11/9~~; ~~11/16~~ 11/23 ^{11/10} 11/21 ²⁰¹⁸
 [Transmission lines
 [RLC networks

76 Pulse transmission and transformation ~~11/23~~ ^{11/30} 12/1 ²⁰¹⁸
 [self-magnetic insulation in vacuum lines
 [pulse transformers
 [High voltage power supply
 [Transformation lines ^{11/28, 12/5} 2018

77. Power and voltage adding

~~12/14~~ 12/14 12/20
2017 2018

- Addng of power
- voltage adding

79.

Diagnostics

12/21, 12/28, 12/29, 12/26
2017 2018

- Electromagnetic - Field sensors
 - Capacitive sensor
 - Inductive
- Current-viewing resistors (CURS)
- Current measurements based on Faraday Effect.
- E-field - - - - - Electro-optic effects.
- Magnetic ion energy analysers
- Vacuum voltage monitors.

710. Applications of pulsed-power system

1/4 1/2
2017 2018

78

7 Introduction to pulsed-power system 24

* Pulsed power is a scheme where stored energy is discharged as electrical energy into a load in a short pulse or ~~as~~ short pulses with a controllable repetition rate.

~ Example of pulsed power in daily life:

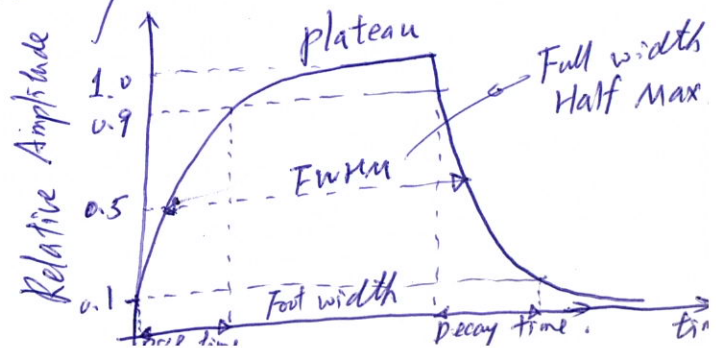
- Driven piles
- Hammer.
- making ~~sticky~~ rice cake. → great example of short pulses with a controllable repetition rate

* Pulsed power in general: $P \sim 10^9 \text{ W (1 GW)}$
 $E \gtrsim \text{kJ}$

The highest energy and power that have been achieved in a single pulse are in the order of 100 MJ & few hundred TW, respectively.

- $V: 10 \text{ kV} \sim 50 \text{ MV}$
- $I: 1 \text{ kA} \sim 10 \text{ MA.}$

* A pulse is characterised by its shape, i.e., by its rise & fall times and by the duration and flatness of its plateau region



- Pulse rise time - the time it takes the voltage to rise from 10% to 90%. PS

- Pulse } fall time - - - - - fall
 } decay 90% to 10%.

- Both the fall and the rise time of a pulse depend on the evolution of the "Load impedance," which in most cases varies with time.

- pulse duration - no unique definition.

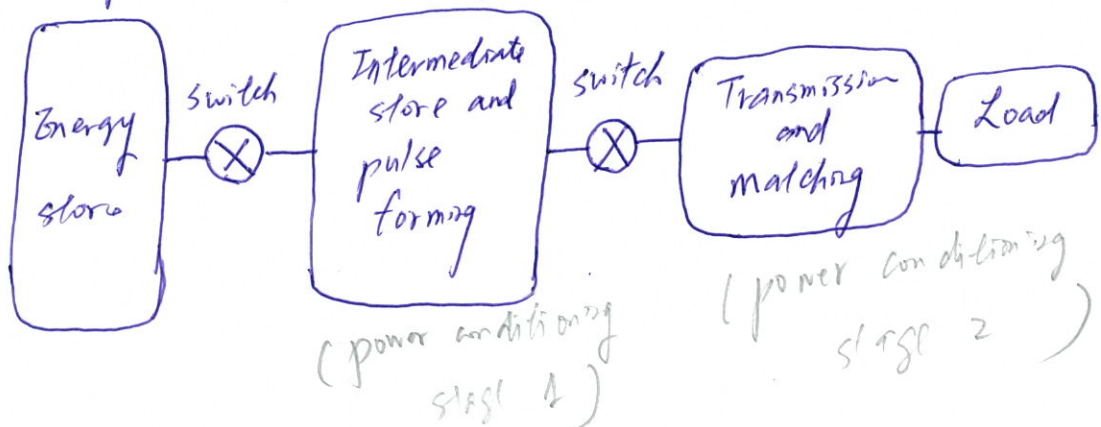
↳ FWHM

⊙ ~~Sometimes~~ It is defined as the duration at 90% of the peak amplitude.

⊙ Flatness of the plateau region is an important requirement for driving some ~~low~~ loads, such as Pocket cells.

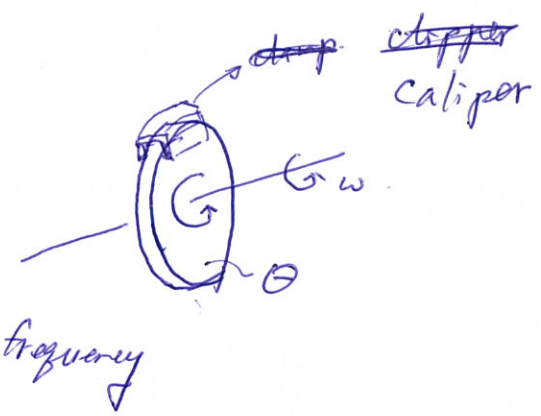
- A ~~general~~ generator scheme for the production of high-power electrical pulses is always based on an energy store that is charged slowly at a relatively low charging power and ~~is~~ is discharged rapidly by acting a switch.

- To achieve the desired power magnification factor and to shape the pulse, the above process can be repeated several times.



* The energy can be stored either chemically, mechanically, Pb. or electrically.

↳ Mechanical energy:



$$W_{kin} = \frac{1}{2} \Theta \omega^2$$

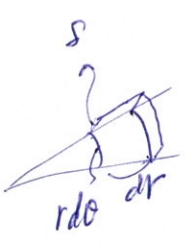
↑ moment of inertia
↙ angular frequency

For a massive cylinder: $\Theta = \frac{1}{2} M R^2$
 ↑ mass ↙ radius

$$\Rightarrow W_{kin} = \frac{1}{2} \cdot \frac{1}{2} M R^2 \cdot \omega^2$$

⇒ Stored energy density: $\omega = \frac{W_{kin}}{M} = \frac{1}{4} R^2 \omega^2$

- The ultimate energy density is limited by the tensile strength of the material used to construct the rotor.



$$d\Sigma = \frac{dF}{A} = \frac{(r d\theta s dr \rho) \cdot r \omega^2}{r d\theta \cdot s} = \rho \omega^2 r dr$$

$$\Sigma = \int_0^R \rho \omega^2 r dr = \frac{1}{2} \rho \omega^2 R^2$$

$$\Sigma = \rho \omega^2 r dr$$

↑ tensile strength

$$\Sigma = \int_0^R \rho \omega_{max}^2 \frac{r^2}{2} dr$$

for a stainless steel cylinder or radius 1m.

$\omega_{max} = \frac{400}{300}$ sec. AISI 302 stainless steel

$\Sigma = 520 / 860$ MPa
 ↑ yield strength ↑ ultimate tensile strength.

$$\rho = 8.19 \text{ g/cm}^3 = 8190 \text{ kg/m}^3$$

$$\omega \sim \sqrt{\frac{\Sigma}{\rho r^2}} = \sqrt{\frac{2 \cdot 860 \times 10^6}{8190 \cdot 1}} = 458 \sim 400 \text{ /sec}$$

$$\omega_{kin} = \frac{1}{4} R^2 \omega^2 = \frac{1}{4} \cdot 1^2 \cdot \left(\frac{400}{300}\right)^2 = 4 \times 10^4 \text{ J/kg}$$

high strength alloy ASTM A514 steel

$\rho = 7.8 \text{ g/cm}^3$ $\Sigma = 690 / 760$ MPa
 ↑ yield strength ↑ ultimate tensile strength.

$$\omega = \sqrt{\frac{2 \cdot 690 \times 10^6}{7800 \cdot 1^2}} = 420 \sim 400 \text{ /sec}$$

$$W_{kin} = \frac{1}{4} R^2 \omega^2 = \frac{1}{4} \cdot 1 \cdot 400^2 = 4 \times 10^4 \text{ J/kg} = 3.1 \times 10^8 \text{ J/m}^3$$

- The problem with mechanical storage is to release the energy in a sufficiently short time. p7

→ Several electrical compression stages are needed in combination with the mechanical storage to achieve the desired power level.

Ex: Electrical energy can be stored either capacitively in an electric field or inductively in a magnetic field.

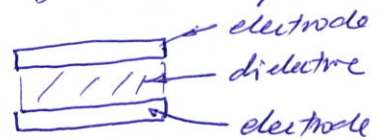
Ex1: Electric field:

$$W_e = \frac{1}{2} \epsilon \cdot \epsilon_0 E^2$$

for oil impregnated paper: $\epsilon = 6$, breakdown strength $E = 0.78 \times 10^8 \text{ V/m}$

$$\Rightarrow W_e = \frac{1}{2} \times 6 \times 8.85 \times 10^{-12} \cdot (0.78 \times 10^8)^2 = 161 \text{ kJ/m}^3$$

With the finite packing density:



$$E \quad \text{or} \quad W_e = \frac{1}{2} C V^2, \quad C = \epsilon \epsilon_0 \frac{A}{d}$$

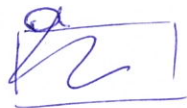
$\Rightarrow d \uparrow, \epsilon_0 \uparrow \rightarrow$ space is ~~not~~ occupied by the electrode.

\Rightarrow ~~can~~ to estimate the energy storage in space

$$W_e' \approx \frac{1}{2} \times W_e \approx 80 \text{ kJ/m}^3$$

Ex2: Magnetic field:

$$W_B = \frac{1}{2} \mu_0 \mu_r \frac{B^2}{2\mu_0}$$



The maximum energy density is limited by the onset of melting at the conductor surface or by the mechanical strengths of the storage inductor.

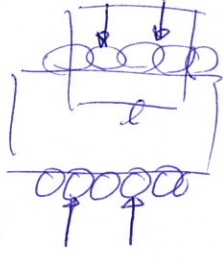
$$C_p \cdot \rho \cdot T = \frac{B^2}{2\mu_0} \cdot \rho \cdot \frac{1}{\rho} \text{ kJ/m}^3$$

↑ heat capacitor per unit mass
 ↑ mass density
 ↑ surface temperature

→ a factor of order unity depending on the form of the pulse

$$B \cdot l = \mu_0 N I$$

$$\Rightarrow B = \mu_0 n I \propto I$$



$$E = P \cdot t = I^2 \cdot R \cdot t \propto B^2 \cdot R \cdot t$$

$$\Rightarrow C_v \rho T = \frac{1}{2\mu_0} B^2 \cdot l \approx \frac{B^2}{2\mu_0} \quad \text{take } l = 1$$

$$B^2 \approx \sqrt{2\mu_0 \cdot C_v \cdot \rho \cdot T} = \sqrt{2 \times 4\pi \times 10^{-7} \times \frac{0.385 \text{ J}}{10^3 \text{ kg} \cdot \text{K}} \times 8960 \cdot (1085 - 25)}$$

Copper: $C_v = 0.385 \text{ J/g} \cdot \text{K}$ $= 96 \text{ T} \approx 100 \text{ T}$

melting: $T = 1085^\circ \text{C}$

$$\rho = 8.96 \text{ g/cm}^3 = 8960 \text{ kg/m}^3$$

$P_B \leq \Sigma$ - yield strength $\Sigma = 70 \text{ MPa}$ for Cu

$$\Rightarrow \frac{B^2}{2\mu_0} \leq \Sigma \Rightarrow B \leq \sqrt{2\mu_0 \Sigma} = \sqrt{2 \times 4\pi \times 10^{-7} \times 70 \times 10^6} = 13 \text{ T}$$

~~$W_B = \frac{1}{2} \mu_0 n^2 B^2 = \frac{1}{2} \times 4\pi \times 10^{-7} \Rightarrow W_B = \frac{1}{2} \frac{B^2}{\mu_0}$~~

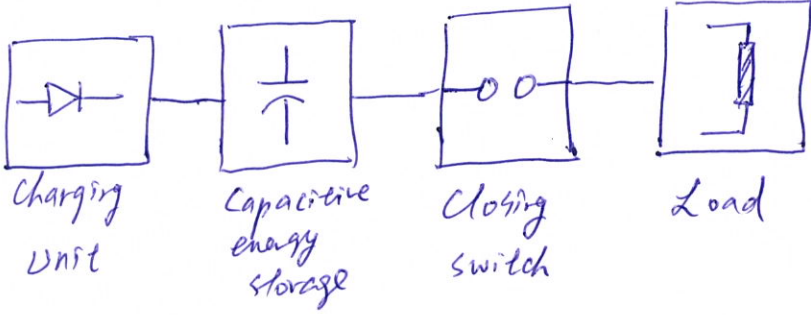
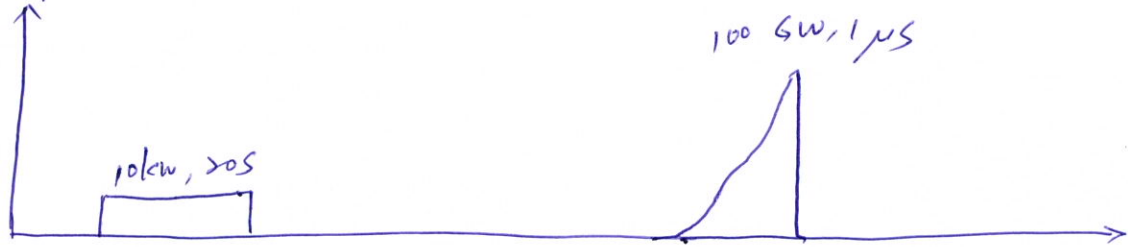
~~$W_B = \frac{1}{2} \mu_0 B^2 = \frac{1}{2}$~~ $= \frac{1}{2} \frac{13^2}{4\pi \times 10^{-7}} = 6.7 \times 10^7 \text{ J/m}^3$

$= 67000 \text{ kJ/m}^3$

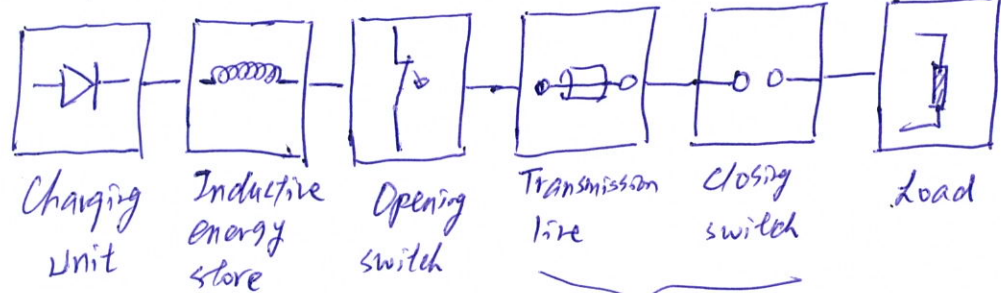
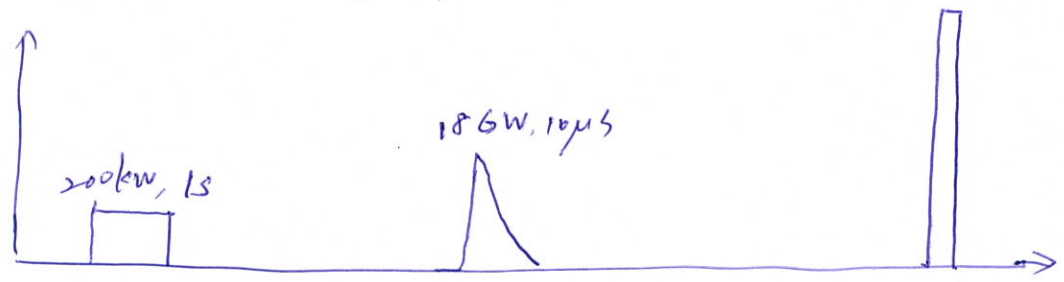
\Rightarrow The energy density stored in a magnetic field can be about 2 orders of magnitude higher than that storable in an electric field!!

- * Capacitive storage - requires one or more closing switches which remain open during charging and hold the charging voltage.
- power multiplication is done by current amplification.
- * Inductive storage - requires an opening switch which is closed during charge-up, carrying a large current at this stage.
- power multiplication is done by voltage amplification.

Capacitive storage $w_e = 10 - 50 \text{ kJ/m}^3$

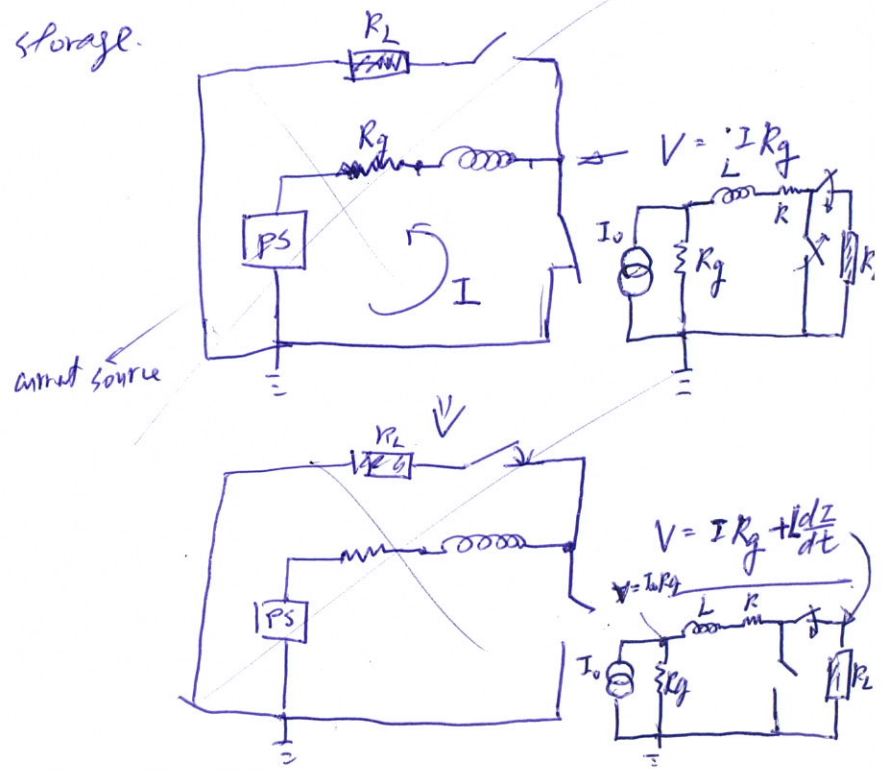
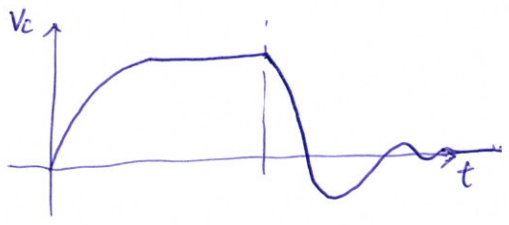
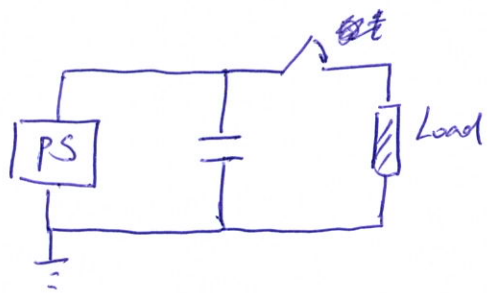


Inductive storage $w_m = 1 - 50 \text{ MJ/m}^3$



1. Compressing stage
2. Compressing stage (pulse forming line)

Example of Capacitive storage.



Review of circuit analysis

P10

* Kirchhoff's Current Law

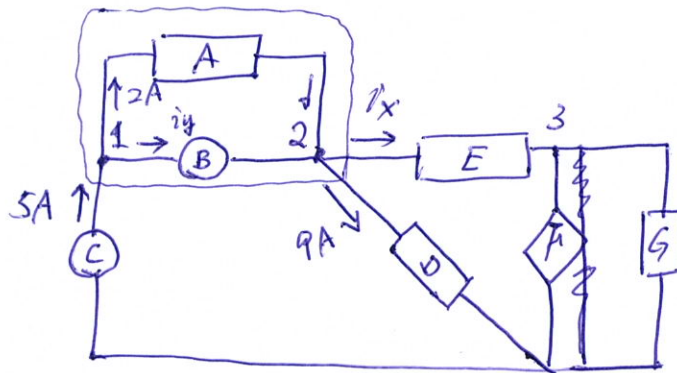
- At any instant in time, the algebraic sum of all currents leaving any closed surface is zero

$$i_1 + i_2 + \dots + i_N = 0,$$

or in abbreviated notation:

$$\sum_{k=1}^N i_k = 0$$

where i_k is the k^{th} current of the N currents leaving the closed surfaces.



$$\begin{aligned} i_y + 2 - 5 &= 0 \\ \Rightarrow i_y &= 3 \text{ (A)} \\ -5 + i_x + 9 &= 0 \\ \Rightarrow i_x &= -4 \text{ (A)} \end{aligned}$$

* Kirchhoff's Voltage Law

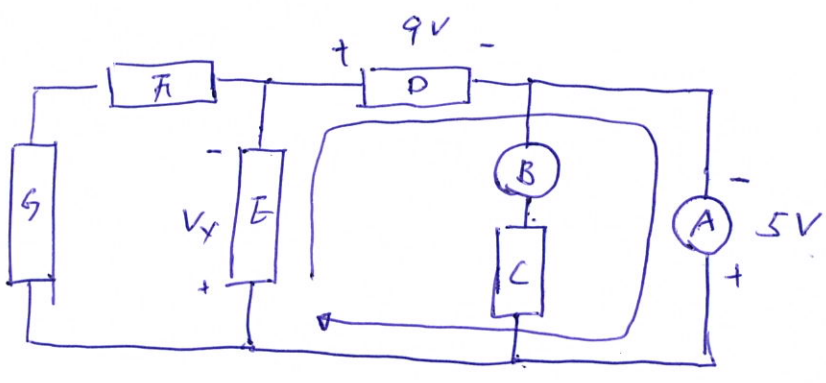
- At any instant in time, the algebraic sum of all voltage drops taken around any closed path is 0:

$$V_1 + V_2 + \dots + V_N = 0.$$

or in abbreviated notation:

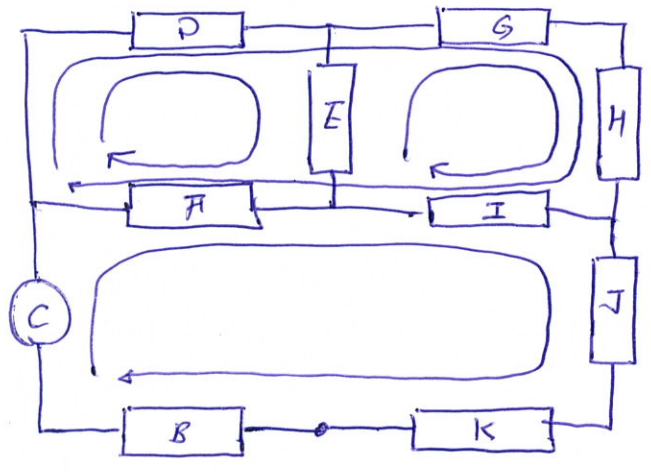
$$\sum_{k=1}^N V_k = 0$$

where V_k is the voltage drop, taken in the direction of the path along the k^{th} segment of the N segments in the closed path.

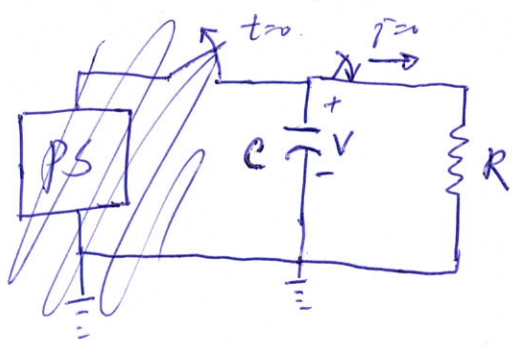


$$-V_x - 9 + 5 = 0 \Rightarrow \underline{V_x = -4 \text{ V}}$$

* Loops, Meshes, and Planar Networks



* Source-free RC circuit.



* ~~Assuming~~
 ⇒ Assuming that the capacitor is fully charged to V_0 .
 At $t=0$, the switch is opened

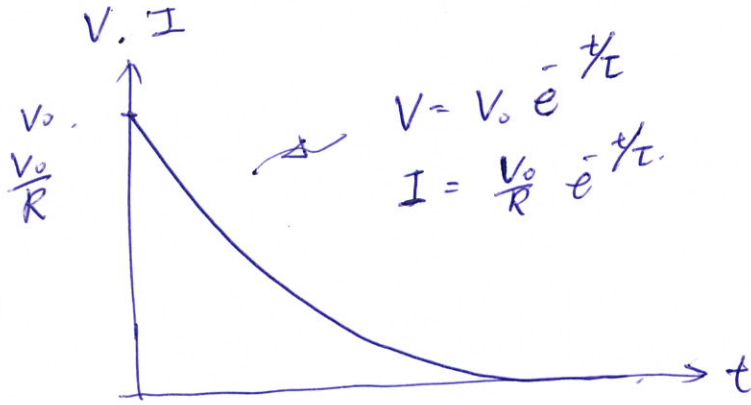
$$V_c - IR = 0 \quad I = \frac{dQ}{dt} = -C \frac{dV}{dt} \quad C = \frac{Q}{V}$$

$$\Rightarrow V_c + RC \frac{dV}{dt} = 0 \quad \text{or} \quad \frac{dV}{dt} + \frac{1}{RC} V = 0$$

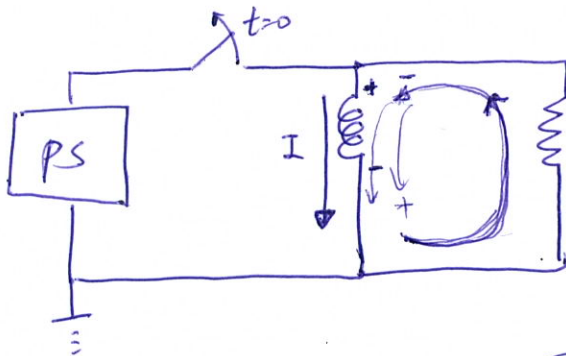
$$\Rightarrow \int \frac{dV}{V} = -\frac{1}{RC} \int dt \Rightarrow \ln \frac{V(t)}{V(0)} = -\frac{t}{RC}$$

$$\Rightarrow V(t) = V_0 e^{-\frac{t}{RC}} = \frac{V_0 e^{-\frac{t}{RC}}}{1} \quad \tau_c = RC$$

$$I = -C \frac{dV}{dt} = +V_0 C \left(+\frac{1}{\tau} \right) e^{-\frac{t}{\tau}} = \frac{V_0}{R} e^{-\frac{t}{\tau}}$$



* Source-free RL circuit



* Assuming the current is at steady state for $t \leq 0$, $I(0) = I_0$
At $t=0$, the switch is opened

~~$V_L = IR + V_L = 0 \Rightarrow V_L = L \frac{dI}{dt}$~~

$-IR - V_L = 0 \quad V_L = L \frac{dI}{dt}$

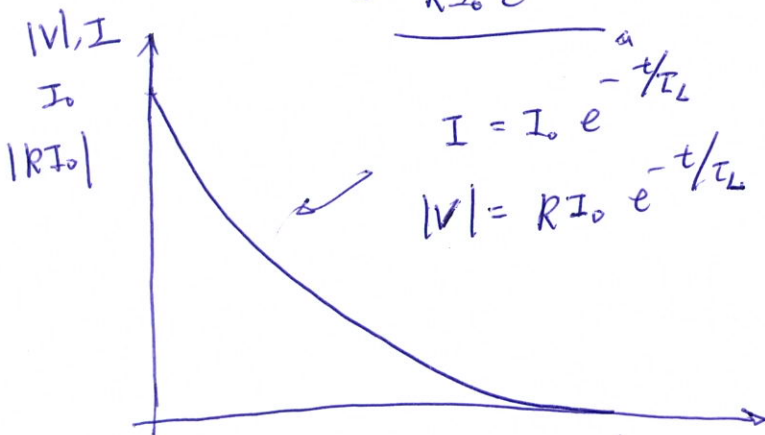
$\Rightarrow IR + L \frac{dI}{dt} = 0 \quad \Rightarrow \frac{dI}{dt} + \frac{R}{L} I = 0$

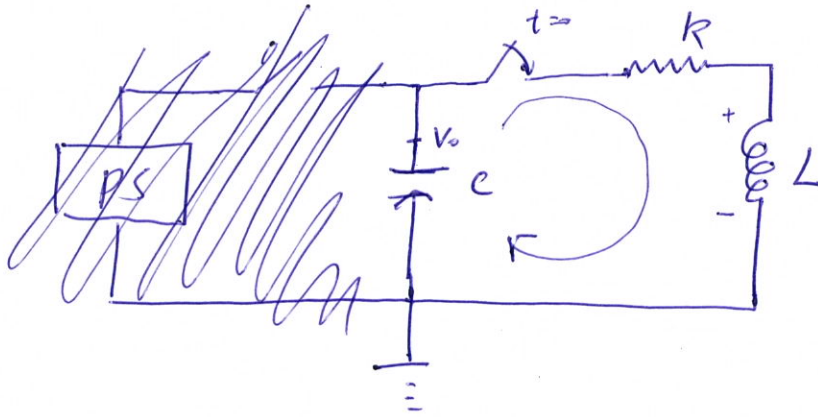
$\Rightarrow \int \frac{dI}{I} = -\frac{R}{L} \int dt \quad \Rightarrow \ln \frac{I(t)}{I(0)} = -\frac{R}{L} t = -\frac{t}{\tau_L} \quad \tau_L = \frac{L}{R}$

$\Rightarrow I(t) = I_0 e^{-\frac{R}{L} t} = I_0 e^{-\frac{t}{\tau_L}}$

$V(t) = L \frac{dI}{dt} = L \cdot I_0 \cdot \left(-\frac{1}{\tau_L}\right) e^{-\frac{t}{\tau_L}}$

$= -RI_0 e^{-\frac{t}{\tau_L}}$





Assuming that the capacitor is fully charged to V_0 , $I(0) = 0$
 At $t=0$, the switch is opened,

$$V_0 - IR - L \frac{dI}{dt} = 0 \quad I = \frac{dQ}{dt} = -C \frac{dV}{dt}$$

$$\Rightarrow V + RC \frac{dV}{dt} + LC \frac{d^2V}{dt^2} = 0$$

$$\frac{d^2V}{dt^2} + \frac{R}{L} \frac{dV}{dt} + \frac{1}{LC} V = 0$$

$$D^2 + \frac{R}{L} D + \frac{1}{LC} = 0 \quad \Rightarrow D = \frac{-\frac{R}{L} \pm \sqrt{\left(\frac{R}{L}\right)^2 - \frac{4}{LC}}}{2}$$

$$\Rightarrow V = e^{-\frac{R}{2L}t} \left(\alpha e^{\sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}t} + \beta e^{-\sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}t} \right)$$

$$1) \left(\frac{R}{2L}\right)^2 - \frac{1}{LC} < 0 \quad \Rightarrow V = e^{-\frac{R}{2L}t} \left(\alpha e^{i\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t} + \beta e^{-i\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t} \right)$$

$$= e^{-\frac{R}{2L}t} \left[\alpha \cos\left(\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t\right) + \beta \sin\left(\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t\right) \right]$$

$$V(t=0) = V_0 = \alpha$$

$$\Rightarrow V = V_0 e^{-\frac{R}{2L}t} \cos\left(\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t\right)$$

$$V = V_0 e^{-\frac{R}{2L}t} \left[\cos\left(\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t\right) + \beta \sin\left(\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t\right) \right]$$

$$I = -C \frac{dV}{dt} = -C \left\{ -\frac{R}{2L} e^{-\frac{R}{2L}t} \left[V_0 \cos(\sqrt{\dots}t) + \beta \sin(\sqrt{\dots}t) \right] + e^{-\frac{R}{2L}t} \left[-\sqrt{\dots} V_0 \sin(\sqrt{\dots}t) + \sqrt{\dots} \beta \cos(\sqrt{\dots}t) \right] \right\} \quad P14$$

$$I(0) = 0 = -C \left\{ -\frac{R}{2L} V_0 + \sqrt{\dots} \beta \right\}$$

$$\Rightarrow \beta = \frac{R}{2L} V_0 \cdot \frac{1}{\sqrt{\dots}} = V_0 \frac{R/2L}{\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}}$$

$$= \frac{V_0}{\sqrt{\frac{4L^2}{R^2} \cdot \frac{1}{LC} - 1}} = \frac{V_0}{\sqrt{\frac{4L}{R^2 C} - 1}}$$

$$V(t) = V_0 e^{-\frac{R}{2L}t} \left[\cos\left(\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t\right) + \frac{R/2L}{\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}} \sin\left(\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t\right) \right]$$

~~$$I(t) = -C \left\{ -\frac{R}{2L} e^{-\frac{R}{2L}t} \left[V_0 \cos(\sqrt{\dots}t) + \beta \sin(\sqrt{\dots}t) \right] + e^{-\frac{R}{2L}t} \left[-\sqrt{\dots} V_0 \sin(\sqrt{\dots}t) + \sqrt{\dots} \beta \cos(\sqrt{\dots}t) \right] \right\}$$~~

$$I(t) = -C \left\{ -\frac{R}{2L} e^{-\frac{R}{2L}t} \left[V_0 \cos(\sqrt{\dots}t) + \frac{V_0 \cdot R/2L}{\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}} \sin(\sqrt{\dots}t) \right] + e^{-\frac{R}{2L}t} \left[-\sqrt{\dots} V_0 \sin(\sqrt{\dots}t) + \sqrt{\dots} \frac{V_0 \cdot R/2L}{\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}} \cos(\sqrt{\dots}t) \right] \right\}$$

$$= -C V_0 e^{-\frac{R}{2L}t} \left\{ \left(-\frac{R}{2L} V_0 + V_0 \frac{R}{2L} \right) \cos(\sqrt{\dots}t) - \left(\frac{(R/2L)^2}{\sqrt{\dots}} + \sqrt{\dots} \right) \sin(\sqrt{\dots}t) \right\}$$

$$= +C V_0 e^{-\frac{R}{2L}t} \frac{\frac{(R/2L)^2}{\sqrt{\dots}} + \sqrt{\dots}}{\sqrt{\dots}} \sin(\sqrt{\dots}t)$$

$$= \frac{V_0}{L} \frac{1}{\sqrt{\left(\frac{1}{LC}\right) - \left(\frac{R}{2L}\right)^2}} e^{-\frac{R}{2L}t} \sin(\sqrt{\dots}t) = \frac{V_0}{\sqrt{\frac{4}{C} - \left(\frac{R}{2}\right)^2}} e^{-\frac{R}{2L}t} \sin\left(\sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2}t\right)$$

$$\begin{aligned}
 i(t) &= -\frac{V_0}{2} e^{-\frac{R}{2L}t} \left\{ \left(1 + \frac{R/2L}{\sqrt{\dots}}\right) \left(\sqrt{-\frac{R}{2L}}\right) e^{\sqrt{\dots}t} - \left(1 - \frac{R/2L}{\sqrt{\dots}}\right) \left(\sqrt{+\frac{R}{2L}}\right) e^{-\sqrt{\dots}t} \right\} \\
 &= -\frac{CV_0}{2} e^{-\frac{R}{2L}t} \left\{ \frac{(\sqrt{\dots})^2 - (R/2L)^2}{\sqrt{\dots}} e^{\sqrt{\dots}t} - \frac{\sqrt{\dots}^2 - (R/2L)^2}{\sqrt{\dots}} e^{-\sqrt{\dots}t} \right\}
 \end{aligned}$$

~~$$= -\frac{V_0}{2} \frac{e^{-\frac{R}{2L}t}}{\sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}}} \left[\frac{1}{L} e^{\sqrt{\dots}t} - \dots \right]$$~~

$$= \frac{V_0}{2} e^{-\frac{R}{2L}t} \cdot \frac{+1/L}{\sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}}} \left[e^{\sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}}t} - e^{-\sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}}t} \right]$$

$$= V_0 e^{-\frac{R}{2L}t} \frac{1}{\sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}}} \left[\frac{e^{\sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}}t} - e^{-\sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}}t}}{2} \right]$$

$$= \frac{V_0}{\sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}}} e^{-\frac{R}{2L}t} \sinh\left(\sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}}t\right)$$

Plot 3 conditions !!

$$2) \left(\frac{R}{2L}\right)^2 - \frac{1}{LC} = 0 \Rightarrow D = -\frac{R}{2L}$$

$$V = (\alpha + \beta t) e^{-\frac{R}{2L}t}$$

$$V(t=0) = V_0 = \alpha \Rightarrow V = (V_0 + \beta t) e^{-\frac{R}{2L}t}$$

$$I(t) = -c \frac{dV}{dt} = -c \left[\beta e^{-\frac{R}{2L}t} - \frac{R}{2L} (V_0 + \beta t) e^{-\frac{R}{2L}t} \right]$$

$$I(t=0) = 0 = -c \left[\beta - \frac{R}{2L} V_0 \right] = 0 \Rightarrow \beta = \frac{R}{2L} V_0$$

$$\Rightarrow V = \left(V_0 + \frac{R}{2L} V_0 t \right) e^{-\frac{R}{2L}t} = V_0 \left(1 + \frac{R}{2L} t \right) e^{-\frac{R}{2L}t}$$

$$I = -c \frac{dV}{dt} = -c \left[\frac{R}{2L} V_0 e^{-\frac{R}{2L}t} - \frac{R}{2L} V_0 e^{-\frac{R}{2L}t} - \frac{R}{2L} \cdot \frac{R}{2L} V_0 t e^{-\frac{R}{2L}t} \right]$$

$$= c \cdot \left(\frac{R}{2L}\right)^2 V_0 t e^{-\frac{R}{2L}t} = c \cdot \frac{1}{4L} V_0 t e^{-\frac{R}{2L}t}$$

$$= \frac{V_0}{L} \cdot t \cdot e^{-\frac{R}{2L}t}$$

-----> η

$$3) \left(\frac{R}{2L}\right)^2 - \frac{1}{LC} > 0$$

$$V = e^{-\frac{R}{2L}t} \left(\alpha e^{\sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}} t} + \beta e^{-\sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}} t} \right)$$

~~$$= e^{-\frac{R}{2L}t} \left(\alpha \cosh\left(\sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}} t\right) + \beta \sinh\left(\sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}} t\right) \right)$$~~

$$V(t=0) = V_0 = \alpha + \beta$$

$$I = -c \frac{dV}{dt} = -c \left\{ -\frac{R}{2L} e^{-\frac{R}{2L}t} \left[\alpha e^{\sqrt{\dots} t} + \beta e^{-\sqrt{\dots} t} \right] + e^{-\frac{R}{2L}t} \left[\alpha \sqrt{\dots} e^{\sqrt{\dots} t} - \beta \sqrt{\dots} e^{-\sqrt{\dots} t} \right] \right\}$$

Dre

$$I(t=0) = 0 = -e \left\{ -\frac{R}{2L} [\alpha + \beta] + (\alpha\sqrt{-} - \beta\sqrt{-}) \right\} = 0 \quad P16$$

$$\Rightarrow \left(\sqrt{-} - \frac{R}{2L} \right) \alpha - \left(\sqrt{-} + \frac{R}{2L} \right) \beta = 0$$

$$\Rightarrow \begin{cases} \alpha + \beta = V_0 \\ \left(\sqrt{-} - \frac{R}{2L} \right) \alpha - \left(\sqrt{-} + \frac{R}{2L} \right) \beta = 0 \end{cases} \Rightarrow \alpha = \frac{\sqrt{-} + \frac{R}{2L}}{\sqrt{-} - \frac{R}{2L}} \beta$$

$$\beta \left[1 + \frac{\sqrt{-} + \frac{R}{2L}}{\sqrt{-} - \frac{R}{2L}} \right] = V_0$$

$$\Rightarrow \beta = \frac{V_0}{2} \frac{\sqrt{-} - \frac{R}{2L}}{\sqrt{-}}$$

$$= \frac{V_0}{2} \left(1 - \frac{R/2L}{\sqrt{-}} \right)$$

$$\frac{\sqrt{-} - \frac{R}{2L} + \sqrt{-} + \frac{R}{2L}}{\sqrt{-} - \frac{R}{2L}} = \frac{2\sqrt{-}}{\sqrt{-} - \frac{R}{2L}}$$

$$\alpha = \frac{\sqrt{-} + \frac{R}{2L}}{\sqrt{-} - \frac{R}{2L}} \cdot \frac{V_0}{2} \frac{\sqrt{-} - \frac{R}{2L}}{\sqrt{-}} = \frac{V_0}{2} \frac{\sqrt{-} + \frac{R}{2L}}{\sqrt{-}} = \frac{V_0}{2} \left(1 + \frac{R/2L}{\sqrt{-}} \right)$$

$$= \frac{V_0}{2} \left(1 + \frac{R/2L}{\sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}} \right) = \frac{V_0}{2} \left(1 + \frac{1}{\sqrt{1 - \frac{4L}{R^2 C}}} \right)$$

$$= \frac{V_0}{2} \left(1 + \frac{1}{\sqrt{1 - \frac{4L}{R^2 C}}} \right)$$

$$\Rightarrow V(t) = e^{-\frac{R}{2L}t} \cdot \frac{V_0}{2} \left[\left(1 + \frac{1}{\sqrt{1 - \frac{4L}{R^2 C}}} \right) e^{+\sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}t} + \left(1 - \frac{1}{\sqrt{1 - \frac{4L}{R^2 C}}} \right) e^{-\sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}t} \right]$$

$$I(t) = -ce^{-\frac{R}{2L}t} \left\{ -\frac{R}{2L} [\alpha e^{\sqrt{-}t} + \beta e^{-\sqrt{-}t}] + \alpha\sqrt{-} e^{\sqrt{-}t} - \beta\sqrt{-} e^{-\sqrt{-}t} \right\}$$

$$= -ce^{-\frac{R}{2L}t} \left\{ \alpha \left(\sqrt{-} - \frac{R}{2L} \right) e^{\sqrt{-}t} - \beta \left(\sqrt{-} + \frac{R}{2L} \right) e^{-\sqrt{-}t} \right\}$$

72 Static and Dynamic Breakdown Strengths of Dielectric Materials

PI8

72.1 Introduction

* We will ~~start~~ talk about the gas, liquid, and solid dielectrics

* Dielectric substances serve both as "insulators" in generator components such as capacitors, HV transmission lines, & transformers, and as "working media" in switches.

* The properties of these devices are strongly depend on
[electric breakdown strength.
dielectric constant.

* The dielectric strength of an insulant can be defined as "the maximum field stress that the material can ~~with~~ withstand for a given time".

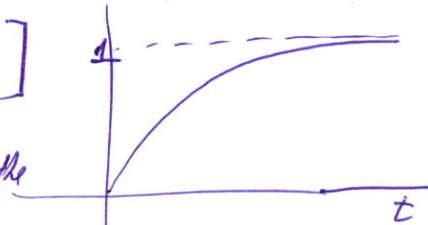
* Integrated field-time action:

failure probability: $\ln [1 - F(E, t)] = -\alpha \int_0^t E^b t^a dt$

$F(E, t)$: probability of ~~that~~ failure after time t .

$\alpha, a, b \rightarrow$ determined experimentally.

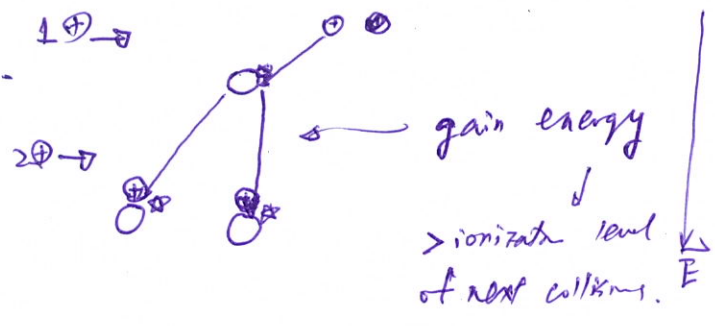
$$F(E, t) = 1 - \exp \left[-\alpha \int_0^t E^b t^a dt \right]$$



* Electric strength ~~is~~ also depends on the sample "geometry", "pressure", "temperature", and the "electrode material".

* At the microscopic level, breakdown requires the presence of sufficiently energetic charge particles that have acquired enough energy from the applied electric field between two energy-dissipating collisions to ionise the material and to create more charge particles.

stop



* In most cases, electrons dominate the breakdown process since the mobility is much larger than that of ions.

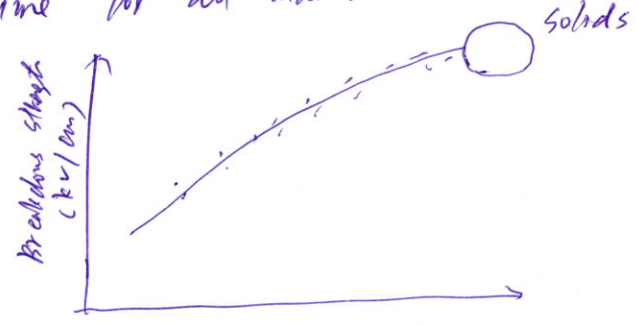
$$E_k = \frac{1}{2} m v^2 \Rightarrow v = \sqrt{\frac{2E_k}{m}} \Rightarrow s = vt \Rightarrow t = \frac{s}{v}$$

$$\Rightarrow t = \frac{s}{\sqrt{\frac{2E_k}{m}}} \sim \frac{s}{\sqrt{2E_k}} \sqrt{m} \quad n = \frac{\#}{V} \sim \frac{\#}{s^3} \Rightarrow s \sim n^{-1/3}$$

$$t \sim \frac{1}{n^{1/3}} \sqrt{m}$$

* In order for an electron to acquire enough energy between collisions, its mean free path in the material must be sufficiently large.

* Mean free path depends essentially on the density of the material, the electric breakdown strength should be the same for all materials with the same density.



- * Gaseous or liquid dielectric - self-repairing after a breakdown
- Solid dielectric - remains irreversibly destroyed.
- Liquid dielectric - preferred if large heat losses have to be removed

~~Gas~~ Gas

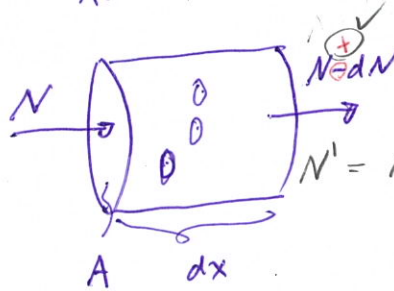
2.2 Gases

2.2.1 Static Breakdown.

* the electric strength of a gas is determined by the magnitude of its atomic and molecular reaction cross-sections for electron collisions. \rightarrow ionisation and attachment cross-sections.

σ : cross section of each atom.

n : # atom per unit volume have not collided on anything



= $n \cdot A \cdot dx$

total cross sect: $\sigma_{tot} = \sigma \cdot n \cdot A \cdot dx$

$N' = N - \Delta N < N$
 $\Delta N < 0$

probability of a particle causing an interaction in this layer: (dx)

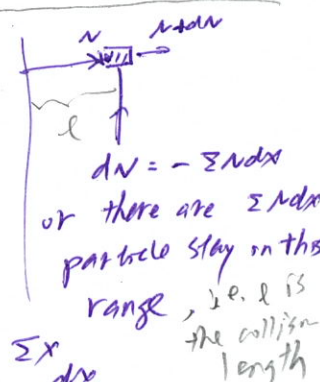
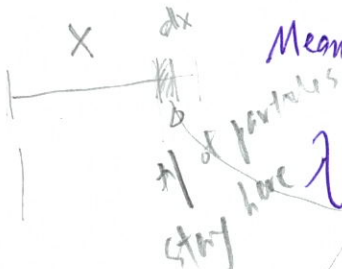
$$P = \frac{\sigma_{tot}}{A} = \frac{\sigma n A dx}{A} = \sigma n dx \equiv \sum dx$$

$$\Delta N = -N \cdot P = -N \sum dx \Rightarrow \frac{dN}{N} = -\sum dx$$

$$N(x) = N_0 e^{-\sum dx}$$

Mean free path - a particle can move without a collision is: average length of ~~the~~ that % of particles NOT colliding atoms \downarrow

$N' < N$, ...
% of collis. = $N P$
 $\Delta(N' - N) = N \sum dx$
 $\Delta N \Rightarrow -\Delta N = N \sum dx$
 $\frac{dN}{N} = -\sum dx$



$$\lambda = \frac{\int x dN'}{\int dN'} = \frac{1}{N_0} \int x \cdot \sum \cdot N(x) dx$$

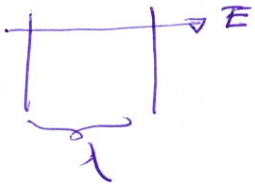
$$dN' = -dN = \sum N dx$$

$$u = x \quad du = e^{-\sum x} dx$$

$$du = dx \quad v = -\frac{1}{\sum} e^{-\sum x}$$

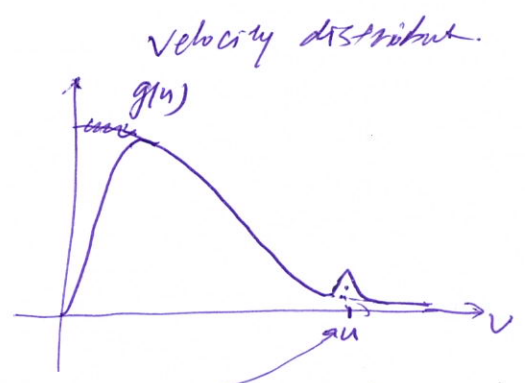
$$= \sum \left[-\frac{1}{\sum} x e^{-\sum x} \right]_0^\infty + \frac{1}{\sum} \int e^{-\sum x} dx = -\frac{1}{\sum} e^{-\sum x} \Big|_0^\infty = \frac{1}{\sum}$$

Between each collision, the kinetic energy increases:



$$\lambda \cdot eE = \frac{1}{2} m u^2$$

$$\Rightarrow u = \sqrt{\frac{2eE\lambda}{m}}$$



- Mean time between ionising collisions for electron with velocity u

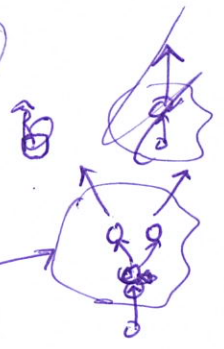
$\tau_i = \frac{\lambda_i}{u} \Rightarrow$ the rate of ionisation is:

$$\frac{1}{\tau_i} = \frac{u}{\lambda_i} = \sum \sigma_i u$$

to p=1a
showing drift cross section

of ionising collisions per second leading to growth of the swarm equilibrium velocity distribution function

$$\left\langle \frac{dN_e}{dt} \right\rangle = \int_0^{\infty} \frac{N_e \cdot g(u) \cdot du}{\tau} = N_e \int_0^{\infty} (\sum \sigma_i u) g(u) du$$



$$\frac{dN_e}{dt} = \frac{\partial N}{\partial t} + \frac{\partial x}{\partial t} \frac{\partial N}{\partial x} = \frac{\partial N}{\partial t} + u \frac{\partial N}{\partial x}$$

Assume that the swarm does not spread i.e. $\frac{\partial N}{\partial x} = 0 \rightarrow N(x,t) = N(x)$

and introduce a mean swarm velocity $\langle u \rangle$

$$\Rightarrow \frac{dN_e}{dt} = \frac{\partial N}{\partial t} + \langle u \rangle \frac{\partial N}{\partial x} \rightarrow \langle u \rangle \frac{\partial N}{\partial x} = N \int \sum \sigma_i u g(u) du$$

Mean swarm velocity $\langle u \rangle$:

$$\alpha = \frac{\int \sum \sigma_i(u) \cdot u \cdot g(u) du}{\int \sum \sigma_i(u) \cdot g(u) du}$$

& assume $\frac{\partial N}{\partial x} = N \alpha$

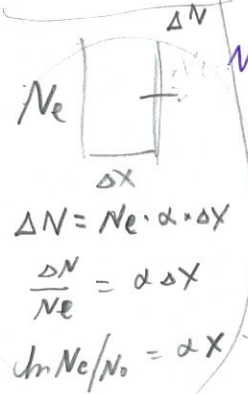
α : ionisation coefficient, # of ionisation events performed by an electron in a unit length

$$\Rightarrow N_e(x) = N_0 \exp(\alpha x)$$

Notice that $\frac{\alpha}{p}$ is a unique function of $\frac{E}{p}$, where p is the gas pressure under normal conditions.

$$\frac{\alpha}{p} = F\left(\frac{E}{p}\right)$$

☆ come back after p=1e



the same @ p=1e

σ cross section \rightarrow collisional cross section:

- elastic collisions - NO energy exchanges
Momentum is redistributed.

- inelastic collisions - energy exchanged between the collision partners
 \rightarrow production of molecules & particles

\rightarrow * Elastic collisions:

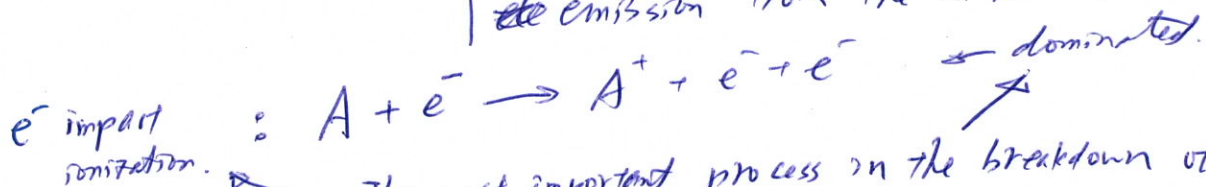


* Inelastic collisions: a portion of the kinetic energy before collision is converted to potential energy of one of the particles in the system.



The process of ionization is dominated by e^- acceleration in an electric field and is greatly aided by the appearance of ionization electrons.

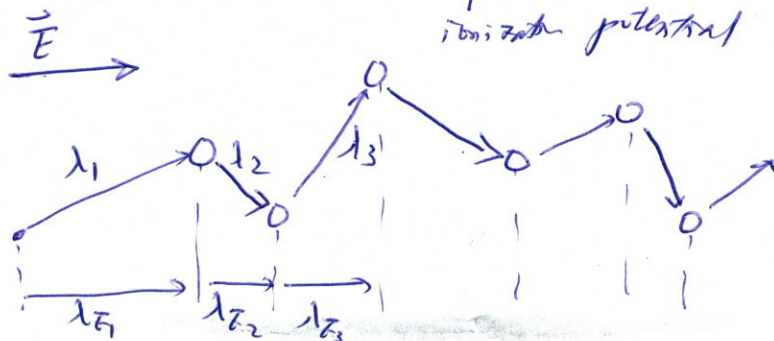
electrons $\left\{ \begin{array}{l} \text{ionization in the gas.} \\ \text{electron emission from the cathode.} \end{array} \right.$



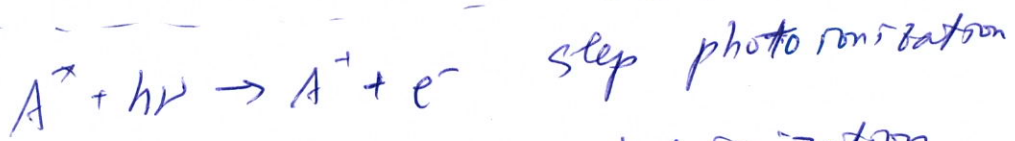
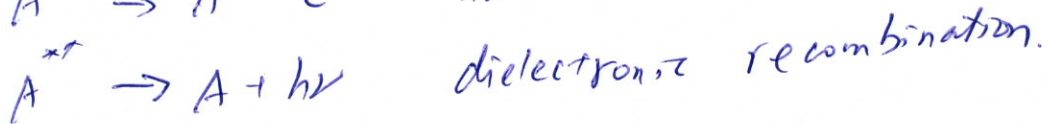
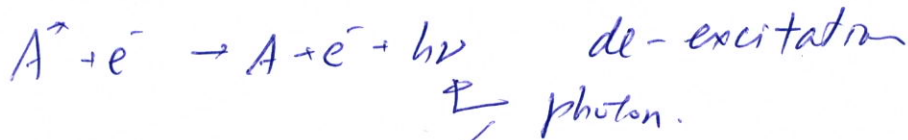
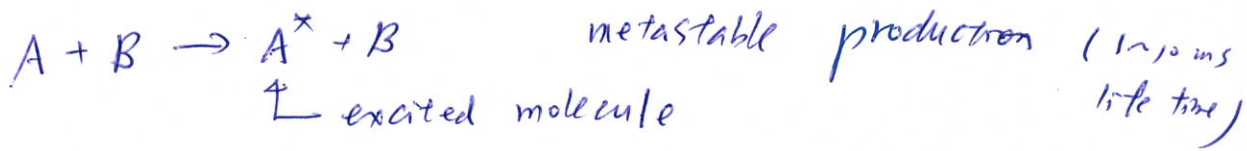
The most important process in the breakdown of gases but is not sufficient alone to result in breakdown.

$$q_e \cdot E \cdot \lambda_{Ei} \geq q_e V_i$$
 \leftarrow requirement.

\uparrow
ionization potential



• Photoionization & collisions w/ excited molecules p21 b



photoionization is very complex:

$h\nu$ w/ $\lambda = 125 \text{ nm (UV)}$ \odot 9.9 eV can ionize almost all gases despite that almost all molecules & atom have ionization energy $> 9.9 \text{ eV}$. !!

- dust or water vapor \rightarrow emit e^- through ~~phr~~ ^{absorber}
- All photoionization occurs between 6 ~ 50 eV

→ Penning ionization:

p. 10



- May be from impurities or Engineered mixture → Penning mixture

A Penning mixture is a mixture of an inert gas w/ a small amount of a quench gas.

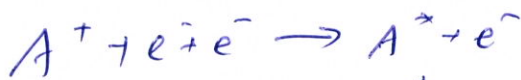
↑
lower ionization potential than the 1st excited state of the inert gas.

Ex: Neon lamp: Ne + <2% Ar

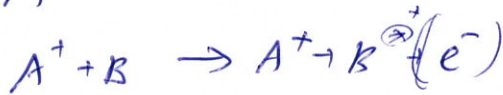
plasma display: He/Ne + Xe.

Gas ionization detector: Ar/Xe, Ne/Ar, Ar/Acetylene

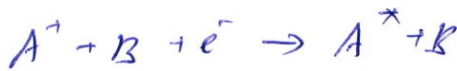
→ More complex collisions:



3-body collision.



ion impact excitation



ion impact ionization.

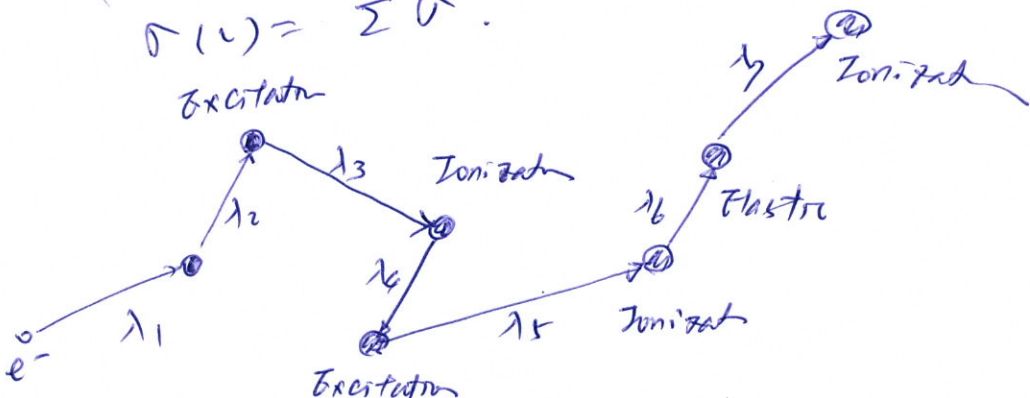
Total collisional cross sections:

$$\sigma(v) = \sigma_{el} + \sigma_{ex} + \sigma_{ion}$$

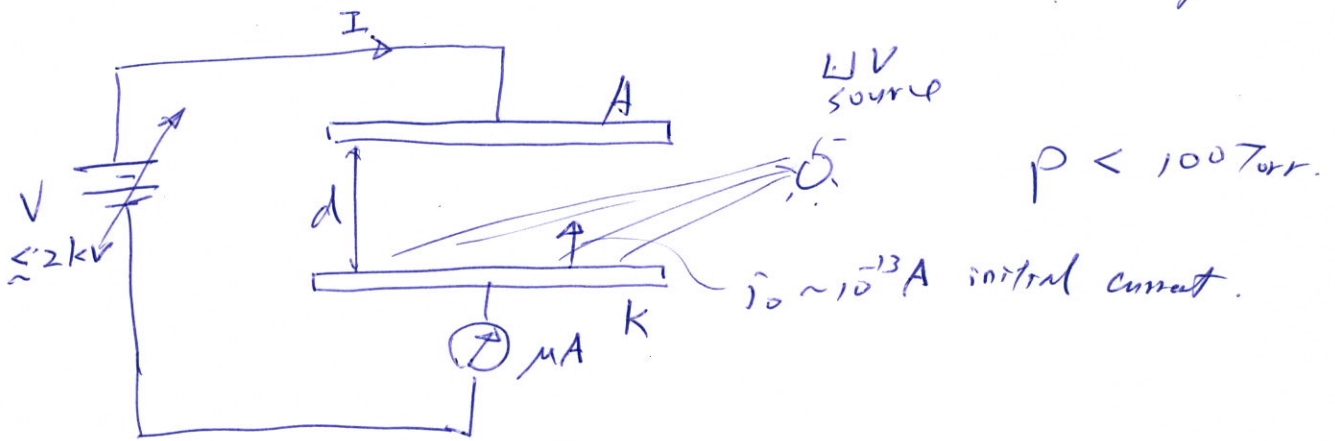
↑ ↑ ↑
electron impact excitation s.e.p. ionization
ionization.

← dominated.

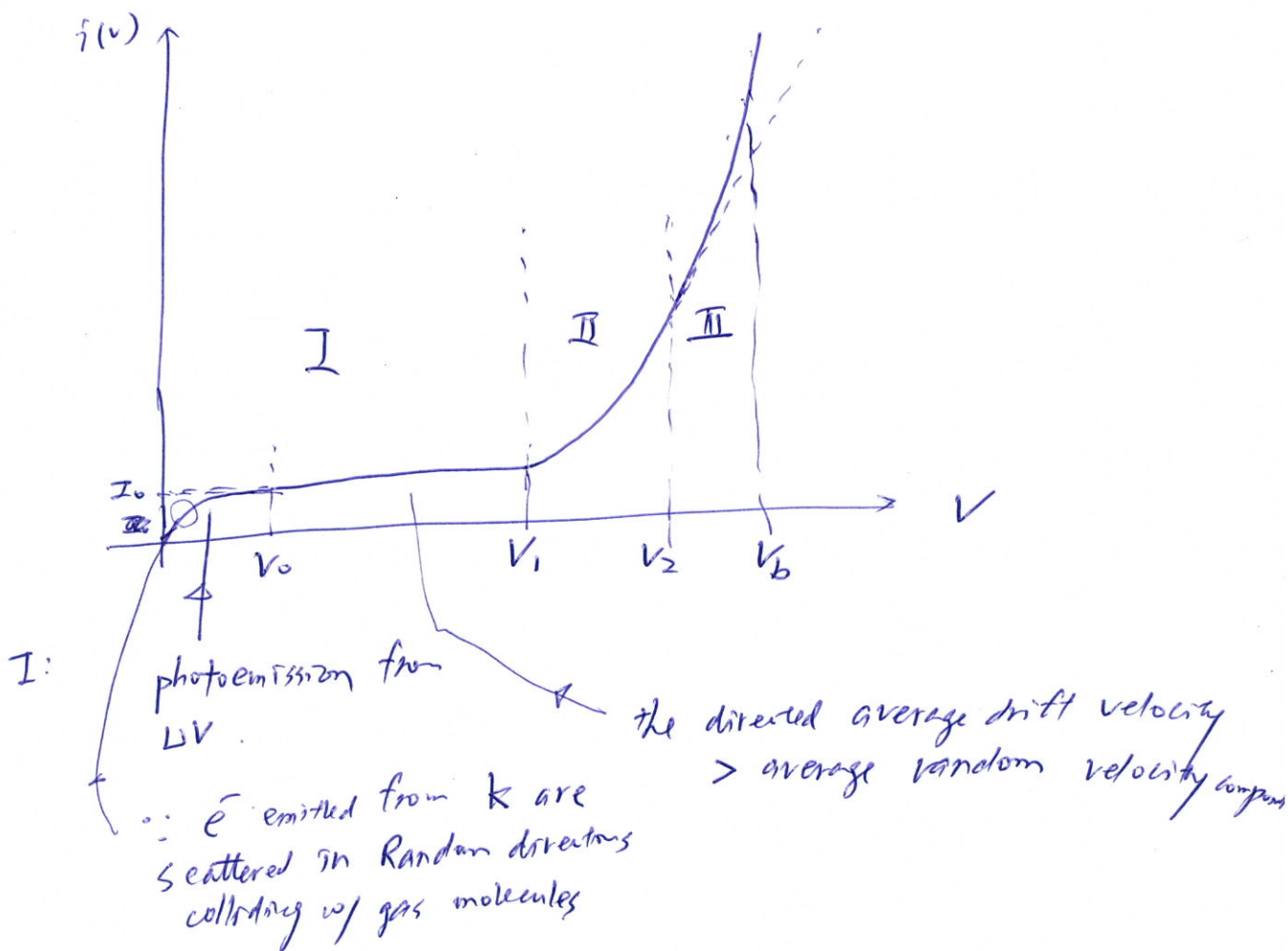
$$\sigma(v) = \sum \sigma_i$$



* Electric breakdown - Townsend's Experiments p. 21



$V \uparrow \Rightarrow I(V) \uparrow$ till spark was produced.



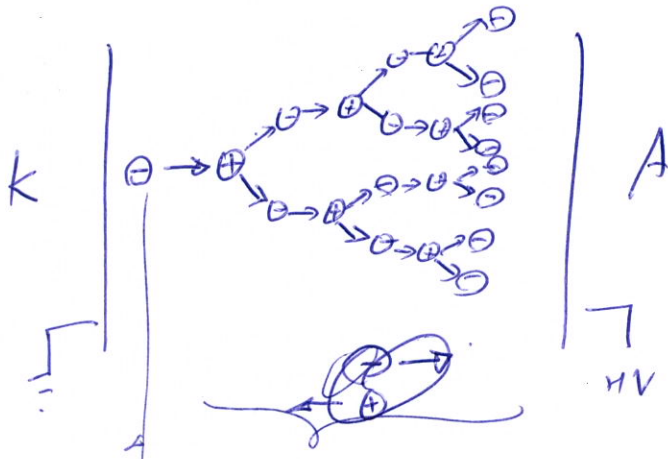
II: The Townsend 1st ionization region

$$I(d) = I_0 e^{\alpha d}$$

III: The Townsend 2nd ionization region (Townsend primary ionization coefficient)

- single-electron avalanche is not sufficient to carry the circuit-limited current
- successor avalanches are formed by positive ions, resulting from ionization collisions w/ primary e^- , bombarding K, and liberating e^-

* Electron Avalanche



present naturally

or photon

or cosmic rays

static charge

cascade ionization

$$I = \underbrace{e}_{\uparrow} \cdot n \cdot V_d$$

e⁻ drift velocity

go back to p21 w/ ⚡

$$dn = n(x) \cdot \alpha \cdot dx$$

ionization coefficient

$$\Rightarrow \int \frac{dn}{n} = \alpha \int dx \Rightarrow n(x) = n_0 e^{\alpha x}$$

electron drift toward anode
ion cathode

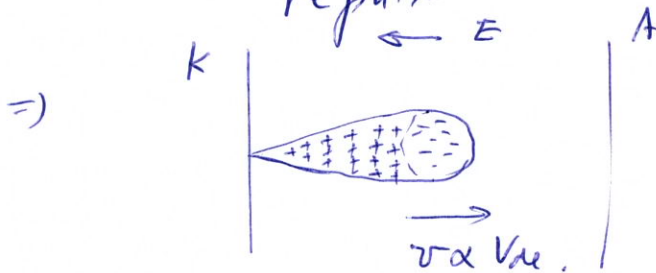
$$V_{de} \sim 10^7 \text{ cm/sec}$$

$$V_{di} \sim 10^5 \text{ cm/sec}$$

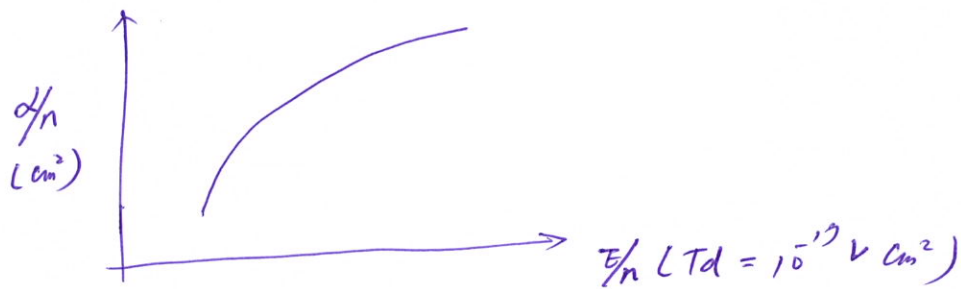
⇒ separation of charges

Additionally, e⁻ in the avalanche head diffuse ∴ repulsion of like charges.

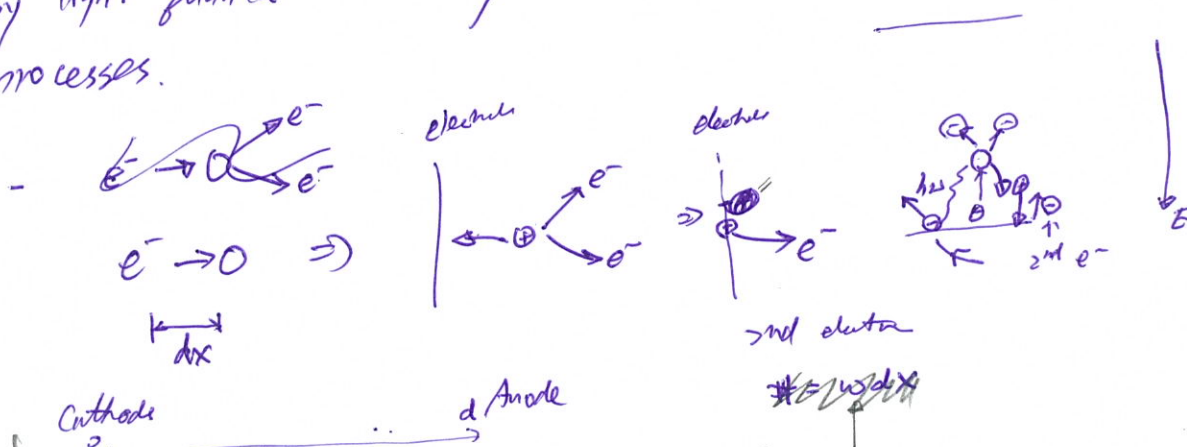
Space charge effect



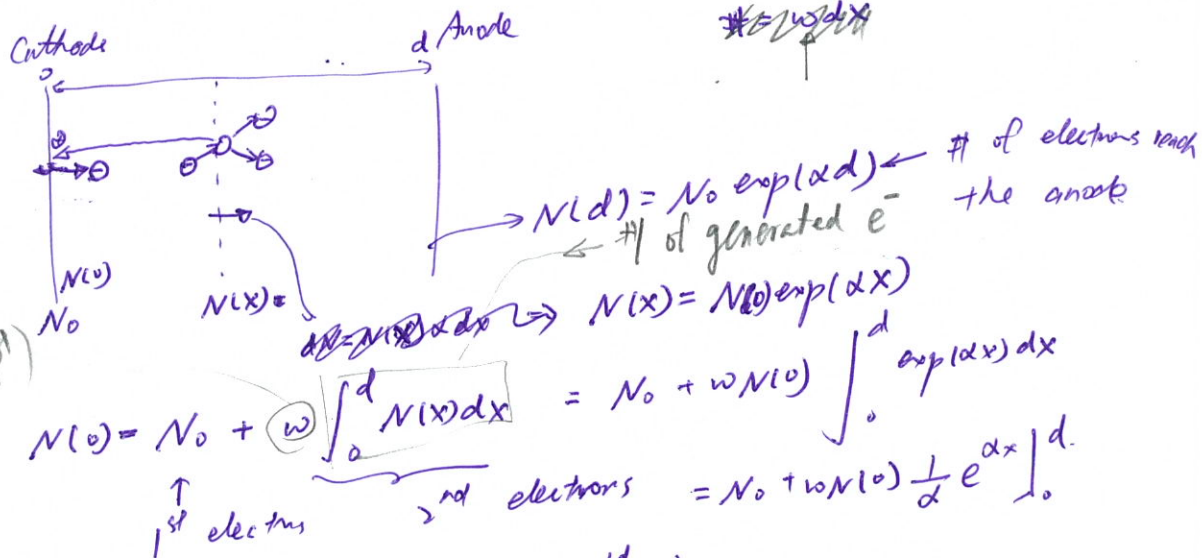
→ $\frac{d}{p}$ or $\frac{d}{n}$ can be determined experimentally.



* Secondary electrons - electrons released from the cathode by ions that have drifted to the electrode, as well as by light quanta created by recombination and de-excitation processes.



generates w coefficient of e^- from the A
 # of total e^- (generated 1st)



$$\Rightarrow N_0 = N_0 + \frac{w}{\alpha} N_0 (e^{\alpha d} - 1)$$

$$\Rightarrow N_0 = \frac{N_0}{1 - (w/\alpha)(e^{\alpha d} - 1)}$$

$$\Rightarrow N(d) = \frac{N_0 e^{\alpha d}}{1 - \frac{w}{\alpha}(e^{\alpha d} - 1)}$$

N_0 : is the # of electrons released from the cathode by external processes.

* Avalanche grows occurs when the denominator equals to 0 1223

$$1 - \frac{\omega}{\alpha} (e^{\alpha d} - 1) = 0 \quad \text{or} \quad \frac{\omega}{\alpha} (e^{\alpha d} - 1) = 1$$

This is called the "Townsend condition" for ignition.

→ In this case, the insulation of the cathode-anode gap breaks down and a self-sustained discharge is created.

to p. 239 →

* Experiments show that $\frac{\omega}{p}$ is also a function of $\frac{E}{p}$

i.e. $\frac{\omega}{p} = f\left(\frac{E}{p}\right)$, $\frac{\alpha}{p} = F\left(\frac{E}{p}\right)$

$$\Rightarrow \frac{\omega}{\alpha} (e^{\alpha d} - 1) = 1 \Rightarrow \frac{\omega/p}{\alpha/p} (e^{\alpha/p \cdot pd} - 1) = 1$$

$$\Rightarrow \frac{f(E/p)}{F(E/p)} (e^{F(E/p) \cdot pd} - 1) = 1$$

~~∴ pd can be determined if $f(E/p)$ & $F(E/p)$ are known~~

∴ $E = \frac{U}{d}$, i.e. $\frac{E}{p} = \frac{U}{pd}$

∴ U can be set solved for a given pd if

$f(E/p)$ & $F(E/p)$, i.e., $f\left(\frac{U}{pd}\right)$ & $F\left(\frac{U}{pd}\right)$, are known.

$$\Rightarrow \underline{U_b = \Pi(pd)}$$

Paschen Law: The breakdown voltage U_b of a uniform-field gap is a unique function Π of pd .

* In certain region $\frac{\alpha}{p} \approx A e^{B \frac{E}{p}}$ $\frac{\alpha}{p} = A e^{-B \frac{p/E}{U}}$

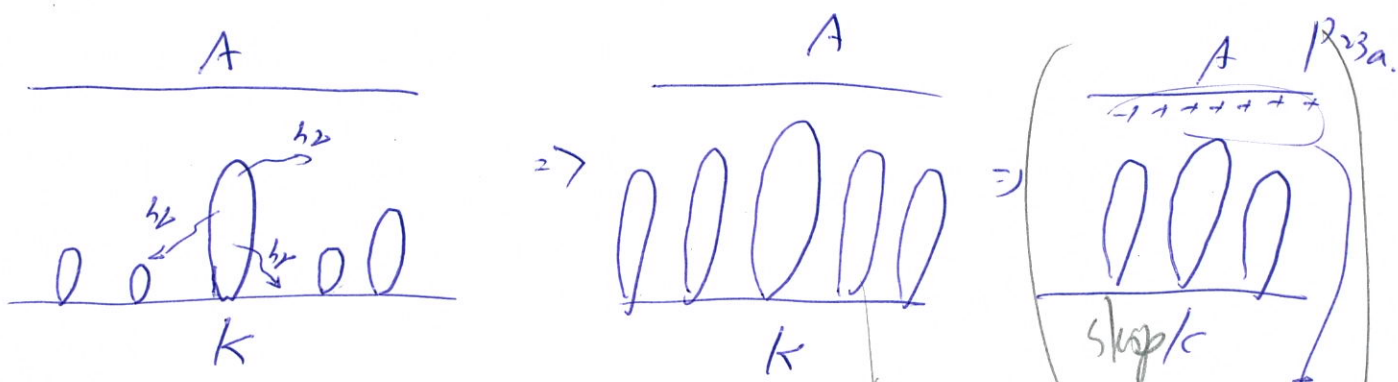
A & B are constants for a given gas.

At $\gamma \equiv \frac{\omega}{\alpha} = \frac{f(E/p)}{F(E/p)} = \gamma\left(\frac{E}{p}\right)$, which is a slowly varying function of $\frac{E}{p}$ over a wide range.

$$\Rightarrow \gamma (e^{\alpha d} - 1) = 1 \Rightarrow \gamma (e^{\frac{\alpha}{p} \cdot pd} - 1) = 1 \Rightarrow e^{\frac{\alpha}{p} \cdot pd} = 1 + \frac{1}{\gamma}$$

$$\frac{\alpha}{p} \cdot pd = \ln\left(1 + \frac{1}{\gamma}\right) \Rightarrow A e^{-B \frac{pd}{U}} = \frac{\ln\left(1 + \frac{1}{\gamma}\right)}{pd} \Rightarrow e^{\frac{B \cdot pd}{U}} = \frac{A \cdot pd}{\ln\left(1 + \frac{1}{\gamma}\right)}$$

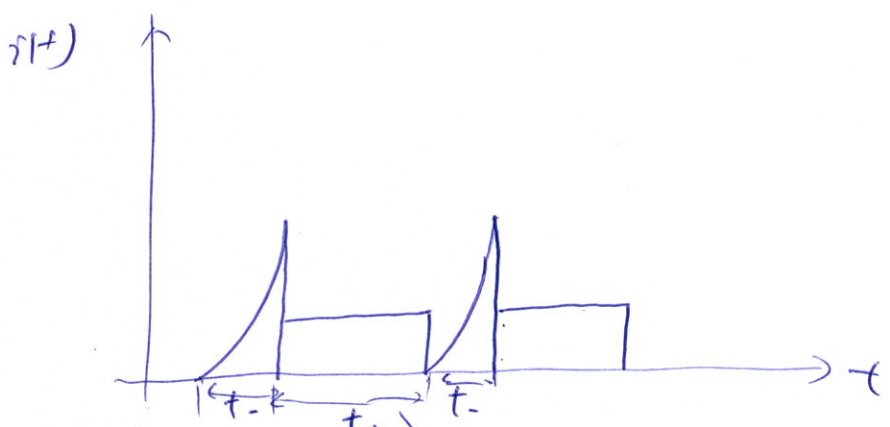
$$\Rightarrow \underline{\underline{\frac{B \cdot pd}{U} = \ln\left[\frac{A \cdot pd}{\ln\left(1 + \frac{1}{\gamma}\right)}\right]} \Rightarrow U_b = \frac{B \cdot pd}{\ln\left[\frac{A \cdot pd}{\ln\left(1 + \frac{1}{\gamma}\right)}\right]}}$$



* Multiple 2nd Mechanisms

until the curved is limited by the p system

space charge



from photon

from ion bombardment

two photon $\sim 10^{10}$ c/sa

slow \because ion drift velocity is slow $\sim 10^5$ km/sa

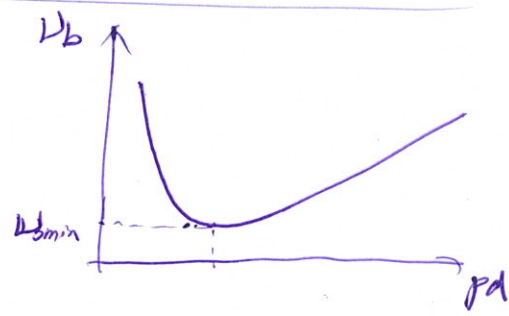
* 2nd electrons generation are strongly dependent on the cathode material.

back to p23

Gas	A (1/(mm bar))	B (KV/(mm bar))	Range of E/p for validity (KV/(mm bar))
Air	1130	27.4	11-45
N ₂	977	25.5	8-45
H ₂	376	9.8	11-30
He	210	2.6	2-11
Ar	1020	13.5	8-45
CO ₂	1500	32.9	37-75

$$U_b = \frac{B \cdot pd}{\ln[A \cdot pd / \ln(1 + \gamma/c)]}$$

$$\Rightarrow U_b = \frac{B \cdot x}{\ln[A \cdot x/c]} \quad x \equiv pd$$

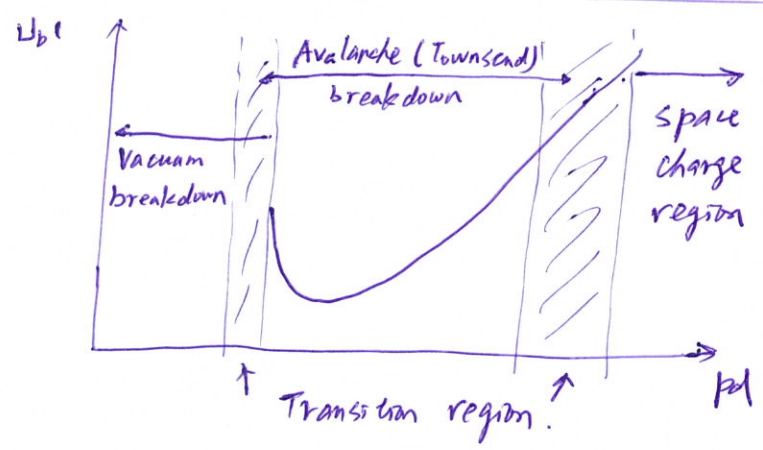


$$\frac{dU_b}{dx} = \frac{B \cdot \ln[A \cdot x/c] - Bx \cdot \frac{1/c}{A \cdot x/c}}{[\ln(A \cdot x/c)]^2} = \frac{B[\ln(A \cdot x/c) - 1]}{[\ln(A \cdot x/c)]^2} \stackrel{!}{=} 0$$

$$\Rightarrow \ln(A \cdot x/c) - 1 = 0 \Rightarrow x = e \cdot \frac{c}{A}$$

$$U_b = \frac{B \cdot x}{\ln[e \cdot \frac{c}{A} \cdot \frac{A}{c}]} = \frac{B \cdot x}{\ln e} = B \cdot x = e \cdot c \cdot \frac{B}{A}$$

$$\Rightarrow U_{b,min} = e \cdot \ln[1 + \frac{1}{\gamma}] \cdot \frac{B}{A} \quad (9) \quad pd = e \cdot \frac{\ln(1 + \frac{1}{\gamma})}{A}$$



* With a voltage lower than $U_{b,min}$, it is impossible to cause the breakdown of a gap with a uniform field distribution.

* At ^{very} high field strengths, field emission of electrons from the electrodes occurs. (for left & far right of Paschen curve)

* The most commonly used high-strength gas is SF₆.

SF₆ belongs to a group of "electronegative gases", which are characterised by the ability to attach electrons to the molecule, which then becomes a "negative ion".

⇒ attachment coefficient: γ - attachment ~~coefficient~~ probability of an electron per unit path length.

* other electronegative: compounds containing Halogens (Cl, F, I, ... & O₂).

Effective ionisation coefficient: $\alpha_e = \alpha - \gamma = P f\left(\frac{E}{P}\right)$

⇒ Electron avalanche formation becomes possible only if $\alpha_e > 0$. Ex: $\frac{E}{P} > 8.84 \text{ kV/(mm bar)}$ is needed for SF₆

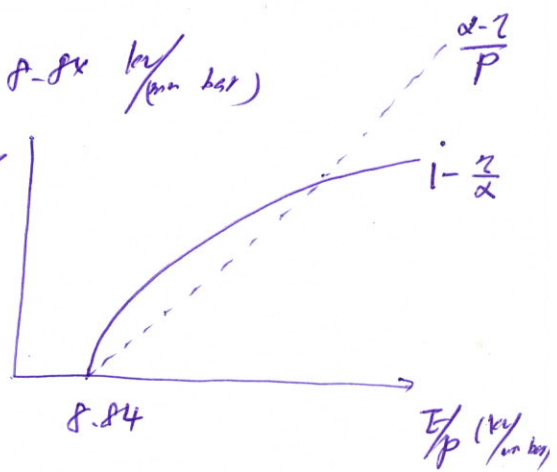
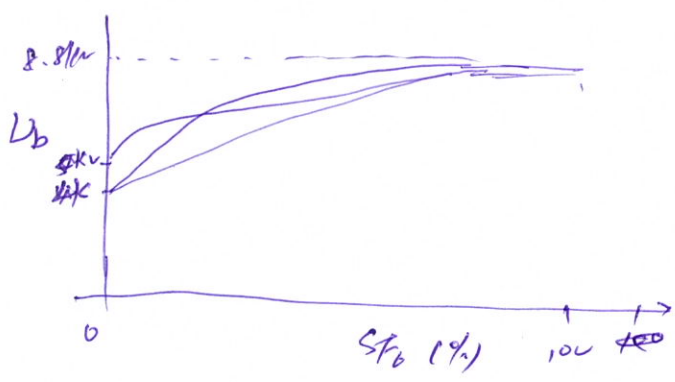
$$\frac{\alpha - \gamma}{P} = k \left[\frac{E}{P} - \left(\frac{E}{P}\right)_0 \right]$$

for SF₆: $k = 27.2 \text{ kV}$, $\left(\frac{E}{P}\right)_0 = 8.84 \text{ kV/(mm bar)}$

Sketch

∴ $L_b = pd \cdot 8.84 \text{ [kV/(mm bar)]} \rightarrow 10.5 \text{ kV}$
 derivat - see next page.

* SF₆ maintains a high electric strength even if it is diluted with another gas.



* Vapours of higher strength than SF₆ are known, but most of them liquefy at atmospheric pressure and room temperature.

eg 2.8: $\gamma (e^{\alpha d} - 1) = 1 \Rightarrow \alpha d = \ln(1 + \frac{1}{\gamma})$

eg 2.15: $\frac{\alpha_e}{P} = \frac{\alpha - \gamma}{P} = K \left[\frac{E}{P} - \left(\frac{E}{P}\right)_0 \right] = K \left[\frac{U}{Pd} - \left(\frac{E}{P}\right)_0 \right]$

$\Rightarrow \alpha_e d = \frac{\alpha_e}{P} \cdot Pd = Pd \cdot K \left[\frac{U}{Pd} - \left(\frac{E}{P}\right)_0 \right] = \ln(1 + \frac{1}{\gamma})$

$\Rightarrow U_b = Pd \left(\frac{E}{P}\right)_0 + \frac{1}{K} \ln(1 + \frac{1}{\gamma})$

$= Pd \cdot 8.84 \text{ (kV/mm bar)} + 0.5 \text{ eV for SF}_6$

Quadratic ansatz \rightarrow for gas are not electronegative or are only weakly so:

$\frac{\alpha_e}{P} \sim \left[\frac{E}{P} - \left(\frac{E}{P}\right)_0 \right]^2$

$\Rightarrow \frac{\alpha_e}{P} \sim \left[\frac{U}{Pd} - \left(\frac{E}{P}\right)_0 \right]^2$

$\alpha_e d = \frac{\alpha_e}{P} \cdot Pd = Pd \cdot \left[\frac{U}{Pd} - \left(\frac{E}{P}\right)_0 \right]^2 = \ln(1 + \frac{1}{\gamma})$

$\Rightarrow \sqrt{Pd} \left[\frac{U}{Pd} - \left(\frac{E}{P}\right)_0 \right] = \sqrt{\ln(1 + \frac{1}{\gamma})}$

$U = \left(\frac{E}{P}\right)_0 \cdot Pd + \sqrt{\ln(1 + \frac{1}{\gamma})} \cdot \sqrt{Pd} \rightarrow \text{eg 2.18}$

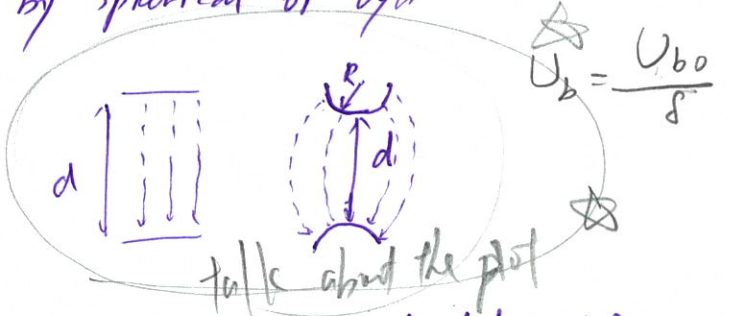
skip
 $\frac{\alpha}{P} = A \left| 1 - \frac{BP}{E} + \frac{1}{2} \left(\frac{BP}{E}\right)^2 \right|$

plot to compare to path curve.

Gas	$(E/P)_0$ (kV/mm bar)	C (1eV/(bar mm))
CO ₂	3.21	5.88
Air	2.44	2.12
N ₂	2.44	4.85
H ₂	1.01	2.42

The mean breakdown strength can change considerably if a gap is bounded by spherical or cylindrical electrodes especially $d > R$

$U_b = \frac{(E/P)_0 Pd + c(Pd)^{1/2}}{\delta}$



$U_b = \frac{U_{b0}}{\delta}$

- concentric cylinders
- Equal spheres

$\delta = (R/r - 1) / \ln(R/r)$

~~$\delta \approx \frac{d}{2r}$~~
 $\delta \approx \frac{x}{2r}$ for $x/r \gg 1$ where $x = d - 2r$

- Equal parallel cylinders

$\delta \approx \frac{x}{2r \ln(x/r)}$ for $x/r \gg 1$ where $x = d - 2r$

* For very inhomogeneous field configurations
(needle geometries)

p2,



$E_{needle} > E_{flat}$

keep

$$U_b = \left(\frac{E}{P} \right)_0 pd + c(pd)^{1/2}$$
 ← can only be used

but with d_{eff}

keep this

d_{eff}: It's defined as the distance where the field has dropped to about 80% of its maximum value

* For spherical and cylindrical electrodes,

d_{eff} = 0.115 r & 0.23 r



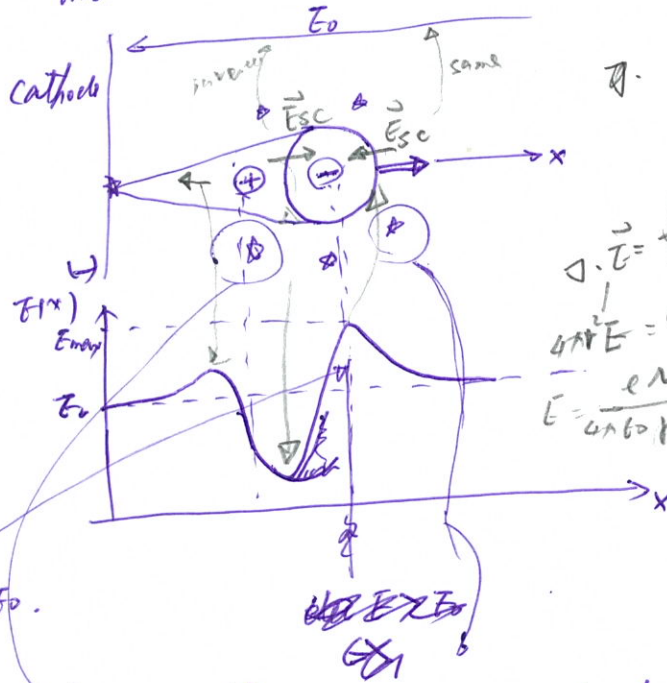
p2/a

2.2.1.1 Space charge effects.

* The space charge was neglected that is created in the electron avalanche was neglected!! But it can not be neglected if there are 10⁶ ~ 10⁸ particles in a gas at atmosphere pressure.

p2/e

* immobile ions stay behind in the avalanche tail.
mobile electrons form the spherical avalanche head.



If there are N charged particles

since the charge density grows by a factor of e over a distance (Δx) ← performed by an e in a unit length.

$$\Delta \cdot \vec{E} = \frac{\rho}{\epsilon_0}$$

$$\Delta \cdot \vec{E} = \frac{eN}{\epsilon_0 \Delta x}$$

$$E_{sc} = \frac{eN}{4\pi\epsilon_0 (\Delta x)^2} = 1.5 \times 10^{17} \frac{N}{(\Delta x)^2} \text{ V/m}$$

For N = 10⁷, Δx = 10⁻² cm

$$E_{sc} = 15 \text{ kV/cm} \approx \text{applied field}$$

ionisation caused by electron is more efficient ∵ E > E0.

⇒ "Streamer mechanism"

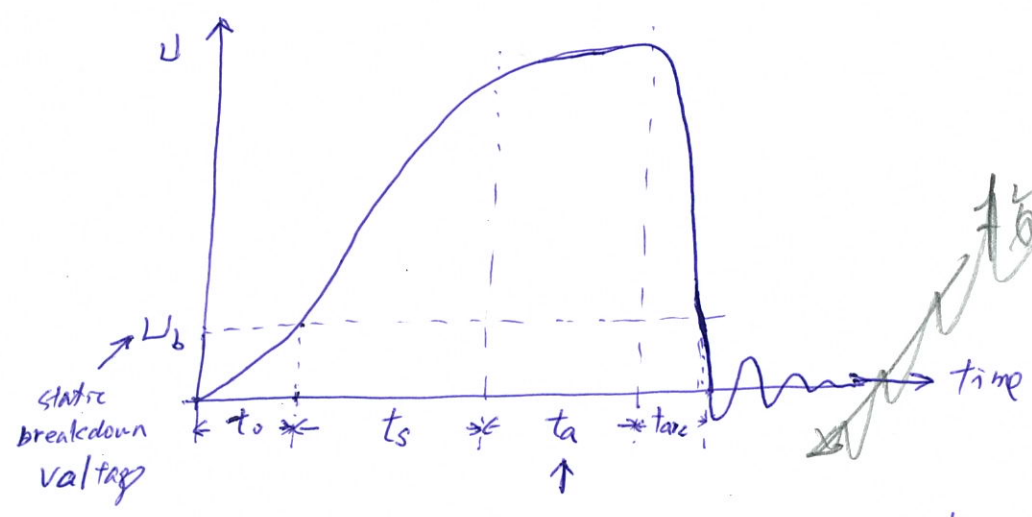
UV light emitted in recombination and de-excitation.
 ⇒ creates electrons by "photoionisation" ahead & behind the avalanche
 ⇒ form a conducting bridge between anode & cathode

* Creating photoelectrons at larger distances from the main streamer can advance the growth of the breakdown ~~to~~ channel rapidly.

add slope $\Rightarrow v = 100 - 1000 \text{ cm}/\mu\text{s}$ was observed at atmospheric pressure.

2.2.2. Pulsed breakdown.

* If a fast-rising pulse across the gap, we must take account into the fact that it takes a finite time before breakdown can occur.



t_0 : the time until the static breakdown U_b is exceeded.

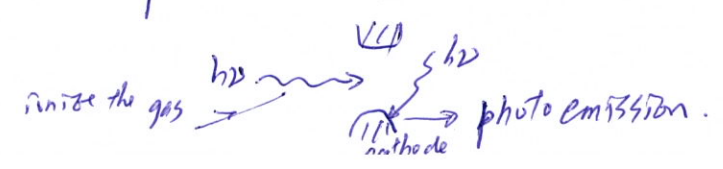
t_s : statistical delay time until an electron able to create an avalanche occurs.

t_a : the avalanche build-up time until the critical charge density is reached.

t_{arc} : the time required to establish a low-resistance arc across the gap.

results from the statistics of electron appearance.

* Free electrons can be created by illuminating the gap volume or the cathode surface with electromagnetic radiation, such as particular UV light, x-rays & γ -radiation.



gets p32 after this page

* Streamer Mechanism. p. 2 a

- For long, atmospheric air gaps \rightarrow can't be explained using Townsend's model
Ex ① $d \sim 1 \text{ cm} \Rightarrow$ short delay time ($< 1 \mu\text{s}$)

For Townsend's model: successive avalanches ~~develop~~
is determined by ion drifting velocity
 $\Rightarrow \Delta t \sim \frac{1 \text{ cm}}{10^5 \text{ cm/s}} \sim 10 \mu\text{s}$

Ex ②: breakdown appears to be independent of cathode material.

Ex ③: Townsend discharge: broad development from the cathode.

However, existence of narrow, luminous discharges originating from either the anode or from the middle of the gap may happen !!

\Rightarrow Streamers - evocative of a thin band of bright light, attached at one end to an electrode and floating toward the other -
"Kanals", channel in German.

* Cathode-directed (positive) streamers (from A \rightarrow K)

Anode-directed (negative) streamers (from K \rightarrow A)

* single-electron avalanche \rightarrow streamer

~~when~~ Streamers develop when the charge density at the head of the avalanche becomes so large that it distorts the applied electric field.

i.e. space charge in the avalanche head generates a self-electric field that is on the order of the applied electric field.

* Criterion for Streamer Onset:

page 6

$$E_r \sim E_0$$

↑
generated by the space charge at the head of the avalanche.

Space charge or $N_{ct} \sim 10^{18} \text{ cm}^{-3}$
↑
of e^- in

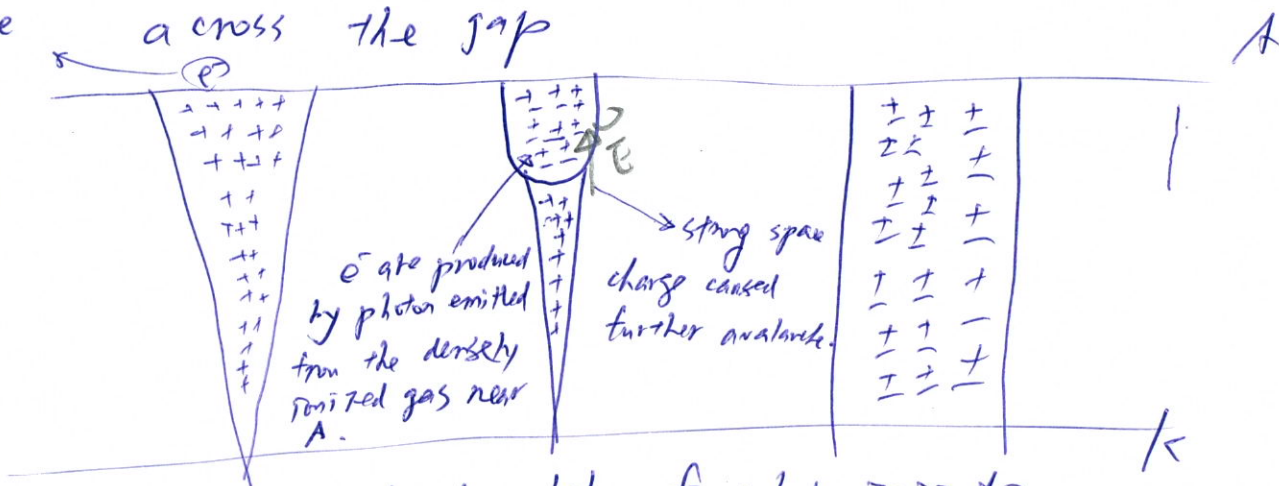
back to p. 77

from A to K

* Cathode-directed (Positive) Streamer.

- When the avalanche has crossed the gap, the e^- are swept into the anode, the ions remaining in a cone-shaped volume extending ^{positive} across the gap.

are gone when they reach A

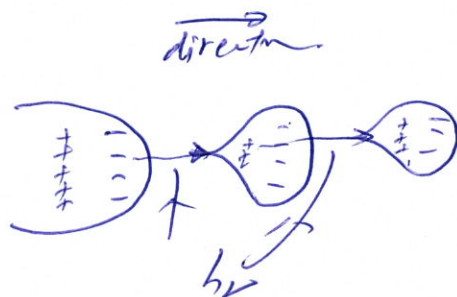
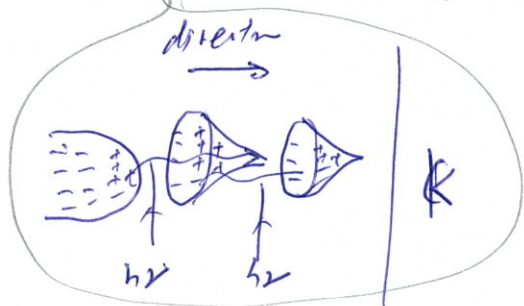


- grows w/ the help of photonization

* Anode-directed (Negative) Streamer:

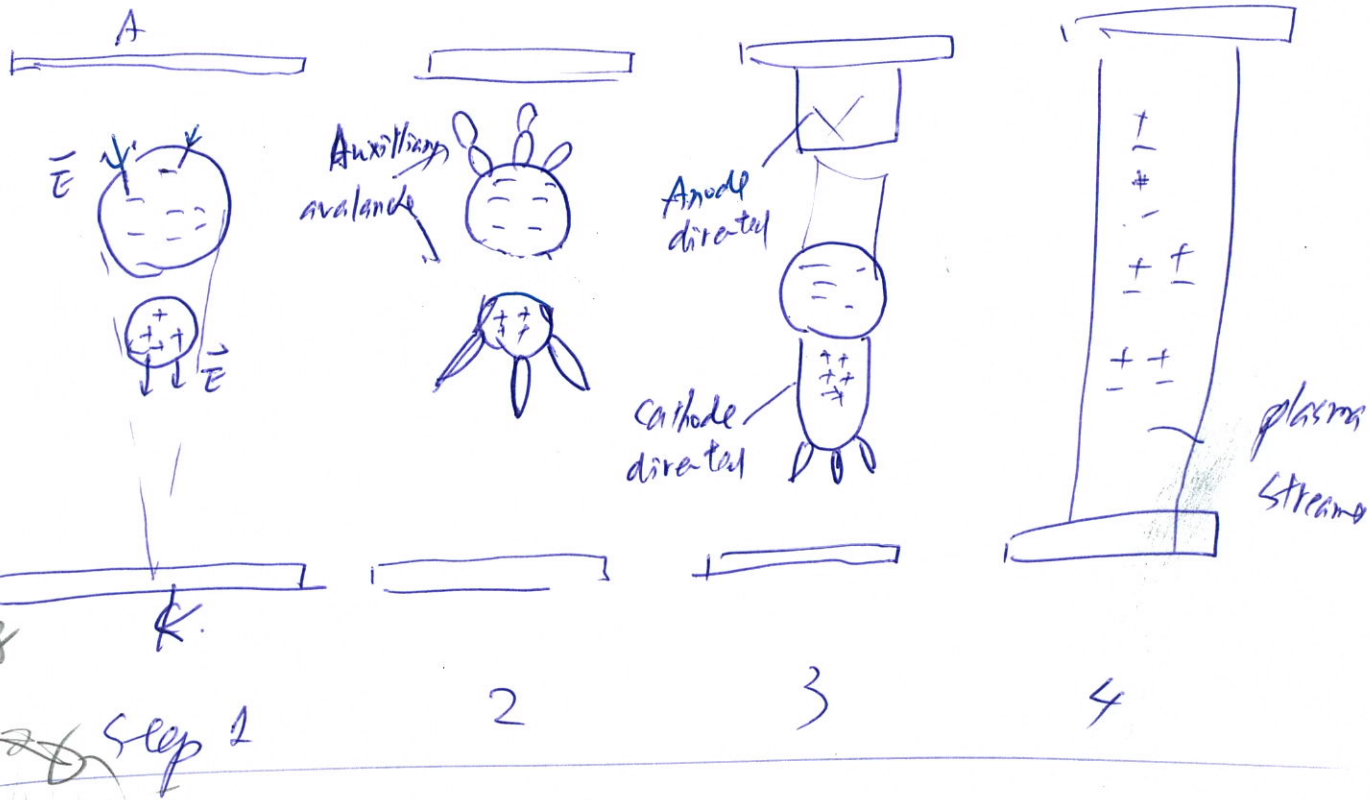
- When the primary avalanche becomes sufficiently strong before reaching the anode.

$$\# \text{ of } e^- \sim 10^{18}$$



Anode

→ Overvolted Streamer:



→ The Corona discharge.

- Corona is a luminous, audible discharge that occurs when an excessive localized electric field gradient causes ionization in the ~~sur~~ surrounding gas.

It manifests easily in highly nonuniform E field geometries.

→ colored glow frequently visible in darkened environment

• subtle hissing sound, volume $\propto V^2$

• O_3 can be generated → rubber can be destroyed

~~NO_2~~
→ NO_2 can be generated w/ moisture.

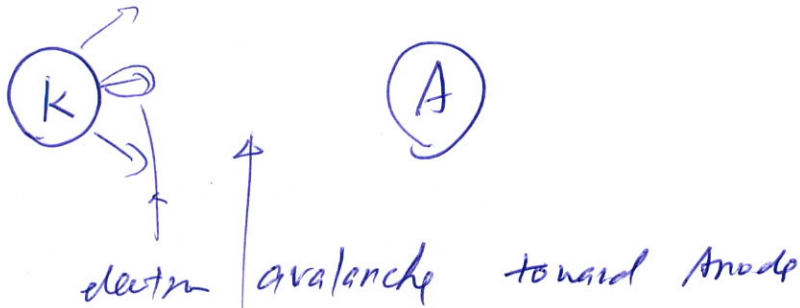
h2.2.2
p28

step 2

after p35c

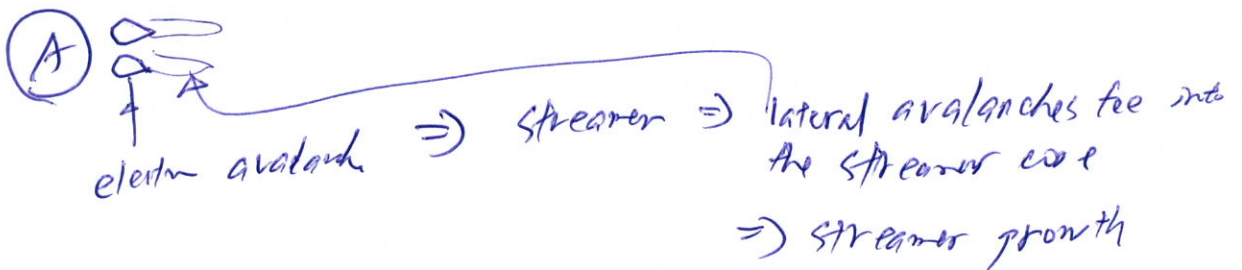
- Negative point corona (Fricke pulses)

P28 ①



- $\Rightarrow \vec{E}$ is too small \rightarrow No more ionization
- $\Rightarrow e^-$ are slowed down \therefore ions left behind
- \Rightarrow attach to gas molecules forming \ominus ions
- $\Rightarrow \vec{E}$ field cancel the external \vec{E} field
- $\Rightarrow \oplus$ & \ominus ions drift to each electrode (current)
- \Rightarrow No more cancel \vec{E} field
- \Rightarrow corona again
- \Rightarrow steady-state corona current when V is high enough

- Positive point corona



* Corona - power loss

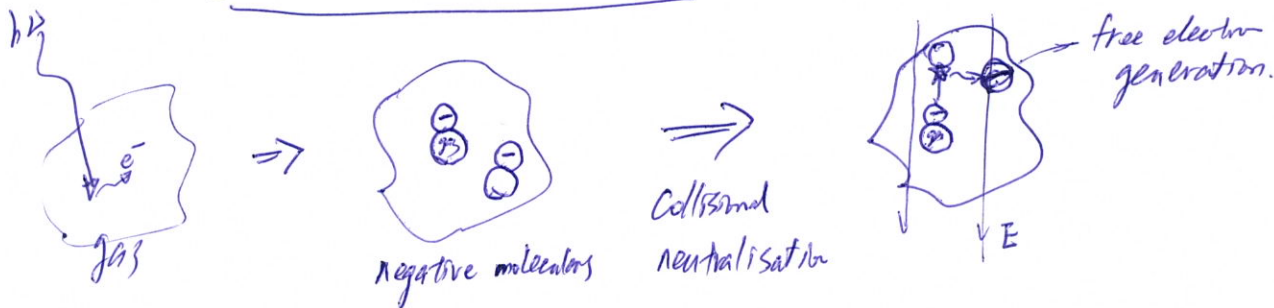
- RA interference.
- service life \downarrow

go back to p36 a9

* Natural radioactivity & cosmic radiation

→ 0.1 ~ 10 free electron / cm³-s in a gas at atmosphere.

- the electron can attach to the gas molecules
- few thousand negative molecular ions / cm³ - few minutes
(SF₆ : 2500 SF₆⁻ ions / cm³ in 5 minutes was measured)
- With electric field → e⁻ can be liberated through collisional neutralisation → free electron generation



$$\dot{n}_s(t) = \delta \cdot n_n \cdot U_n$$

$$U_n = \mu_{mix} \cdot E$$

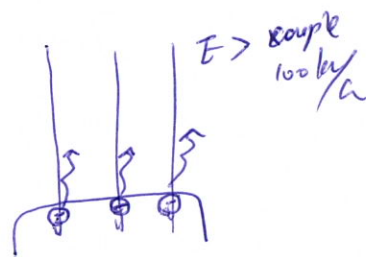
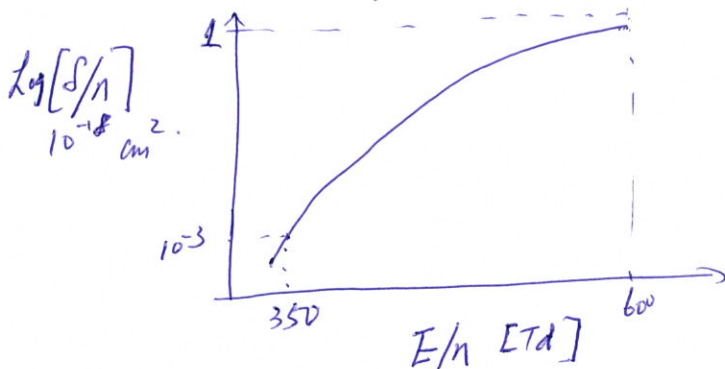
\dot{n}_s : rate of electron detachment / unit volume

n_n : density of negative ion

δ : coefficient of collisional electron detachment

U_n : ion drift velocity

μ_{mix} : mobility - depends on the kind of ions gas composition.



* If $E >$ few times 100 kV/cm → more electrons can leave the metal surface through the funnel effect

The current density (Fowler-Nordheim eq. 1928)

$$j = \frac{1.54 \times 10^{-6} \beta^2 E^2}{\phi} \exp \left\{ - \frac{6.83 \times 10^{-7} \phi^{3/2} (1/y)}{\beta E} \right\}$$

βE ↑
 Enhancement factor - take into account the special conditions at localised emission centers on the metallic surface.

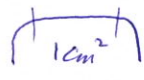
$$O(y) = 0.956 - 1.06 \frac{y^2}{\sqrt{\beta E}}$$

$$y = 3.8 \times 10^{-4} \frac{\sqrt{\beta E}}{\phi}$$

ϕ work func. eV

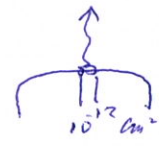
* The importance of localised emission site

To generate 10^6 e/sec. from a flat metallic surface of area 1cm^2 ,



$E \geq 1.2 \times 10^7$ V/cm is needed

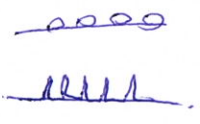
For a localised emission site possessing a field enhancement of $\beta=100$



$\Rightarrow E \geq 2.4 \times 10^5$ V/cm is needed for an area of 10^{-12}cm^2

* Most important emission centers:

- dielectric inclusions
- metallic microprotrusions (whiskers)
- absorbed gases



* Total number of electrons in the gap:

$$N(t) = N_{0n} + N_F(t) + N_S(t)$$

N_{0n} : # of naturally occurring electrons in the gap, independent of time

$N_F(t)$: rate of field-emitted electrons

$N_S(t)$: rate of electron detachment.

* Note that not every electron released into the gap is able to initiate an avalanche even if the voltage is above the static breakdown value !!

\rightarrow Avalanches can grow only in those parts of the gap volume where the local field strength exceeds a certain critical value

\rightarrow For electronnegative gases, E_{crit} is when the ionisation coefficient $\alpha > \eta$ the electron capture coefficient.

* The probability for a single electron to initiate an avalanche.

$$g\left(\frac{E}{P}\right) = 1 - \frac{\eta}{\alpha} \quad \left(\begin{array}{l} \text{for greater } \alpha, \text{ } g\left(\frac{E}{P}\right) \text{ is larger} \\ \text{smaller } \eta \end{array} \right)$$

$$N(t) \rightarrow N_a(t) = \int_{-F}^F g\left(\frac{E}{P}\right) N_{Fi}(t) dt + \int_V g\left(\frac{E}{P}\right) [N_s(t) + N_{io}] dV \quad |33|$$

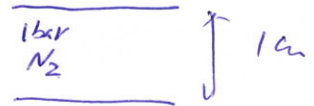
probability that a breakdown has occurred before time t :

$$F(t) = 1 - e^{-\int_0^t N_a dt} \quad (\text{conditional probability})$$

or probability density:

$$f(t) = N_a e^{-\int_0^t N_a dt}$$

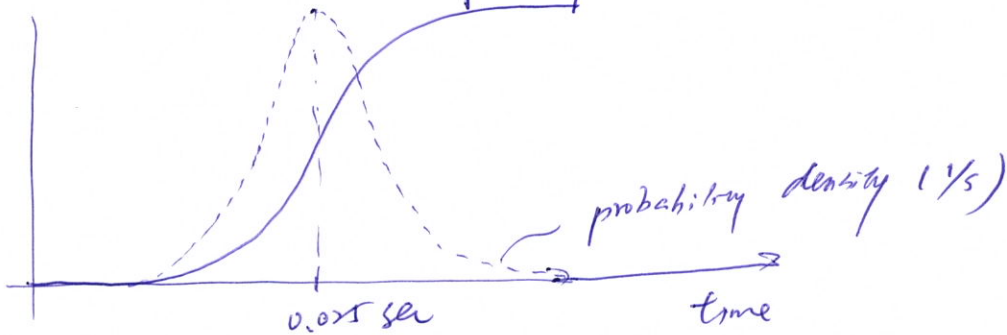
Ex: 1 cm gap w/ 1 bar dry N_2



\Rightarrow static breakdown voltage: 31 kV

If the gap is ramped at 6 mV/sec.

probability of avalanche initiation



slow

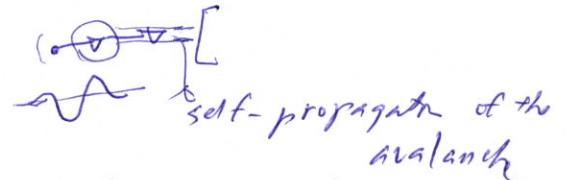
$$\Rightarrow 0.025 \text{ sec} \times 6 \text{ mV/sec} = 150 \text{ kV} \gg 31 \text{ kV} \quad \llcorner$$

\rightarrow After the 1st electron avalanche there are two ways to breakdown.
 Townsend breakdown \rightarrow quasi-stable glow discharge
 streamer mechanism \rightarrow glow-to-spark transition

order

streamer mechanism:

t_a are very different between two

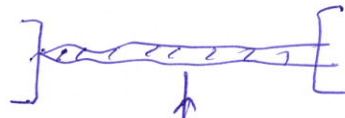


assumes that secondary e^- are released from cathode through interaction with photons & ions \Rightarrow distribute the discharge over a larger volume

The overvoltage must be sufficiently large such that the critical electron number N_{crit} is established in the gap during a single avalanche.
 $\sim 15-20\% >$ static breakdown level \llcorner

2.2.3 Spark Formation

* A conducting channel exists between the anode and the cathode after a streamer has bridged the high-voltage gap.



→ An intense current starts to heat the channel and to ionise it further until a low-resistance channel is established (1926, 1927)

* Pfeiffer's model (1971):

Assuming that a weakly conducting column exists and that its conductivity is increased by collisional ionisation: ($\sigma \uparrow$ as ionisation \uparrow)

$$dN_e = N_e \cdot \alpha \cdot dx$$

electron spreading ~~speed~~ drift velocity

$$= N_e \cdot \alpha \cdot \mu_e E dt$$

electron mobility

$$= N_e \cdot \alpha \cdot \mu_e E \cdot dt$$

mean electric field in the spark channel.

$$j = N_e \cdot \mu_e \cdot e \cdot E (= N_e \cdot \mu_e \cdot e)$$

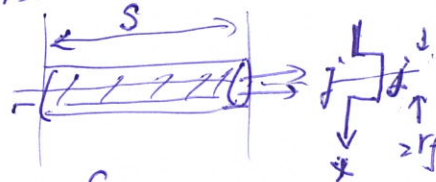
$$\Rightarrow dN_e = \alpha \cdot \frac{j}{e} \cdot dt \Rightarrow N_e = \frac{\alpha}{e} \int_0^t j dt$$

Assuming a homogeneous current density distribution in the column

$$R_f(t) = \frac{U}{I} = \frac{E \cdot s}{j \cdot \pi r_f^2}$$

$$= \frac{E \cdot s}{\alpha \int_0^t j dt \cdot \mu_e \cdot e \cdot E \cdot \pi r_f^2}$$

$$= \frac{s}{\alpha \cdot \mu_e \int_0^t I dt}$$



s: channel length

r_f: radius of the spark channel.

spark resistance

$\mu_e = \frac{N_e E}{j}$
mobility

* This model (Toepfer) says that:

$$R \propto \frac{1}{\int I dt} = \frac{1}{Q} \leftarrow \text{charge that has been flowing through the channel.}$$

* The column expands when it is heated by the current flow.

⇒ It is not considered in the model

⇒ It is only valid for a limited time after the channel is formed, ~10ns in a gas at atmosphere.

* Weizel & Rompe (1964, 1965) model

- channel expansion is ignored as well.

slip

$$R_f(t) = \frac{S}{\sqrt{2 \frac{a}{P} \int_0^t I^2 dt}}$$

a → constant
P → gas pressure

→ * Braginskii (1958)

- consider the thermal expansion of the plasma channel



- assuming a time independent specific conductivity for the plasma channel.

$$R_f(t) = \frac{S}{\pi \sigma b^2 \int_0^t I^{2/3} dt}$$

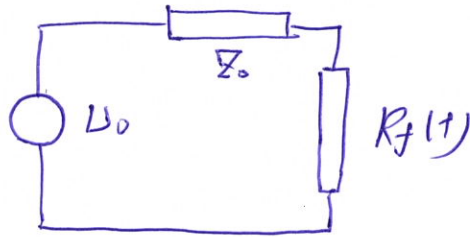
b: a constant depend on density, conductivity & the thermodynamic properties of the plasma.

σ: mean plasma conductivity.

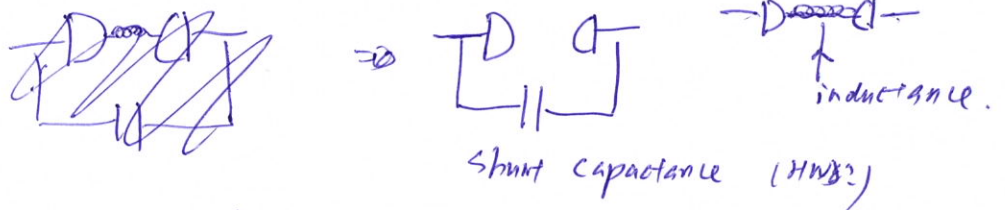
Gas	$k_T = \frac{1}{2} \alpha_{\text{He}}$ (10^4 V s/cm)	a atm $\text{cm}^2/\text{V}^2\text{s}$	σb^2 ($10^4 \text{ A}^{2/3} \text{ cm/V s}$)
Air	0.5 - 0.6		
N ₂	0.4	1.1	3.5
CO ₂	0.5	1.0	3
Argon	0.085	25	10

gato P35a
a plax haw

* Let's determine the current increase and the voltage decrease across the spark using Toepla's relationship. P34



* Inductance of the spark & shunt capacitance are neglected



U_0 : ignition voltage

Z_0 : impedance of the driving source.

$$I_{max} = \frac{U_0}{Z_0 + R_f} \approx \frac{U_0}{Z_0} \quad (\text{generally, } Z_0 \gg R_f)$$

$$I = \frac{U_0}{Z_0 + R_f} = \frac{U_0}{Z_0 + \frac{s}{\alpha \mu_0} \int_0^t I dt} = \frac{U_0}{Z_0 + \frac{s \cdot k}{\int_0^t I dt}}$$

$$\frac{I}{I_{max}} \equiv y = \frac{U_0}{Z_0 + \frac{s \cdot k}{I_{max} \int_0^t \frac{I}{I_{max}} dt}} \cdot \frac{I_{max}}{U_0} = \frac{1}{1 + \frac{s \cdot k}{Z_0 \cdot \frac{U_0}{Z_0} \int_0^t y dt}}$$

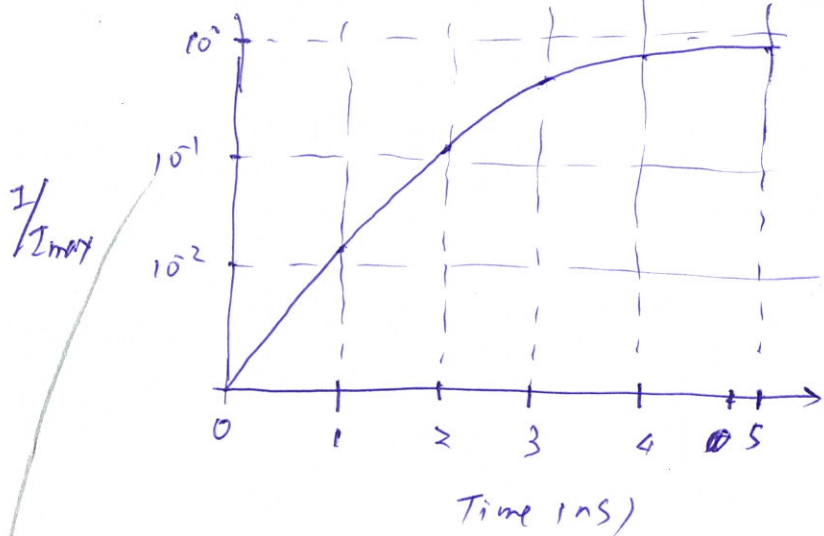
$$\Rightarrow y = \frac{1}{1 + \frac{k}{E_0} \int y dt} \Rightarrow \frac{1}{y} - 1 = \frac{k}{E_0} \int y dt$$

$$\Rightarrow \int y dt = \frac{k}{E_0} \frac{y}{1-y} \Rightarrow \frac{d}{dt} y = \frac{k}{E_0} \frac{dy}{dt} \cdot \frac{(1-y) + y}{(1-y)^2}$$

$$\Rightarrow dt = \frac{k}{E_0} \frac{dy}{y(1-y)^2} \Rightarrow t = \frac{k}{E_0} \left[\ln \left(\frac{y}{1-y} \right) + \frac{1}{1-y} + C \right]$$

Assuming that spark current begins with $y = \frac{I}{I_{max}} = 10^{-3}$

$$\Rightarrow C = 5.906$$



$$K = 0.4 \times 10^{-4} \text{ Vs/cm}$$

$$E_0 = 10^5 \text{ V/cm}$$

N_2 .

rise time: $\tau_{0.1-0.9} = 13.2 \frac{K}{E_0}$

refolding time: $\tau_r = 6.84 \frac{K}{E_0}$

Eq 5.11 * J. C. Martin's (1996) formula:

$$\tau_r = \frac{88}{Z_0^{1/3} E_0^{4/3}} \sqrt{\frac{\rho}{\rho_0}} \quad (\text{ns})$$

Z_0 : impedance driving the channel.

E_0 : the field at the beginning of breakdown.
in unit of 10kV/cm

ρ : the density of the gas

ρ_0 : ~~air~~ under normal condition.
(atmosphere)

7 The corona discharge.

P35
9

Corona - a luminous, audible discharge that occurs when an excessive localized electric field gradient causes ionization in the surrounding area.

- It manifests easily in highly nonuniform electric field geometries



→ colored glow infrequently visible in darkened environment.

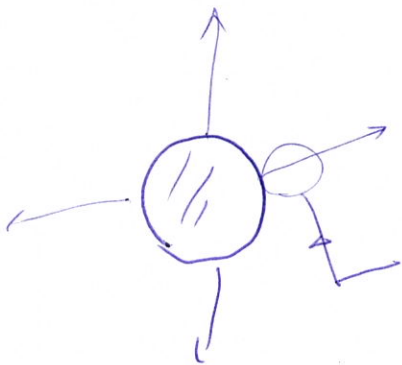
→ a subtle hissing sound, $I \propto V$

⇒ Ozone is generated.

⇒ rubber is destroyed, ~~etc~~ by O_3

NO_3^+ is generated w/ moisture

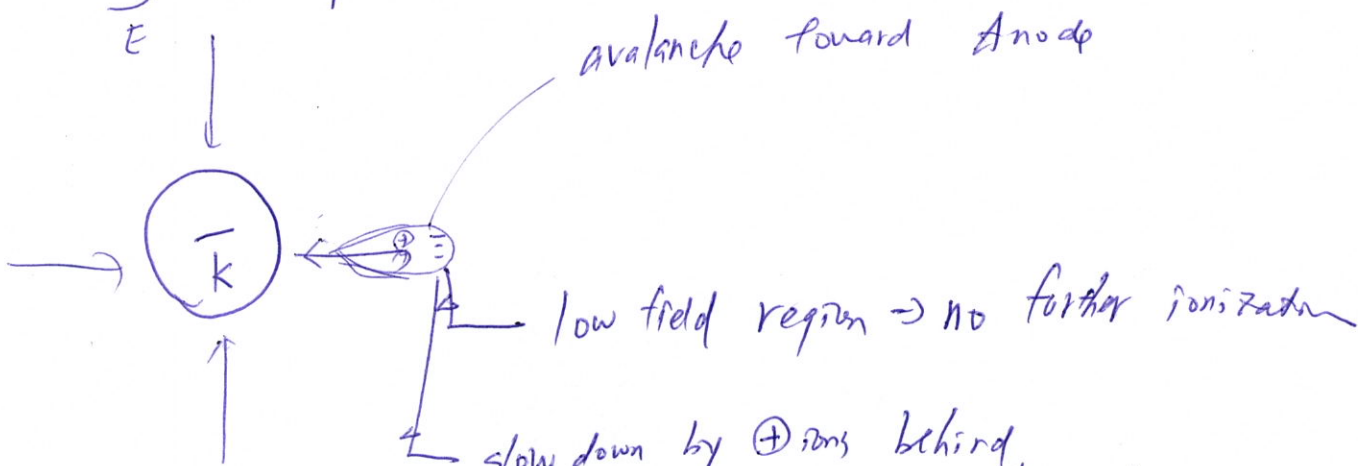
$$E \propto \frac{1}{r^2}, \quad V \propto \frac{1}{r}$$



Townsend breakdown occurs in small region only
 ⇒ luminous glow w/ hissing noise.

• current pulses $\begin{cases} \text{randomly} \\ \text{regularly} \end{cases}$

- Negative point corona - Trichel pulses



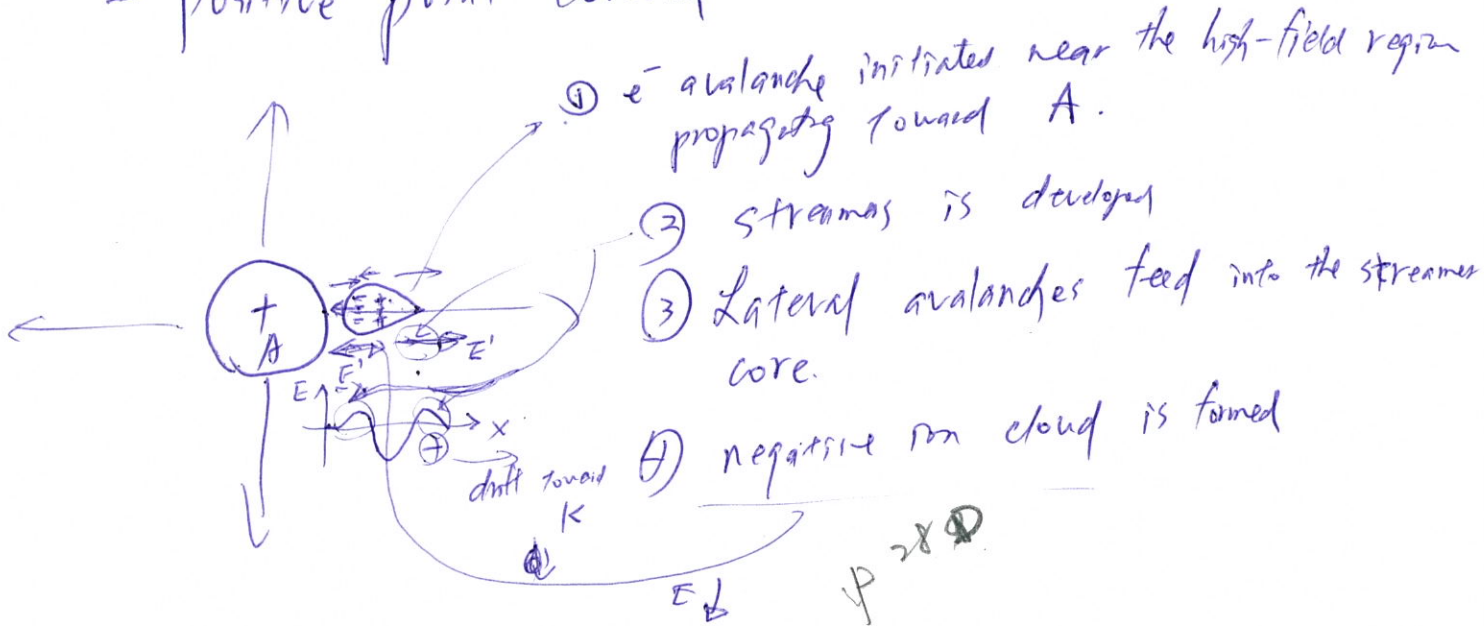
- slow down by \oplus ions behind,
- \Rightarrow attach to gas molecules forming " \ominus ions"
- \Rightarrow reduce the E field point to cathode
- \Rightarrow discharge extinguish

drift toward Anode (current)

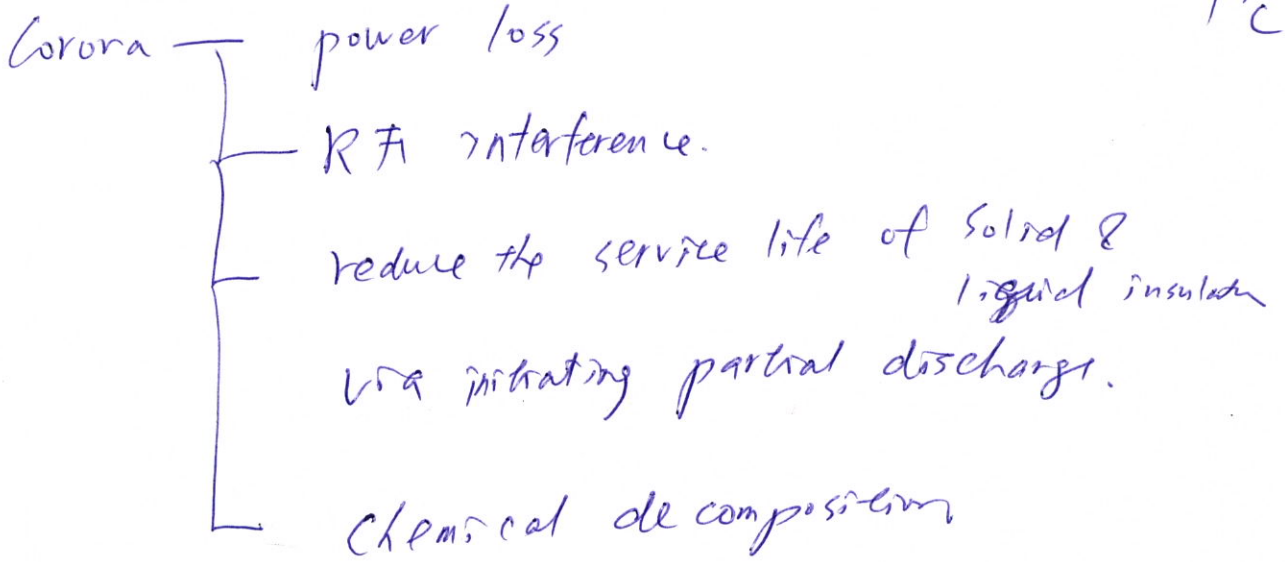
- \Rightarrow away from cathode
- \Rightarrow original E field is re-established
- \Rightarrow Another Trichel current pulse.

- Trichel pulses are regularly placed and only appear in gases exhibiting some e^- attachment, notably air & sulfur hexafluoride (SF_6)

- Positive point corona



- ① e^- avalanche initiated near the high-field region propagating toward A.
- ② streamer is developed
- ③ Lateral avalanches feed into the streamer core.
- ④ negative ion cloud is formed



↓
photo → SC

2.3 Ligands (Lecture 4)

136b
first

2.3.1 Basic Electrical Processes

* Breakdown initiation in the liquid can be divided into two categories:

- ~~bulk liquid~~
- those associated with the bulk liquid
- those occurring at the electrodes.

~ Lewis 1985, 1987, 1993, 1994a, b, c, 1996, 1998

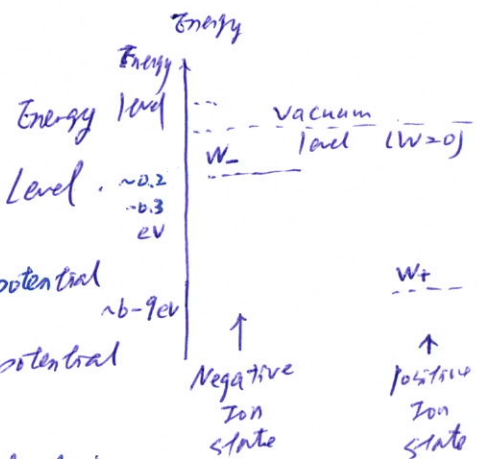
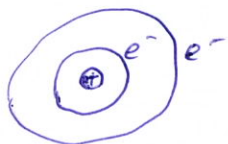
2.3.1.1 Charge in the bulk liquid can arise from

- ① molecular dissociation (分子溶解)
 - ② injection at an electrode.
- no net charge in the liquid
- leads to either an excess or a deficiency of e^- in the bulk.
- 过多
不足

* Charge transport occurs through

- ① molecular electronic state
- ② collective states of clusters of short-range order appearing in the liquid

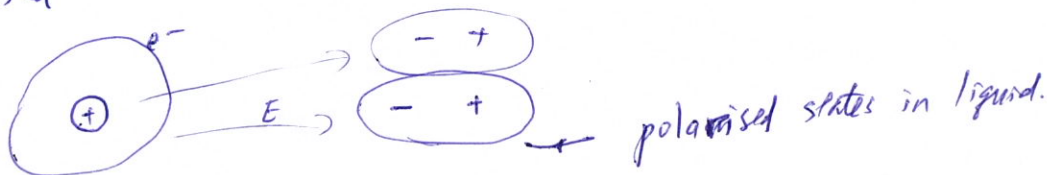
* In atom:



Positive ion state: W_+ → ionisation potential

Negative ion state: W_- → detachment potential

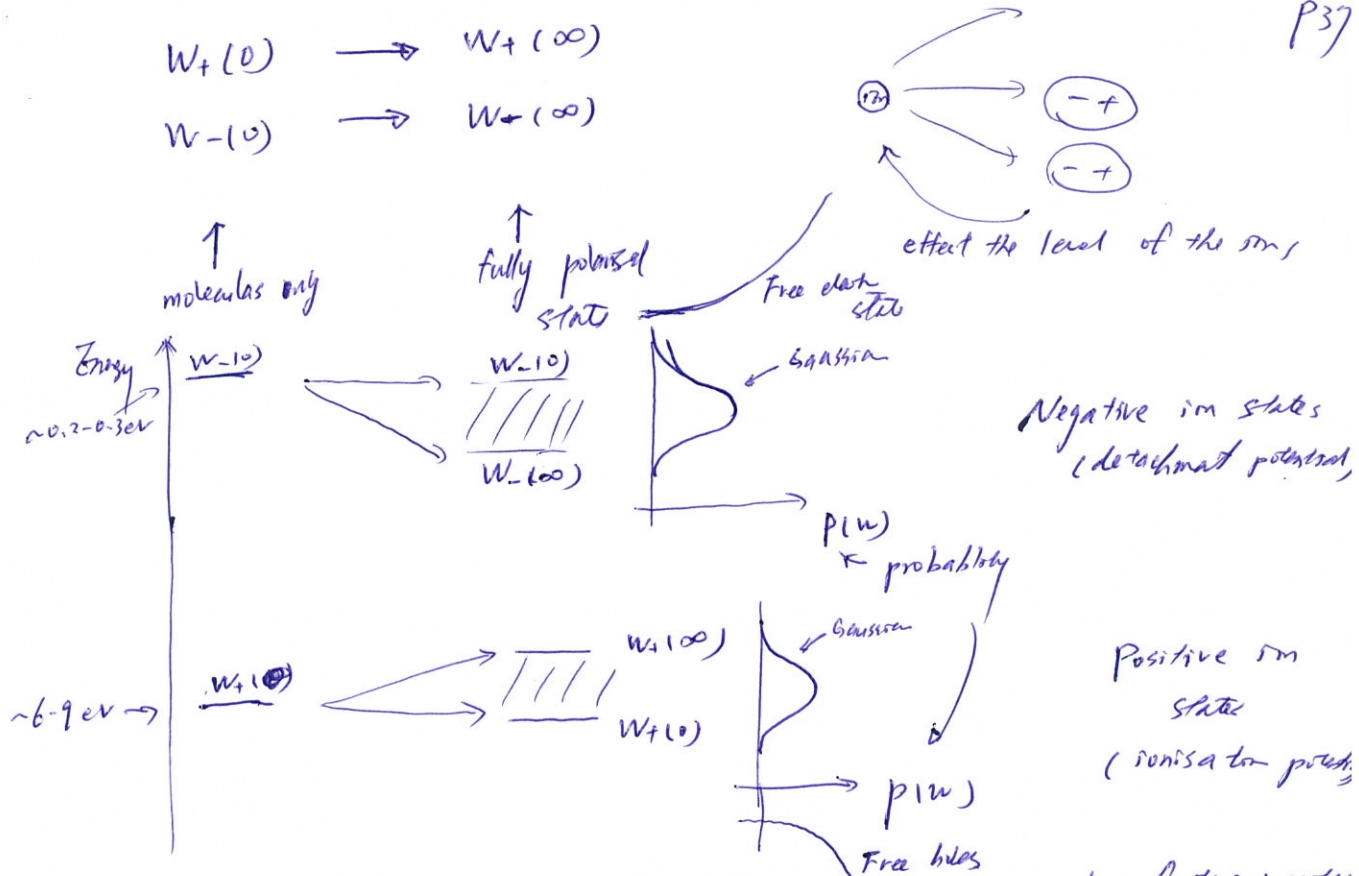
* In liquid: ionised states are modified by the collective polarisation response of the surrounding molecules, and the energy levels corresponding to the fully polarised states shift to $W_+(\infty)$ and $W_-(\infty)$, respectively.



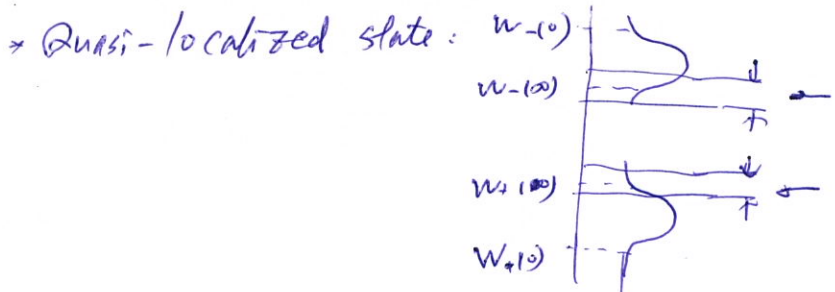
*To create an electrical discharge in liquid: P36₆

① a discharge in gas which occurs in gas bubbles that either are initially present in the liquid and on the electrodes or are formed under the action of voltage. (electrolysis, boiling, degassing of the electrode surfaces, etc.)

② a consequence of the avalanche multiplication of free ~~of~~ charge carriers in the liquid like the model in gas.



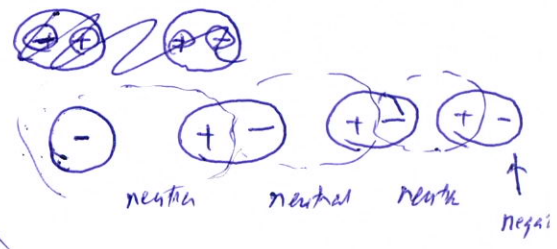
- * The energy associated to the shift " $W_{10} - W_{\infty}$ " consists of two parts:
 - 1) polarisability of the molecular orbitals
 - 2) collective dielectric response of the more remote molecules.
- * When the state of an ion changes by gaining or loss of an electron, molecular reorganisation occurs on a much slower timescale than that needed to relocate the electron.
- * (∵ thermal agitation → Gaussian distribution.)
- * Electron & hole transport in the bulk liquid can be described by a band model (of negative/positive ion states) similar to that for amorphous solids. → no crystallized structure like liquid.
- * (Excess) charge carriers can stay in
 - localised
 - quasi-localised
 - quasi-free mobile states in the conduction band.
- * Quasi-free: e^- energy $> W_{-10}$
 hole energy $< W_{+10}$
 ↳ Carriers can be considered free if they move through a sequence of states in the bands without staying long enough to induce the full electronic polarisation. → mobilities $> 10^{-3} \frac{m^2}{V \cdot sec}$



→ Electrons and holes which have become fully localised drift as ions with their accompanying polarisation shells (polarons),
 mobility $< 10^{-5} \text{ m}^2/\text{V}\cdot\text{s}$



→ Incident radiation & high electric field
 → can free the charge.



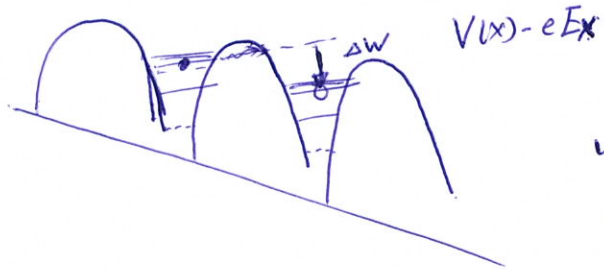
resonance tunneling



periodic potential in a molecular cluster.

existence of phonon energy → heating of the molecules along the electron path.

between quasi-local & quasi-free



High electric field:

with electric field: ΔW is predominantly dissipated as phonon energy → heating of the molecules along the electron path.

High electric fields: electron will be able to "jump over" the potential well. (hopping process) → dissipated as heat or emission of photons.

→ In the quasi-free state: the mobility of electrons (holes) is determined by scattering collisions with the liquid molecules.
 → excite vibrational modes & loss their energy from the E field



- * electron can be in quasi-free ~~states~~ ~~some time~~ & in local states
- * During transit through a liquid, electrons can thus exist for some time in quasi-free and for some time localised states.

⇒ effective mobility:

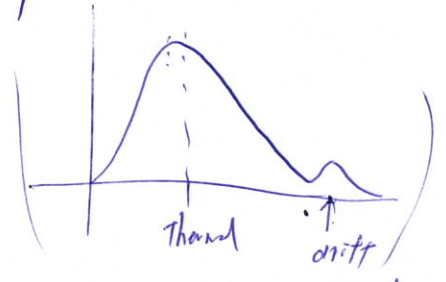
$$\mu_{eff} = \frac{\mu_f t_f + \mu_t t_t}{t_f + t_t}$$

t_f : free state
 t_t : trapped state
 μ : mobility

$t_t = t_0 \exp\left(\frac{E_t}{kT}\right)$ = the time in the trap is determined by the thermal activation energy E_t necessary to liberate the electrons.
 ↑
 reciprocal of an attempt-to-escape frequency?
 For hydrocarbons: $E_t \sim 0.24 \text{ eV}$.

- * With high E field ⇒ $t_t \downarrow$
- * Most of the time, electron transit in conduction band
 ⇒ drift velocity ~~is~~ is limited by collision process (as mentioned in the last page)
- * At very high field ⇒ drift velocity > thermal velocity

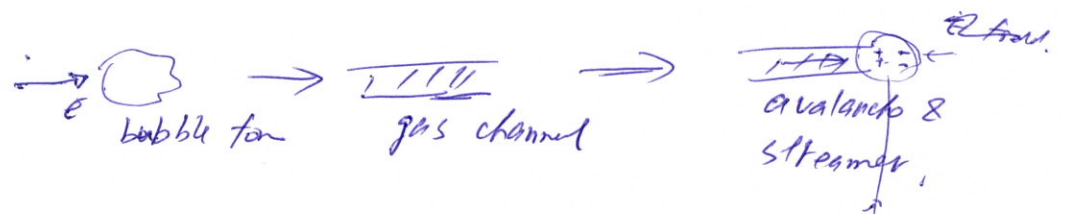
⇒ energy acquisition from the field can become quite high
 In hydrocarbon (ex: H₂), the rate is 10^{14} eV/sec



- ⇒ energy is dissipated by stimulating various molecular vibrational modes with typical quantum energies $h\nu$ of a few tens of an eV
- ⇒ $E_{k,de} > h\nu$ ⇒ cross-section for inelastic collisions ~~is~~
 drops rapidly ⇒ electron can gain sufficient energy to excite the next mode in terms of energy, up to molecular dissociation and ionisation.
- ⇒ Ionisation is very important in the context of breakdown, since it generates a second electrons and a positive ion or hole and an avalanche can build up in the liquid.

* ~ 100 meV is needed to heat the liquid to its boiling point \Rightarrow a region of low density (RLD) may have been created before avalanching occurs in the liquid & normal density

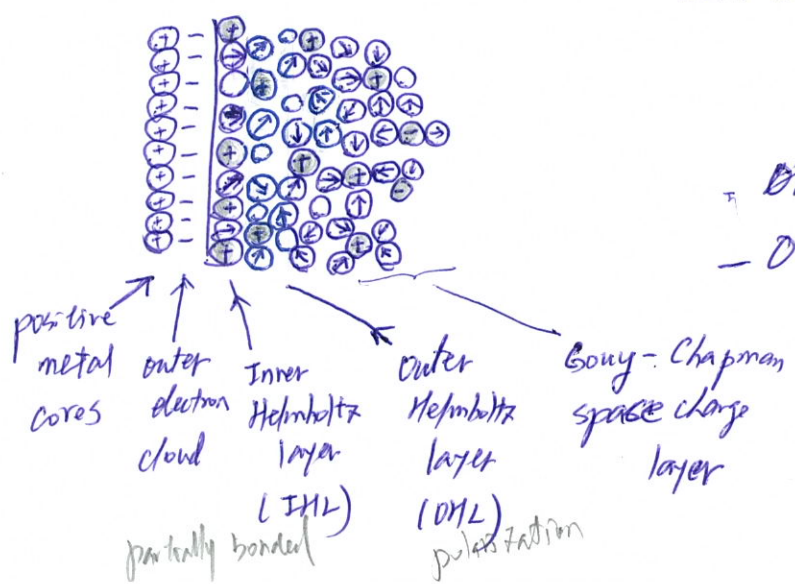
\Rightarrow In RLD, electron avalanches can build up at much lower electric field \Rightarrow ~~can~~ form a growing gas channel \Rightarrow starting point of a streamer similar in gases



* The reported hole mobilities in liquid are typically a factor of 10 smaller than the electron mobility at equal field strength.
 self-propagate of the channel. \leftarrow E field is very high in the streamer head

2.3-1.2 Electrode Processes

- * Electrode processes play a dominant role in the initiation of breakdown in liquid
- * Excess electrons (or holes) may be injected from metallic electrodes into the liquid.
- * metal - dielectric interface

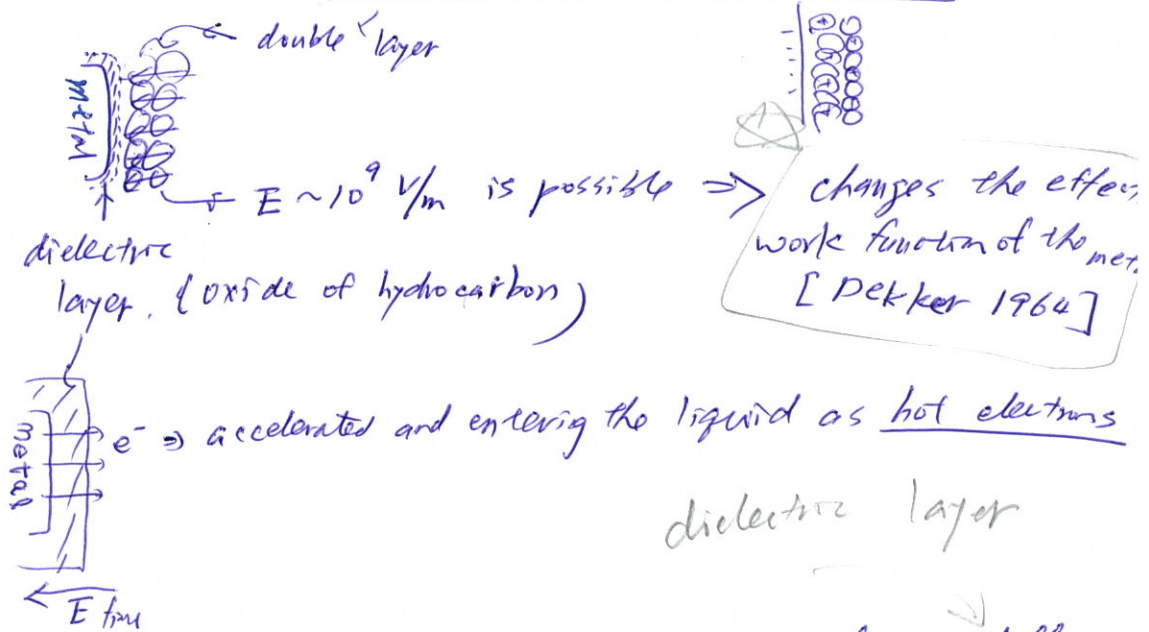


- IHL: a monolayer of ions and molecules chemically or physically bonded. \rightarrow very different from bulk liquid

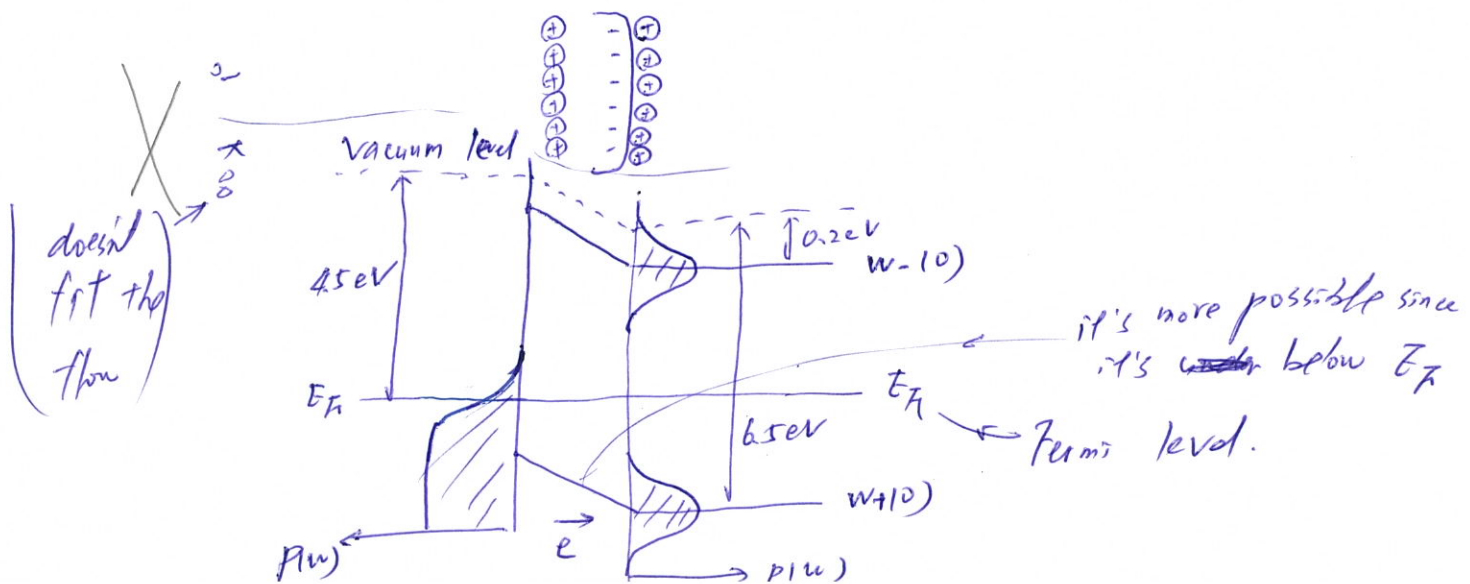
- OHL: ions approach the equilibrium polarization in the bulk liquid.

- Gouy-Chapman space-charge layer - a diffuse region. [14]
- the ions attracted into the Helmholtz layers are not sufficient to compensate all of the charge on the electrode, and the residual E field results in an additional charged layer. → may extend far into the liquid with low ion.

* IML → may become double layer if the ions moving to the surface are not neutralized immediately.

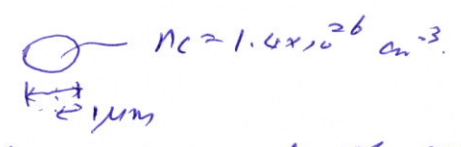


* If the charge transfer through the metal interface is difficult, ions can not be neutralized at the electrodes, the electrodes will become increasingly polarized. → increase in the resistance of the overall system ??



* Less energy is required to expand the nucleation site to a critical size with sufficient low density ($n < n_c$) such that electron impact ionisation can take place and a gas streamer can grow to the critical size.

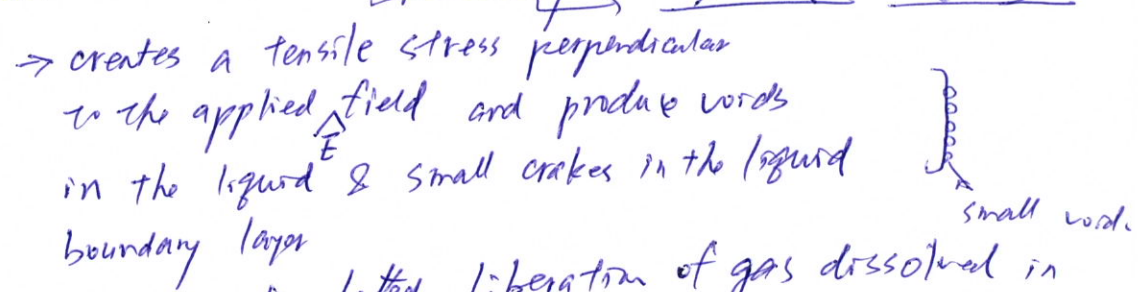
For water, ~~$r_c = 10^{-6} m$~~ , $n_c = 1.4 \times 10^{26} m^{-3}$



* It's still unclear how the large electron density can be injected to achieve the ~~super~~ required superheat.

* An unrealistically large local field enhancement seems necessary to deliver the necessary electron tunnel current.

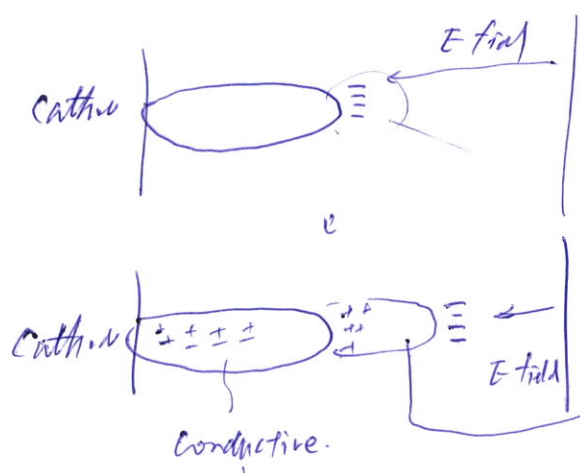
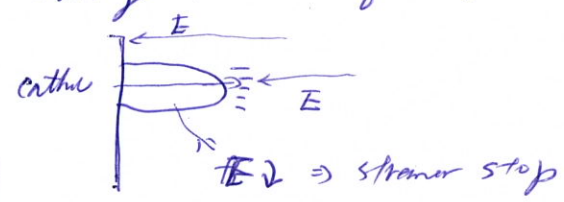
- Scenario 1: electrocapillarity



- Scenario 2: stimulated liberation of gas dissolved in the liquid.

\rightarrow preferentially at rough surfaces with cracks

* Streamer can stop because of the build-up of a negative space charge in the liquid ~~at~~ front of the space



* Electron can be accelerated toward to the streamer tip into the liquid \Rightarrow form a new space charge and start another heating and evaporation cycle.

if it's heated and become a region of low density before the space charge build up \Rightarrow streamer die.

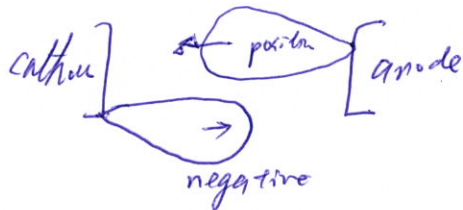
It helps maintaining the potential at the front closed to electrode by causing streamer die.

7.2.2.7 streamer breakdown

px2

→ ~~to~~ insure from power point.

- * Positive and negative streamers propagate towards the cathode and anode respectively

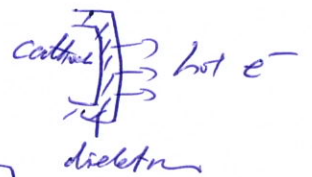


- * Schlieren diagnostics have shown that a streamer consists of a gaseous phase → breakdown strength should increase with pressure ← gas is not formed easily
- * Temperature has a minor effect.

7.2.3.2.1 Cathode initiation (negative streamer)

- * Primary process for the initiation of a negative streamer is the injection of hot electrons into the liquid.

- ① dielectric (oxide) emission



② metallic microprotrusion.

↳ A) on the electrode surface $\frac{1}{2} \mu$

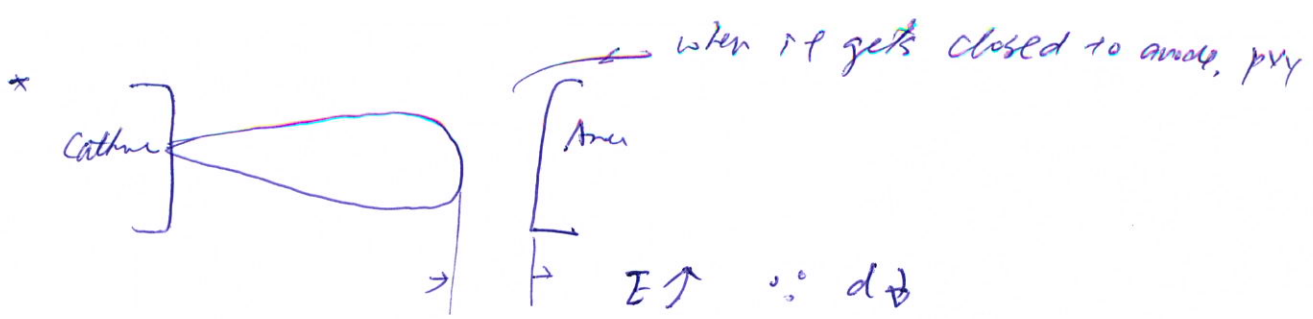
↳ B) contaminant particle in the liquid.

← most of the cases

- * If sufficiently large electron current density is injected into the liquid, a gas bubble of critical size & density may form at the electrode surface.

→ $> 10^9 \text{ J/m}^3$ (for water) must be deposited adiabatically in the liquid to create enough superheating

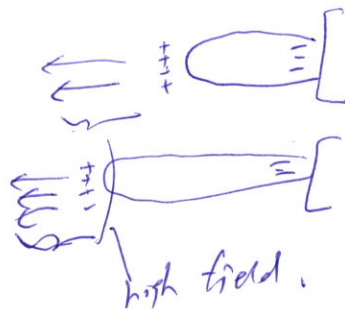
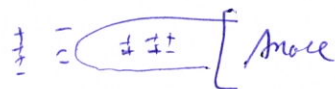
[Jones and Kunhardt, 1995]



⇒ ~~case~~ initiate a secondary or tertiary streamer.

7.2.3.2.2 Anode initiation (positive streamer)

- * Initiated by hole injection from an oxide microregion on the anode surface.
 - liquid-metal interface
 - ↳ liquid-plasma boundary of a streamer.
- * Liberation of electrons from traps, quasi-localised states, or molecules with a low ionisation potential through field ionisation in the vicinity of a microprotrusion on the anode.



7.2.3.2.2 Water:

- * Important dielectric liquid in pulsed-power applications
 - ✓ - High electric breakdown strength (up to 3×10^7 V/m) for μ s electric stress
 - ✓ - High permittivity \rightarrow store large energy densities for short time.
 - water molecules \rightarrow simple structure,
 - ↳ intramolecular electron transport is unimportant
 - possess large dipole moment
 - property ③ metal-liquid boundary layer \approx bulk liquid

- much greater density for the 1st layer than in bulk water p. 5
 - ⇒ strong impact on electron transfer
 - ⇒ — — — the formation of gaps in the boundary layer due to electrocapillarity
- ~~small~~ small fraction ($\sim 10^{-7}$) dissociated into H^+ & OH^-
 - ⇒ a residual conductivity $4 \times 10^{-6} \text{ S/m}$
 - ⇒ Inadequate for DC-insulation
 - ↳ ionic currents do not contribute to the initiation of breakdown for submicrosecond pulses.
- ✓ can dissolve a lot of gases (N_2, O_2, CO_2) ⇒ lead to formation of gas bubbles and thus facilitate the appearance of a streamer.
- ✓ pressure ↑ ⇒ dynamic breakdown strength ↑
- ✓ time lag to breakdown ~~is~~ ~~water~~ in "doubly distilled ~~water~~ water" without gas ↑ 50%

* Transformer oil for insulation: (insulating)

- The natural moistening of insulating oils does not change their pulsed electric strength at voltage action times of 10^{-8} s even if the dc breakdown voltage changes three times!!
- Requirements to the purity of the insulating liquids used in pulsed power systems can be moderated.

Q. 2.4 Solids

The phenomenon of dielectric breakdown in solids is linked inseparably to the progressive destruction of the dielectric medium by electronic or ionic charge carriers that have acquired sufficient energy from the electric field.

Insulator material	Dielectric constant ϵ	Breakdown strength (MV/m) kV/cm
Air	1	3.0
Kapton	3.6	275
Mylar	2.5	200-20
Polyethylene (PE, 聚乙烯)	2.2	127 12.7
Polypropylene (PP, 聚丙烯)	2.5	32.8 32.8
Poly sulphone (聚砜)	3.1	31.5 31.5
Pyrex glass	4-6	20
SF ₆	1.0	8 (per atm)
Teflon	2.0	59
Transformer oil	2.2	10-40
Water	80	20 (for $t < 10 \mu s$)

* Strong binding energies in solid \sim several eV
 impact ionisation $10 - 20$ eV.

Solid insulators : Breakdown strength ~ 100 MV/m.

*

$$\frac{12 \text{ eV}}{100 \text{ MV/m}} = 0.1 \mu\text{m}$$

distance between \Rightarrow electron gain 10 eV in a field of 100 MV/m

\Rightarrow distance between ^{required MFP} $0.1 \sim 1 \mu\text{m}$ each collision (mean free path) such that electron can gain 10 eV of energy in a field of 100 MV/m

Typically, mean free path of $0.1 \sim 1 \mu\text{m}$ is required to ~~break~~ break bonds and ionise material at the observed breakdown field strength.

* The chance of inducing electron avalanches in 2D or 1D lattices such as those of polymers is very small.

* * Damage can be done only if either the damage threshold is reduced or electrons are allowed to move over significantly longer free paths.

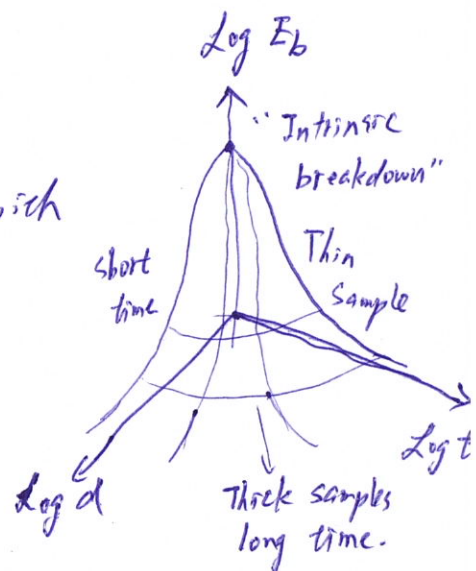
- * Magnitude of the breakdown field depend on:
 - time dependence of the electric field.
 - geometry of the sample.
 - nature of the electrode.

- * Breakdown strength reduces ~~with~~ with
 - increasing thickness
 - longer time

* "Intrinsic" breakdown strength is where the material is without defects & without external influences.

$\sim 2-3$ orders of magnitude above the design stress in technological application.

* Breakdown strength is temperature-independent in most insulating materials, but drops drastically after critical temp. between cryogenic temp & critical temp.

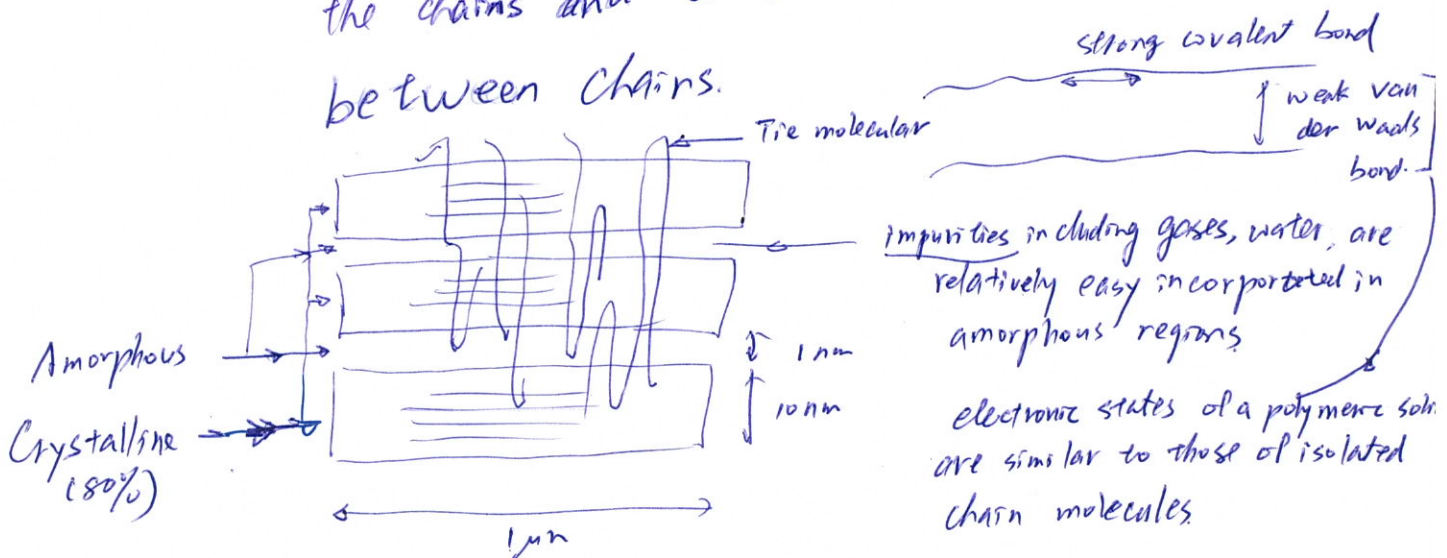


- * The final result of a breakdown is always the formation of a narrow plasma channel.
- * Electroniz charge carrier injection from the electrodes accelerates the breakdown.
- * The presence of macroscopic defects in the material (e.g. void or conducting inclusions) shorten the time to breakdown.
- * The ageing of the electric strength of a material is strongly affected by charge carrier injection & trapping.
- * Damage is done continuously to the material prior to the onset of the final breakdown.
- * Electrical breakdown must at least ~~start~~ begin at a molecular level →
 - charge transport
 - charge injection
 - breakdown.

q. 2.4.2-1. Charge transport.

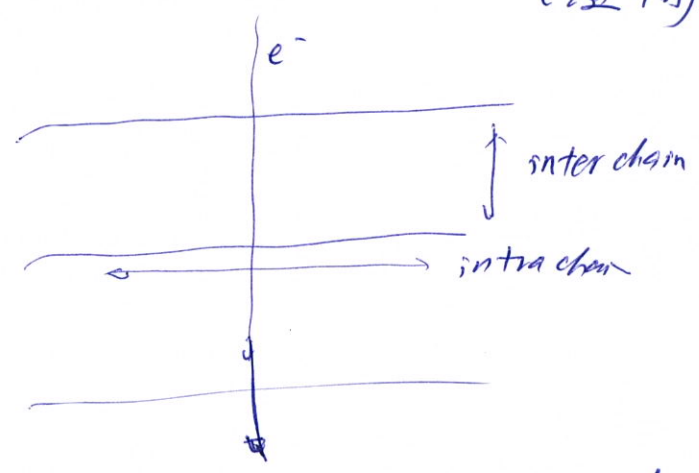
- * The most important solid insulators in pulsed-power technology are organic polymeric dielectrics such as polyethylene (PE) or cast epoxy.

→ long-chain molecules with strong covalent bonding in the chains and weak Van der Waals bonding between chains.

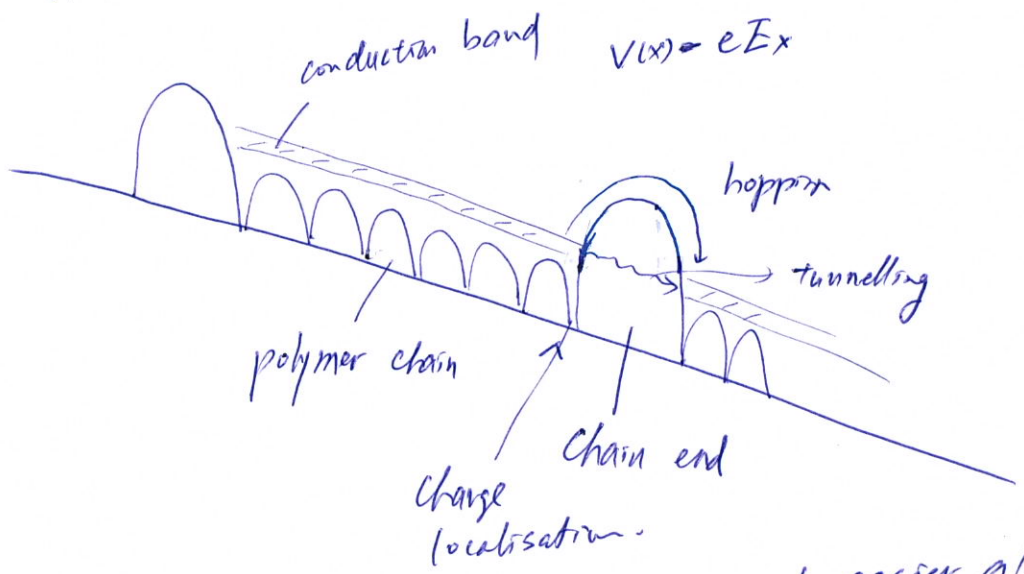


(x) Free-electron transport will follow interchain rather than intrachain (全運問)

(全運問)
Contact??



→ Electrons will move in the ~~periodic~~ periodic potential along chain surface.



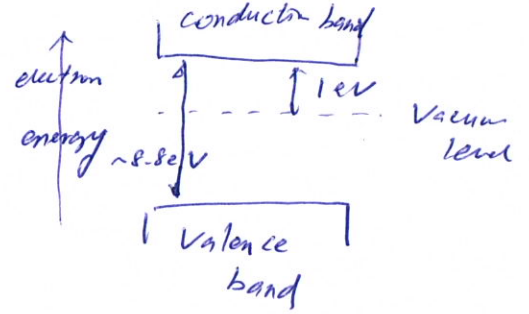
× ~~Electrons~~ Free electrons & Holes transport easier along chains that happen to lie in the field direction.
Chain ends, folds, kinks, and branching will interrupt the periodicity and lead to charge localisation.

→ hopping & tunnelling.

× electrons & holes can become trapped at dopant impurities.

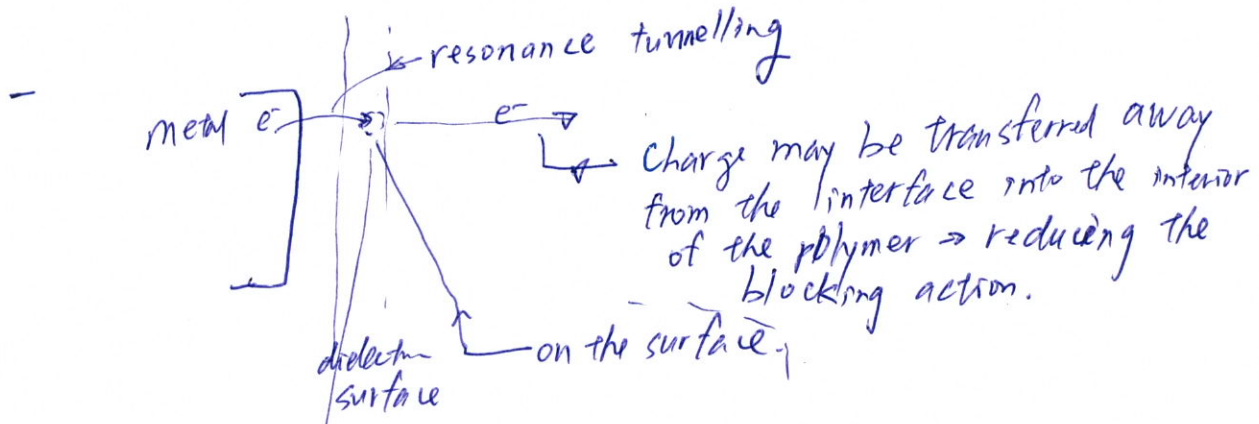
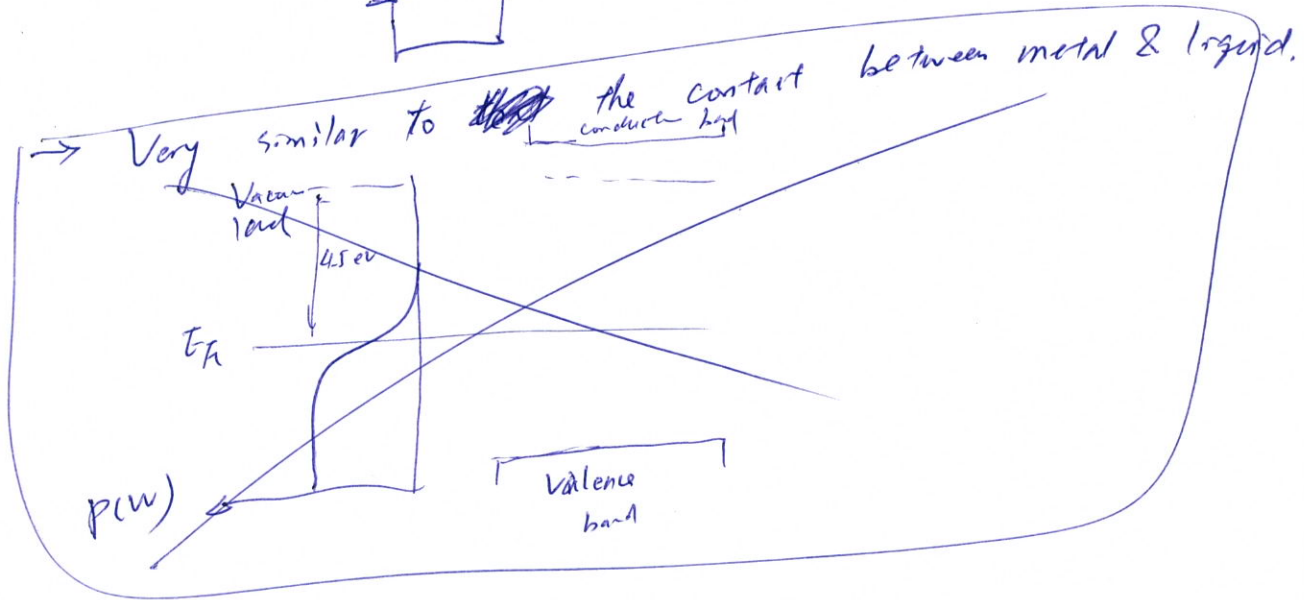
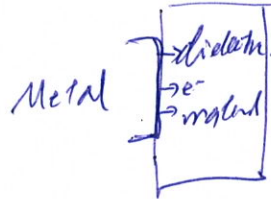
7.4.2.2 Metal - Dielectric Contact.

* The large band gap of insulating polymers ($> 8 \text{ eV}$) makes it very unlikely that mobile charge carriers can be created thermally.



→ appropriate dopants or by injection of electron or holes from metallic electrodes.

→ A metal electrode in contact with a dielectric solid will transfer charge into the solid.



If the charge remains at surface states, further tunnelling will stop and current flow across the surface will become blocked.

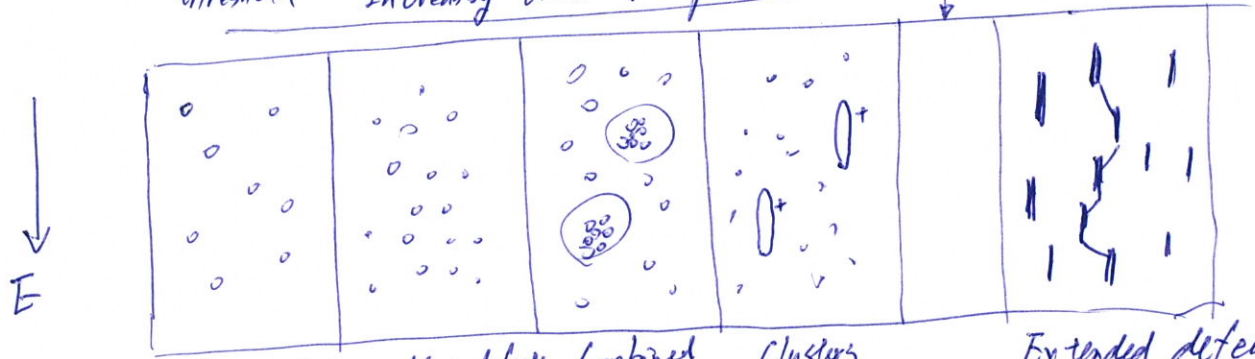
* At even ~~larger~~ larger electric field
 → electrons can reach excited states.
 → Decay from excited states will remove the energy from electrons to the molecular and heat it

* At the highest fields
 → electrons can reach the band of extended conduction states.
 → energy-dissipating mechanism becomes scattering from lattice vibrations → kinetic energies sufficient for ionisation can be reached.

* Note that it is still restricted that the chain is parallel to the field direction.

2.4.2.3 Breakdown.

* Electrons and holes injected from metal electrodes or liberated from shallow traps and subsequently stored in states can concentrate significant energy densities.
 Field below threshold Field above threshold
 Increasing time of exposure to field above threshold



Equilibrium between defect creation and healing

New defects form faster than they disappear

Combined time-field action leads to the formation of clusters

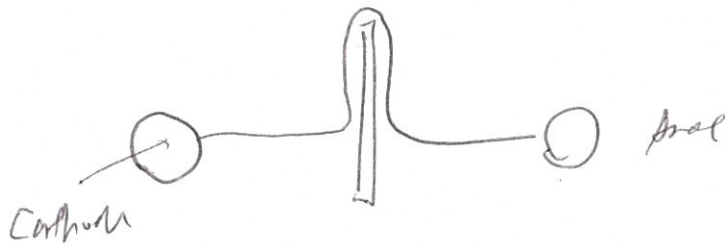
Clusters extend in field direction
 Focusing due to charge build-up

Extended defects align to form a breakdown channel.

7.

Flashover of solid dielectric

part a

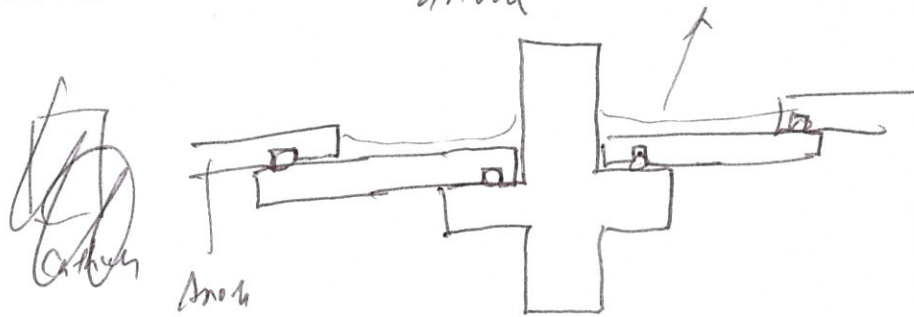


or



Flashover:

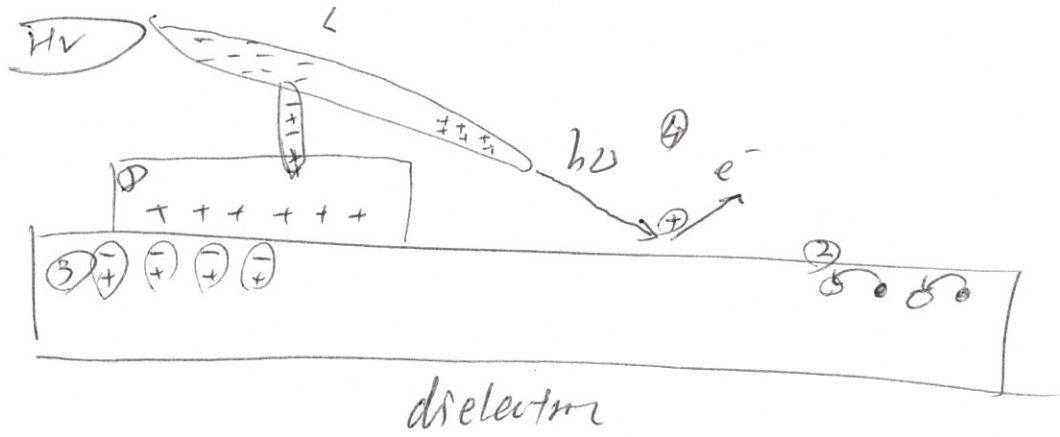
or



or

→ Charge carriers formation near the dielectric.
 → Surface can be a source for the discharge plasma.

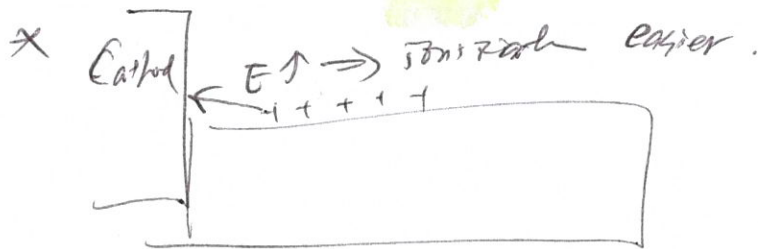
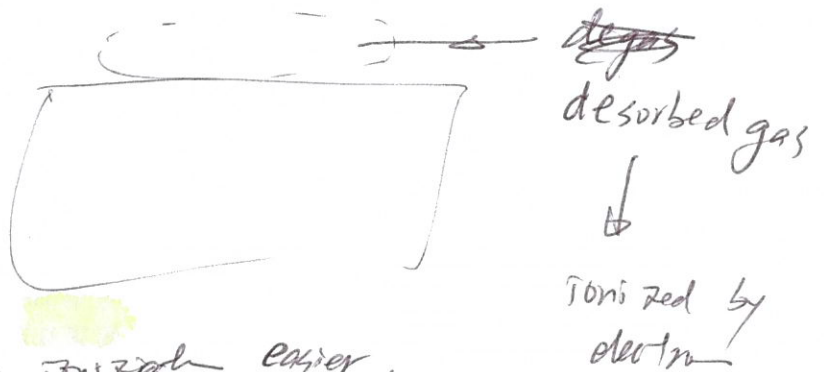
→ Generality of mechanisms of surface discharges in different mediums is in interaction of sparks and streamers w/ the surface of dielectrics



1. surface charge
2. surface conductivity
3. polarization of the insulator
4. photoemission & thermionic emission

* 2nd electron emission from the di-electric surface \rightarrow surface is (+)

* degas:



7 Breakdown in solid.

- Solid insulators function as mechanical supports, enclosures, and feed through.
- Thin films of solid insulation are used in energy storage capacitors & pulse-forming line (PFLs) for high energy density storage, and advances in metallized films w/ their self-healing properties are revolutionary.
- Common solid film insulators: polyethylene terephthalate
paper, polypropylene (PP), Mylar (PET),
& Kapton (polyimide), Teflon, Acrylic, polyvinylidene fluoride ~~PPV~~ (PVDF)
• Outdoor installations: operate in humid & polluted environment.
• For repetitive pulsed power systems: thermal considerations such as effective ~~tot~~ cooling becomes important.

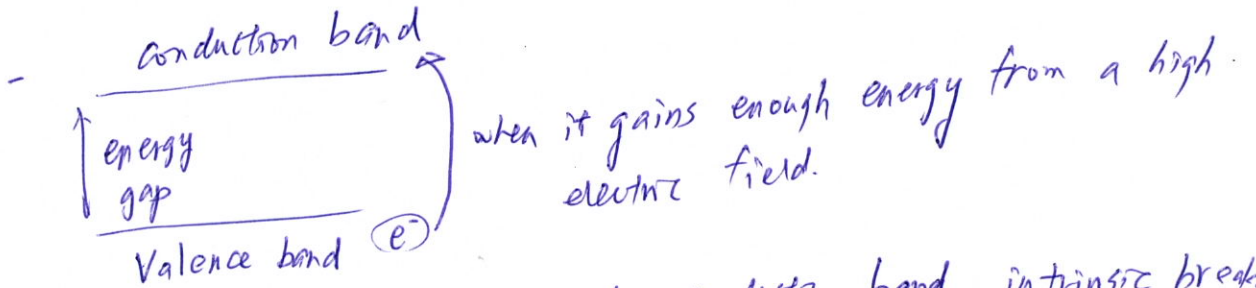
7 breakdown Mechanisms in Solids

- Solids are usually permanently damaged ~~after~~ ^{when} breakdown occurs
 - intrinsic breakdown
 - thermal breakdown
 - electromechanical breakdown
 - partial discharges
 - electrical trees

Intrinsic breakdown

- The highest values of breakdown strength when other sources of imperfections in the material and testing are eliminated.

- The timescale ~ in the order of 10 ns



- w/ sufficient e⁻ in the conduction band, intrinsic breakdown

occurs

- In the range of 5-10 MV/cm.

- In Lab.: it is measured via eliminating all imperfections:

- field non uniformity

- internal discharges from imperfections (foreign particles or voids)

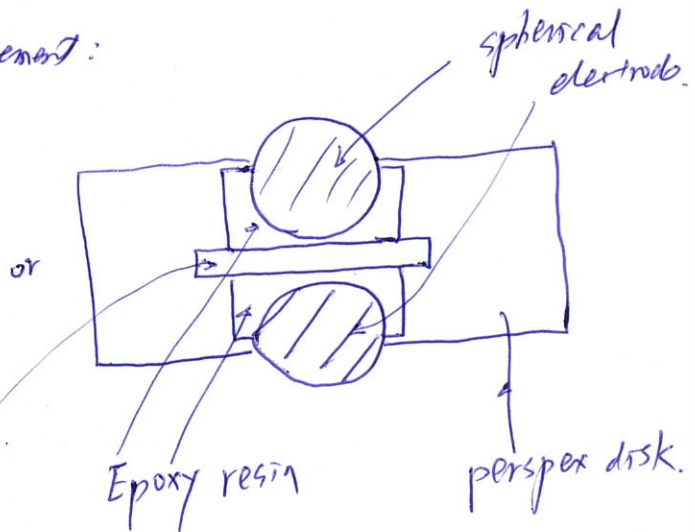
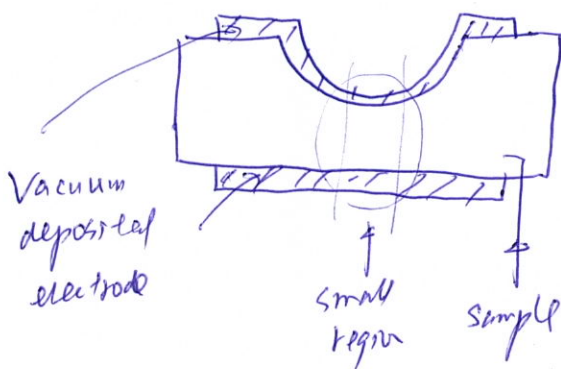
- external discharges - from weak ambient surrounding the solid dielectric.

- mechanical damage.

- field induced chemical attacks.

NOT in practical systems.

- Typical setup measurement:



- Very thin specimens of solid dielectric are used. p3
 - reasonable V ($E = V/d$)
 - probability of imperfections (foreign particles & void) ↓
- proper mechanical support is needed, to avoid electromechanical force.
- Short duration pulses w/ high voltage rising speed.
 - avoid other breakdown mechanism, such as thermal breakdown from joule heating.

• Frohlich criterion: (conduction)

If the net energy gained by an electron ~~from~~ from the electric field is greater than the energy lost to the lattice, the electron is continuously accelerated, resulting in a state of instability and intrinsic breakdown occurs.

→ does not depend on the specimen thickness or waveform, or duration of applied field.

high-energy criterion.

(Energy gain $\propto E^2$
 > Energy loss $\propto E^{-1/2}$)
 X high energy e^- dominates the breakdown

low-energy criterion.

• Avalanche criterion

Conduction electrons gain sufficient energy from the applied field to release further electrons from the lattice, similar to impact ionization in gas.

→ depends on thickness, electrode geometry
 "time to breakdown" would depend on the overvoltage applied to the specimen.

Thermal breakdown.

- happen when $\text{generating heat} > \text{dissipates rate}$
 \uparrow
 Rate of \nearrow
 due to conduction or dielectric losses (AC)
 \rightarrow depends on Voltage
 diffuse to the surrounding.
- If heat gain $>$ loss \Rightarrow thermal equilibrium is unstable.
 \Rightarrow thermal runaway. (热失控)

$$HG_{DC} = \alpha E^2 \leftarrow \text{joule heating. - DC}$$

\uparrow conductivity \nwarrow electric field

$$C_v \frac{dT}{dt} \leftarrow \text{Rate of heat accumulation.}$$

$$\frac{\partial}{\partial x} (k_m \frac{\partial T}{\partial x}) \leftarrow \text{heat lost to a surface A.}$$

$$\Rightarrow HG_{DC} = \alpha E^2 = \underbrace{C_v \frac{\partial T}{\partial t}}_{\text{heat accumulation}} + \underbrace{\frac{\partial}{\partial x} (k_m \frac{\partial T}{\partial x})}_{\text{diffusion (lost)}}$$

\uparrow source.

For AC, dielectric losses from dipole rotation. ~~heat~~ & joule heating.

$$HG_{AC} = E^2 \cdot 2\pi f \cdot \epsilon_0 \cdot \epsilon_r \cdot \tan \delta$$

\nwarrow dielectric loss tangent

$$\Rightarrow HG_{AC} = E^2 \cdot 2\pi f \cdot \epsilon_0 \cdot \epsilon_r \cdot \tan \delta = C_v \frac{\partial T}{\partial t} + \frac{\partial}{\partial x} (k_m \frac{\partial T}{\partial x})$$

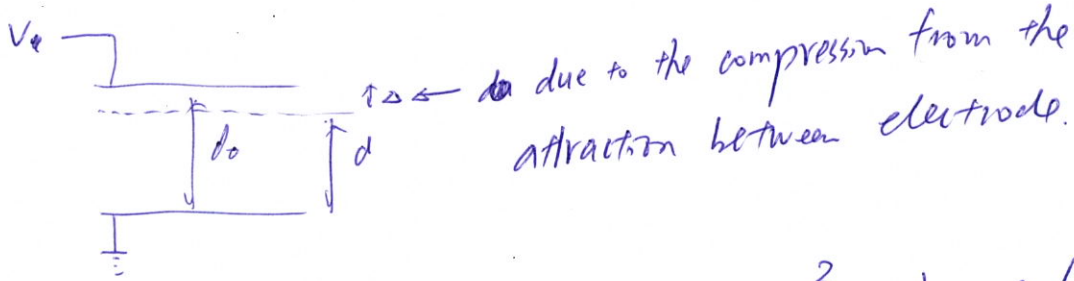
- Generally, the thermal breakdown need not be considered for DC, \because low conductivity of good insulator.
 (electric)

- For pulsed high electric field, w/ high dielectric losses $\rightarrow HG_{AC}$ is important.

Ex: Thermal breakdown @ room temperature, $\sim 10 \text{ MV/cm}$

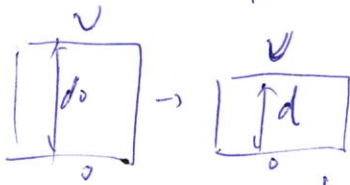
w/ $\sim 100 \text{ kV/cm}$ \leftarrow 2 order less !!

7/9 Electromechanical breakdown



compressive force: $P_c = \frac{1}{2} \epsilon_0 \epsilon_r E^2 = \frac{1}{2} \epsilon_0 \epsilon_r \left(\frac{V}{d}\right)^2$

Hooke's law: $P_c = Y \ln\left(\frac{d_0}{d}\right)$
 ↑
 young's modulus

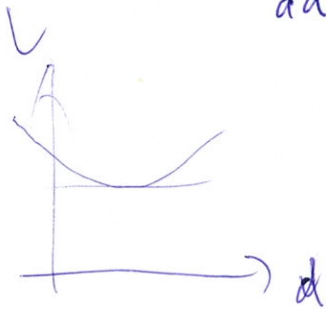


$$\Rightarrow \frac{1}{2} \epsilon_0 \epsilon_r \left(\frac{V}{d}\right)^2 = Y \ln\left(\frac{d_0}{d}\right)$$

$$V^2 = \frac{2Y}{\epsilon_0 \epsilon_r} d^2 \ln\left(\frac{d_0}{d}\right)$$

$$\frac{dV}{dd}: \quad 2V \cdot \frac{dV}{dd} = \frac{4Y}{\epsilon_0 \epsilon_r} d \ln\left(\frac{d_0}{d}\right) + \frac{2Y}{\epsilon_0 \epsilon_r} d^2 \cdot \frac{d}{d_0} \left(-\frac{d_0}{d^2}\right)$$

$$= \frac{2Y}{\epsilon_0 \epsilon_r} \left[2d \ln\left(\frac{d_0}{d}\right) - d \right]$$



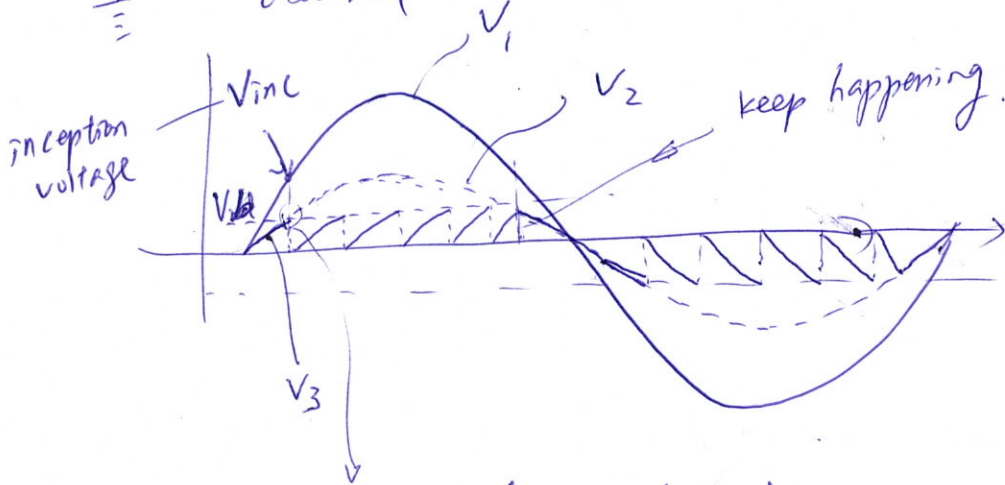
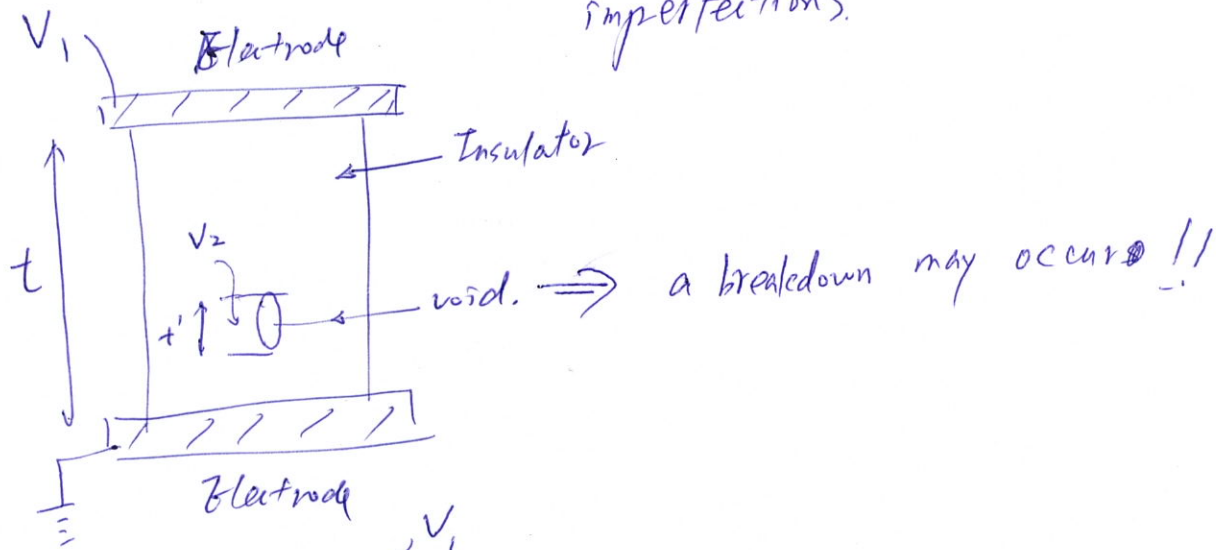
$$\Rightarrow \ln\left(\frac{d_0}{d}\right) = 0.5 \quad \Rightarrow \quad d = d_0 e^{-0.5} = \underline{0.6 d_0}$$

* $\nabla V \uparrow \Rightarrow d \downarrow \Rightarrow$ exceeds the strength of the material
 \Rightarrow mechanical damage.

Partial discharges (PD)

- A PD occurs inside voids embedded in solid dielectrics

↑
imperfections.



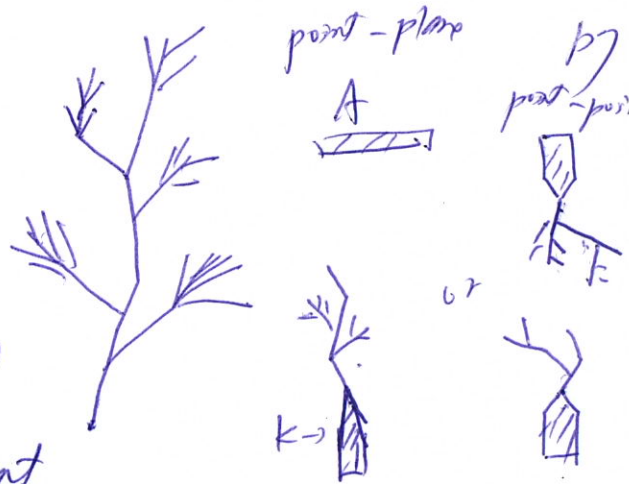
a spark forms in the void
 \Rightarrow V collapses to a low value.

V_b is determined by the Paschen curve where $d = t'$,
 p is p in the void.

- The energy dissipated in the void causes erosion, tracking, treeing and electrochemical deterioration.
- It takes a time period of years.

Electrical Trees

dry trees
water trees



- depends on the properties of dielectric & the environment.

- Over a period of time, may extend to few years, the trees cause the total breakdown.

• Dry trees: — hollow tubes, resembling the branches of trees, which are formed inside a dielectric due to electrical stress

filled w/
- diameters: $10 \sim 500 \mu\text{m}$, mixtures of gases from the decomposition of dielectric material.

- Nucleation sites (seed) — localized field enhancements, ex: asperities on electrodes, embedded foreign particles.

- Initiation: mostly due to voids, electromechanical force

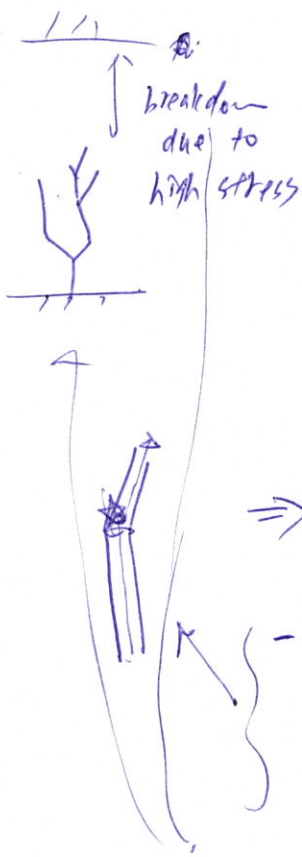
→ fissures, microscopic cracks,

⇒ ~~or~~ cause erosion, tracking, gas evolution, decomposed products.

- The accelerated charged particles impact the walls of the cavities w/ high velocities, leading to

their growth

When a tree occupy a major length of the insulator, the remaining unbridged portion of the insulator will be subjected to extremely high stresses, leading to disruptive breakdown



* Water Trees

128

- If dielectric is hydrophilic (親水) & is immersed in water \rightarrow tree channels filled w/ water.

- When electric stress is removed, water is reabsorbed in the solid dielectric, the channel becomes dry & hollow.

- The electrical conductivity of water ~~stress~~ trees compared to dry trees is high \Rightarrow rapid growth.

underground cable !!

7. Methods of improving solid insulator performance.

- layers of insulating films instead of single layer w/ the same thickness

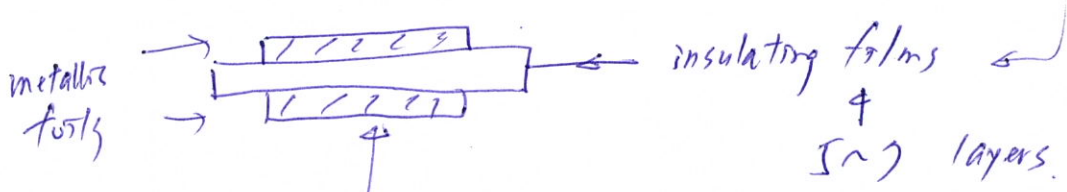
- improving the contact area @ the interface between electrodes & dielectric - metallization & oil impregnation

- controlling a nonuniform field - corona guards / equipotential rings.

- modifying insulator shapes & surface profiles.

\rightarrow reduce the interaction of charge carriers at the surface.

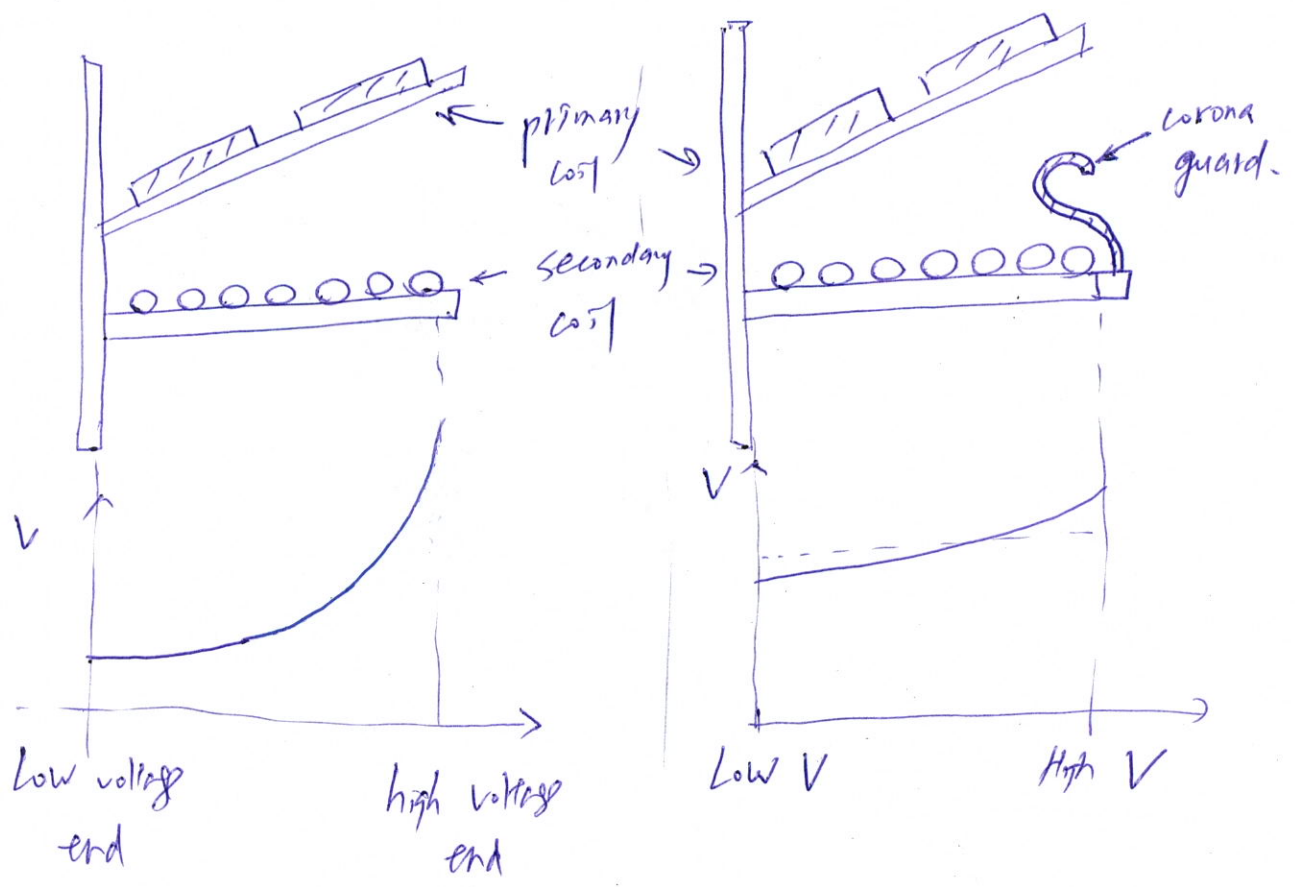
Ex: - Insulation in energy storage capacitors



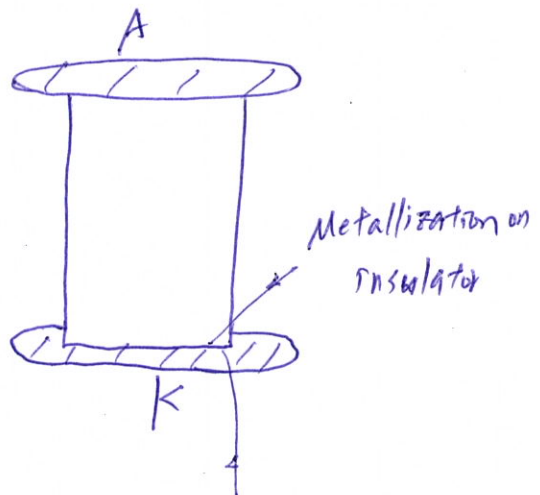
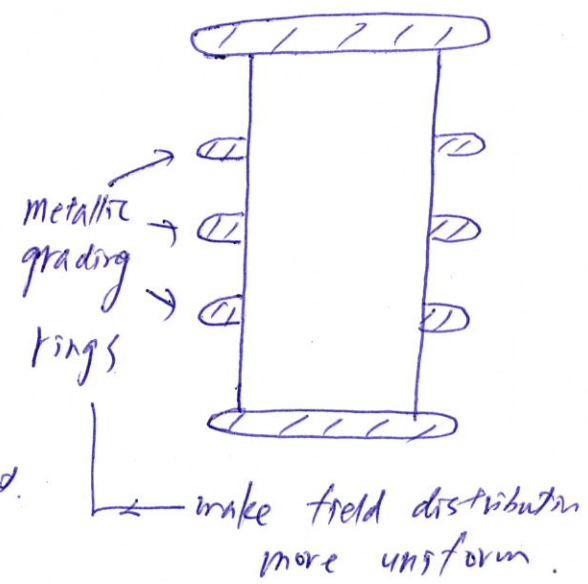
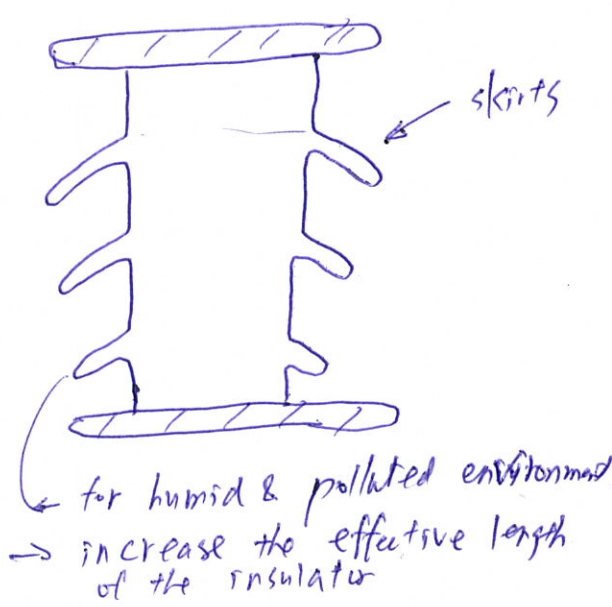
recently: use vapor deposition of Al or Zn
 $\delta = 0.0003 \mu\text{m}$

more layers can be packed \Rightarrow higher ~~the~~ energy density
 \Rightarrow metallization \rightarrow operates under higher field strength !!

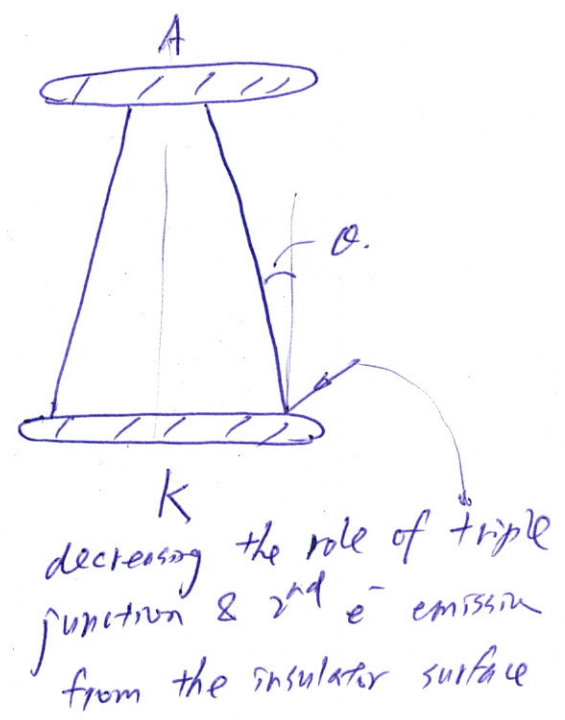
- Surge voltage distribution in a Tesla Transformer



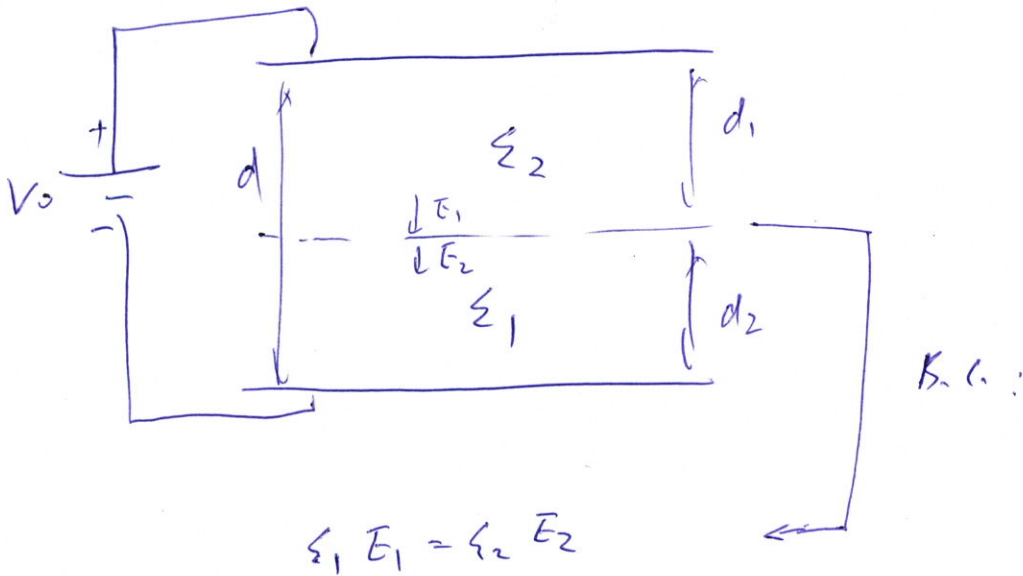
Q Surface flashover in standoff insulators



eliminating the voids & inclusions @ the surface



3 Composite dielectrics:



$$\epsilon_1 E_1 = \epsilon_2 E_2$$

$$E_1 = \frac{V_1}{d_1}, \quad E_2 = \frac{V_2}{d_2}$$

$$\left[\begin{array}{l} \epsilon_1 \frac{V_1}{d_1} = \epsilon_2 \frac{V_2}{d_2} \\ V_1 = \frac{\epsilon_2 d_1}{\epsilon_1 d_2} V_2 \end{array} \right. \quad \left. \begin{array}{l} V_0 = V_1 + V_2 \end{array} \right.$$

$$V_0 = \frac{\epsilon_2 d_1}{\epsilon_1 d_2} V_2 + V_2 = \frac{\epsilon_2 d_1 + \epsilon_1 d_2}{\epsilon_1 d_2} V_2$$

$$V_2 = V_0 \frac{\epsilon_1 d_2}{\epsilon_2 d_1 + \epsilon_1 d_2}$$

$$E_0 \equiv \frac{V_0}{d}$$

$$\left\{ \begin{array}{l} E_2 = \frac{\epsilon_1}{\epsilon_2 d_1 + \epsilon_1 d_2} V_0 = \frac{1}{d_2 + \frac{\epsilon_2}{\epsilon_1} d_1} V_0 \end{array} \right.$$

$$\left\{ \begin{array}{l} E_1 = \frac{\epsilon_2}{\epsilon_1} E_2 = \frac{\epsilon_2}{\epsilon_2 d_1 + \epsilon_1 d_2} V_0 = \frac{1}{d_1 + \frac{\epsilon_1}{\epsilon_2} d_2} V_0 \end{array} \right.$$

$$\text{if } \frac{\epsilon_2}{\epsilon_1} > 1 \quad d_1 + \frac{\epsilon_1}{\epsilon_2} d_2 < d_1 + d_2 = d$$

$$\Rightarrow \underline{E_1 > E_0}$$

3 Liquids

- "All-liquid" pulsed-power system is feasible.

Max: Oil-filled - oil/water-filled PFL
- oil or water spark gap

Max: high dielectric strength

PFL: high dielectric constant +
low conductivity

Spark gap: high thermal conductivity +
minimum decomposition products +
self-healing properties.

- properties:
1. good thermal properties.
 2. low viscosity.
 3. low flammability.
 4. good chemical & thermal stability.
 5. ~~good~~ works in low temperature.
 6. environmental considerations.
 7. low cost.

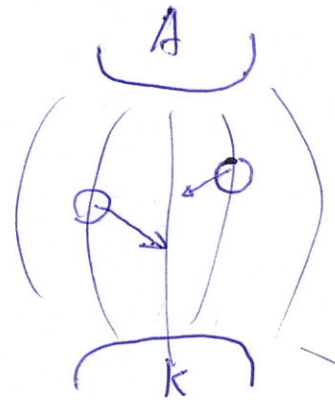
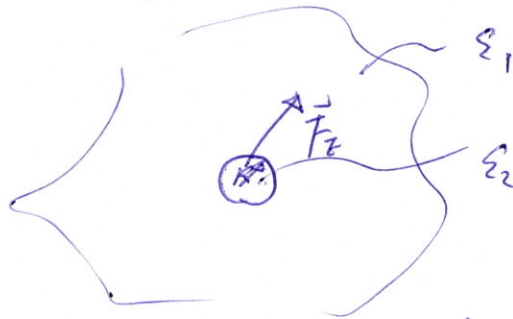
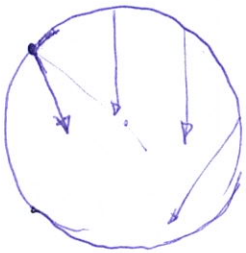
* Breakdown in liquid:

pr2

- particle alignment.
- electronic breakdown.
- Streamers in bubbles.

* particle alignment = solid impurities always exist in a liquid

- convection currents are set up in a liquid dielectric due to particle movements even at low applied voltage.

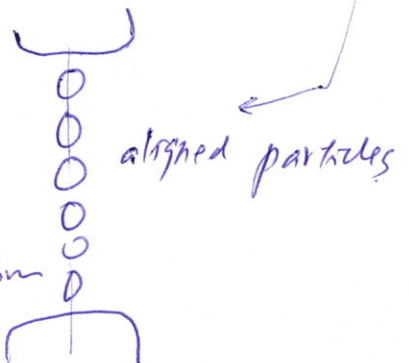


$$\vec{F}_E = \frac{\epsilon_2 - \epsilon_1}{\epsilon_1 + 2\epsilon_2} \cdot R^3 (\vec{E} \cdot \nabla \vec{E})$$

The ~~also~~ force tends to concentrate the solid impurities to the region of the center of the electrodes where the field is fairly uniform.

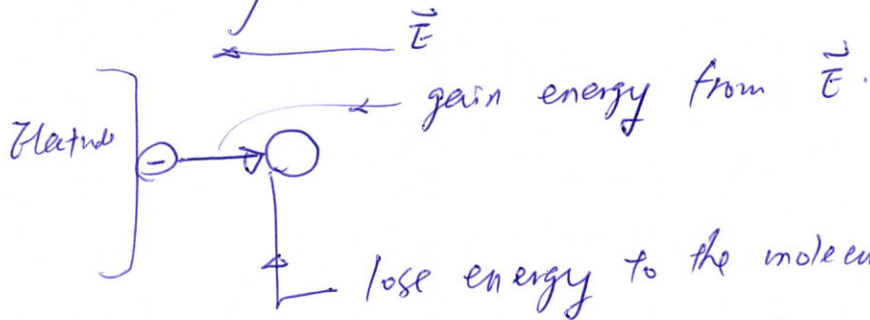
\vec{F}_D - diffusion force.

If $\vec{F}_E > \vec{F}_D$, the alignment of the particles takes place along the center of the electrode and breakdown in the liquid takes place along the aligned particles.



* Electronic breakdown.

- very similar to breakdown in gas.



"nonionizing collisions" \Rightarrow NOT possible for e^- to reach ionization energy.

- elastic, vibration, excitation process

\rightarrow At elevated temperatures & high field strength near an asperity of an electrode.

\rightarrow energy loss \downarrow

\Rightarrow continuous acceleration

\Rightarrow energy $>$ ionization energy.

\Rightarrow more e^- due to impact ionization of the molecule

\Rightarrow avalanche of $e^- \Rightarrow$ breakdown.

* Streamers in bubbles - propagation of streamers in the low-density vapor or bubbles

the process is very similar to that in gases

\Rightarrow Streamer mechanism of liquid breakdown is similar to the growth of electric trees in a solid due to discharge in a void.

low-density vapor

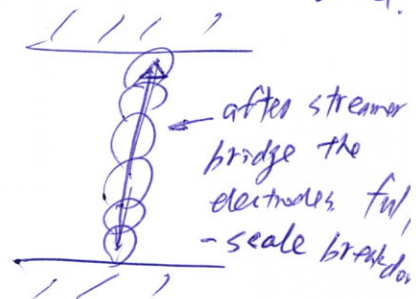


high field due to space charge

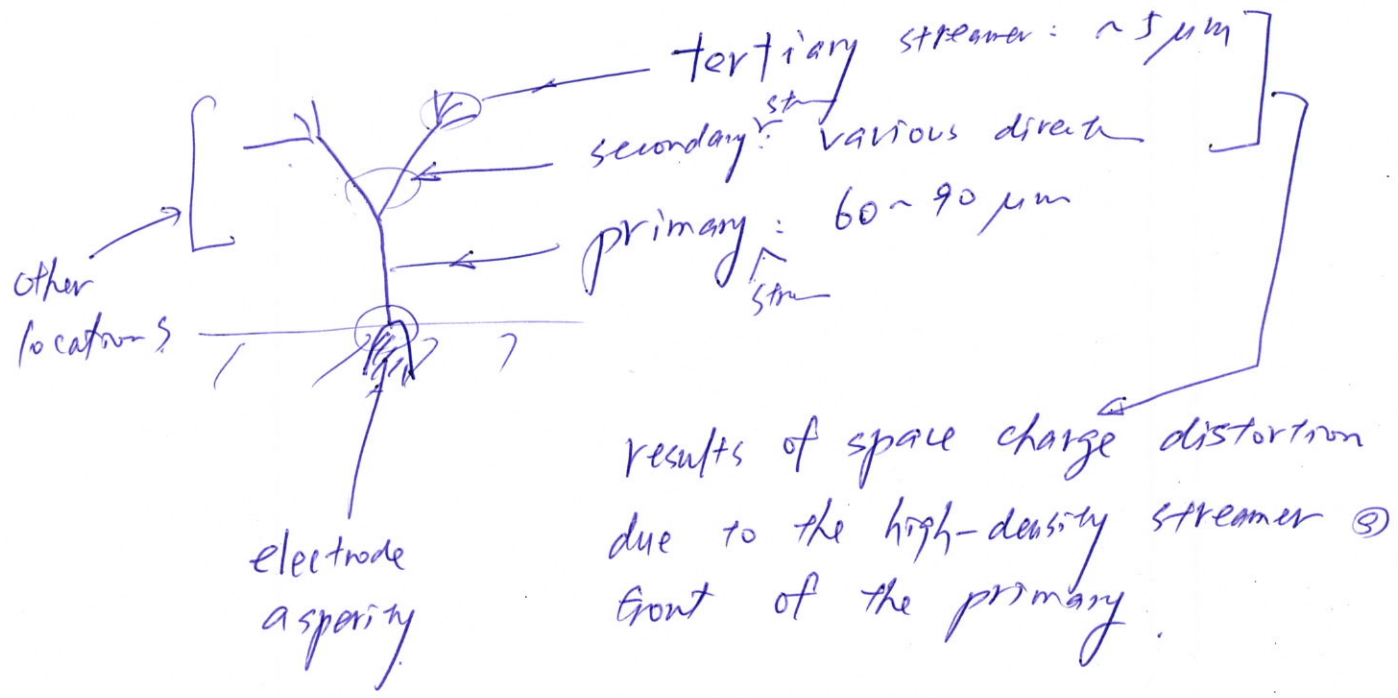
\Rightarrow shockwave & thermal dissipation

\Rightarrow more low-density vapor.

\Rightarrow more ionization



Structure.



* Effect of hydrostatic process.

= breakdown voltage \uparrow w/ $P \uparrow$

~~streamer~~ streamer grow at higher field @ $P \uparrow$

Ex: transformer oil, $V_{brak} \times 3 \sim 4$ @ 4 MPa (140 Atm)

Mechanisms of bubble formation.

- 1) foreign particles
- 2) asperities on electrode causing field emission.
- 3) chemical interaction w/ molecules causing their dissoeraton.
- 4) release of the already existing gas dissolved on the liquid.

- Krasucki's hypothesis:

- a vapor bubble grew continuously & when a critical size was reached.
- break down ~~takes~~ place.

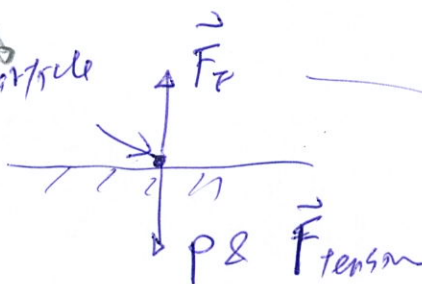
when V is gone → collapse faster than air bubble

⇒ p inside the bubble is "Zero"

- w/ impurity particles → bubble grows preferentially on the particles

→ near the electrode surface.

seed of bubble w/o particle



balance ⇒ causes a zero pressure

- $V_b \uparrow$ as $r_b \downarrow$

r_b of particle

$\gamma_s \uparrow$

surface tension

$p \uparrow$

hydrostatic pressure

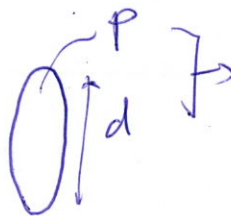
- Kao's hypothesis

- bubble once created starts elongating in the direction of the field, keeping its volume const.

$p \uparrow \Rightarrow r \downarrow$
 $\Rightarrow V_b \uparrow$



→

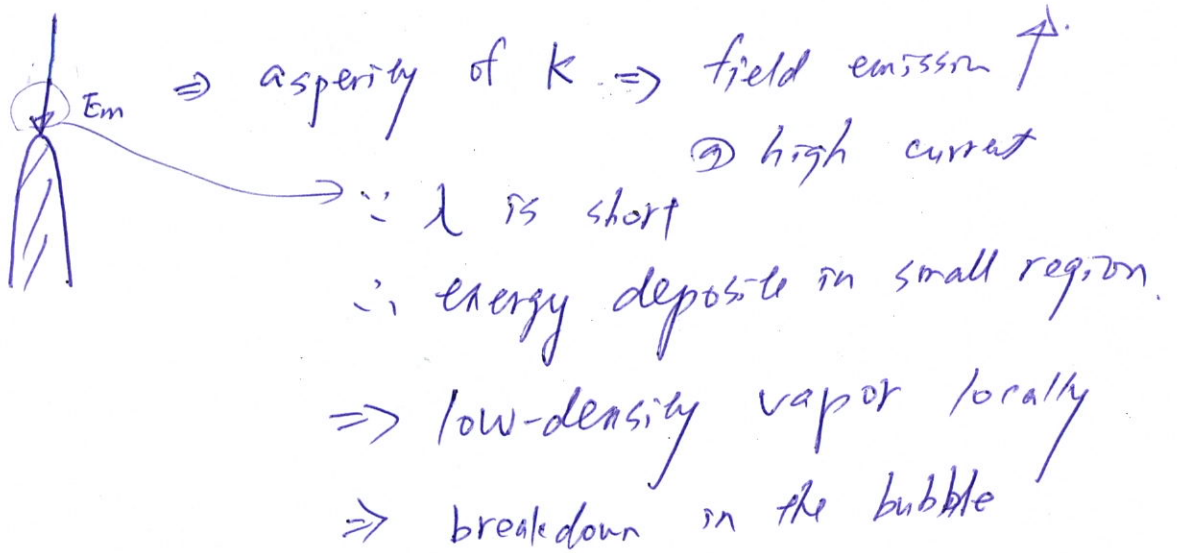


paschen curve





* Sharbaugh & Watson hypothesis



For a pulse w/ few μs \Rightarrow enough energy from field emission to vaporize a small mass of liquid ahead of an asperity into a bubble

$P \uparrow \Rightarrow$ boiling point $T_b \uparrow$
 \Rightarrow more field is required to form the bubble.

- ★ Water: (Er = 80)
- 1) high energy density. in energy storage
 - 2) low impedance in PFL
 - 3) self-healing post breakdown
 - 4) easy maintenance.
 - 5) low cost
 - 6) ease of disposal

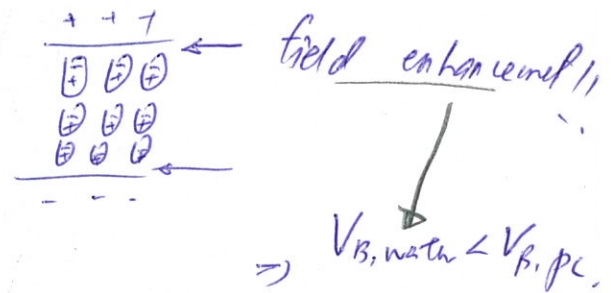
- for pulse w/ short duration (7-30ns) $P17a$
 submega volt, the E field strength
 is $\hat{\sim} \times 2$ for longer duration (30ns-1ms)

3×10^7 V/m for μs electric stress

- dependence of breakdown voltage on Polarity (?)

- E field intensification.

- enhanced field intensification at the apertures
 due to collective orientatn of the dipolar
 water molecules (3) liquid-electrode interface



- ~~For~~ water ($\epsilon_r = 80$)

propylene carbonate ($\epsilon_r = 26$)

* Methods of improving liq. dielectric performance.

- New composition:

In PFL: (vegetable oil): Castor oils ($\epsilon_r = 4.7$)
 v.s. mineral oil ($\epsilon_r = 2.4$)

sealing is important. ← hygroscopic (吸湿性)

Synthetic oil eg. PAO (poly-alpha-olefin), ^{P126}

a silicone oil \rightarrow good for closing SW.

1) resistance to oxidation.

2) lower viscosity, ok @ low temperature

3) good lubrication, ok w/ hydraulic pump

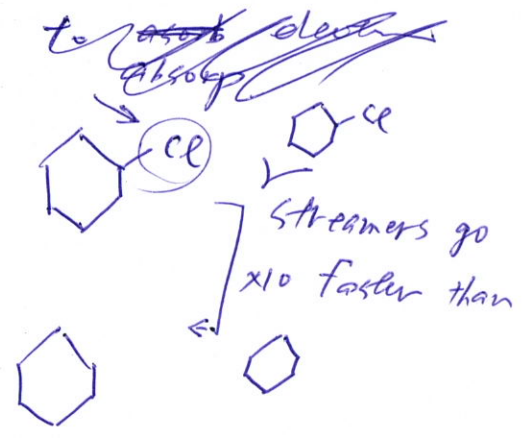
forced flow @ high P & velocity removes the gases evolved by molecular dissociation & erosion from electrodes

- Electron scavengers -

ex: chloro cyclohexane.

v.s.

cyclohexane



or add CCl_4 , more streamer !! (??)

\therefore detrapping of e^- @ high field

- Liquid mixture.

gas: $\text{SF}_6 + \text{N}_2$

solid: paper + polypropylene.

liquid: In PFL: water ($\epsilon_r = 80$)
+ ethylene glycol ($\epsilon_r = 40$)

\Rightarrow increasing intrinsic time const.

Impregnation

when putting insulating films & metallic foils in liquid dielectric:

- ① ⑤ high temperature ⇒ removal of air
- ③ ⑥ vacuum ⇒ trapped ⑥ electrode-liquid interface

Purification

- freed of foreign particles & ions
 - ⇒ filter
 - ⇒ deionizer.
- low temperature ⇒ RF
 - ↳ chiller unit.

Vacuum.

- NO medium → NO breakdown, however
- breakdown does take place ∵ charge ~~particles~~ carriers being injected
 - ⇒ desorbed gas, metal vapors from the electrode.
- "Surface flashover" across the solid insulator, the insulator surface is an electrically weaker medium than vacuum

- Ex:
- ① spark gap sw
 - ② diodes for particle beams, X-rays, microwaves
 - ③ transmission lines for feeding pulsed power into the load.

1) for $E_p = 10^8 - 10^9 \text{ V/cm}$

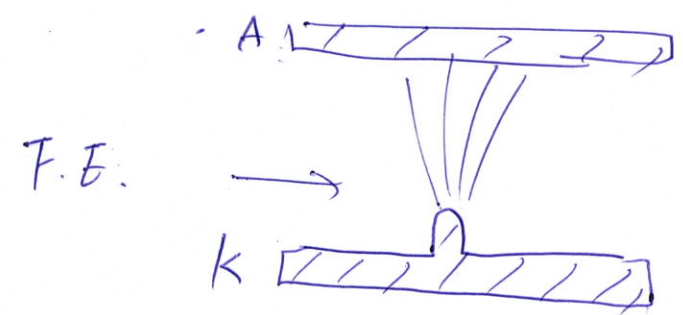
$$j_c = 10^8 - 10^{10} \text{ A/cm}^2$$

→ leads to ABCD breakdown
or other

2) $j_c \rightarrow$ joule heating of ϕ microprojection

→ melting, vaporization, plasma forming
↓
ionizat → breakdown.

3) high-energy e beam on anode
→ heating → metal vapor



4) low work function for K → high field emission

* Microparticle-initiated breakdown

- 1) loosely adhering material being detached from electrode due to electrostatic force
- 2) microprojections, made soft from joule heating by field emission
- 3) vaporization of anode
- 4) Cathode

7 Improving vacuum insulation performance

- conditioning:

~~conditioned breakdown~~

w/ successive breakdown events, the breakdown voltage steadily increases ~~until~~ and attains a steady value

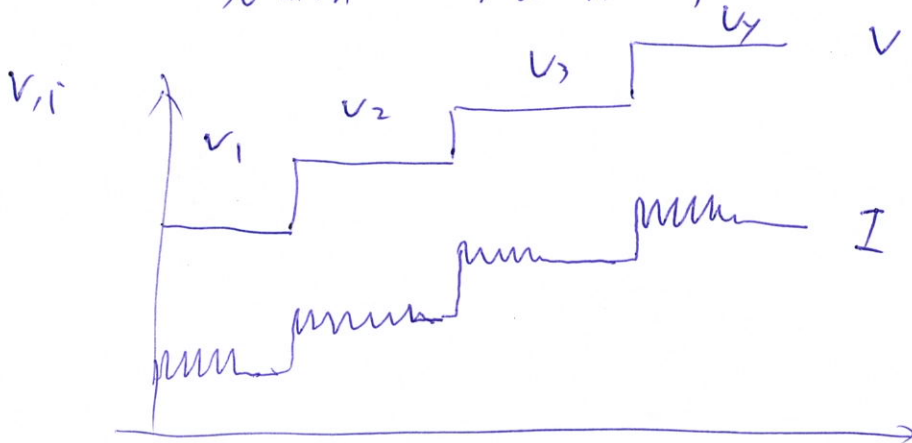
* Current conditioning:

~~current~~

- $I \sim 100 \mu A$

- A breakdown pulse removes a microprojection and the following pulse shifts to another microprojection site.

- 30 min ~ few hours



- AC / DC, start from 50% of expected V_b .
for both electrode.

* spark conditioning

Impulse voltages w/ width of 100s ns is used,

$I \leq$ few A.

- Chemical cleaning $\left\{ \begin{array}{l} \text{reducing impurities} \\ \text{valence band } e^- \text{ energy} \\ \text{is changed} \end{array} \right.$

- Residual stresses are changed \rightarrow hardened work

* Glow discharge cleaning

- H, He, Ar, N₂, SF₆, dry air

- sputter-cleaning

- a continuous flow of gas allowed the removal of impurities

- 30-60 mins using \swarrow , then use Ar to remove O₂.

* Outgassing & annealing

- heaty to $T = 250 \sim 1500^\circ\text{C}$ for several hours for outgassing.

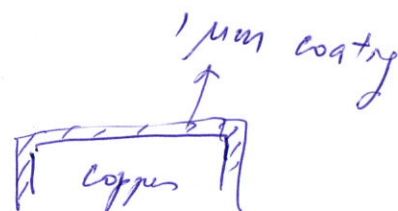
* Surface treatment & coating.

- cobalt-molybdenum

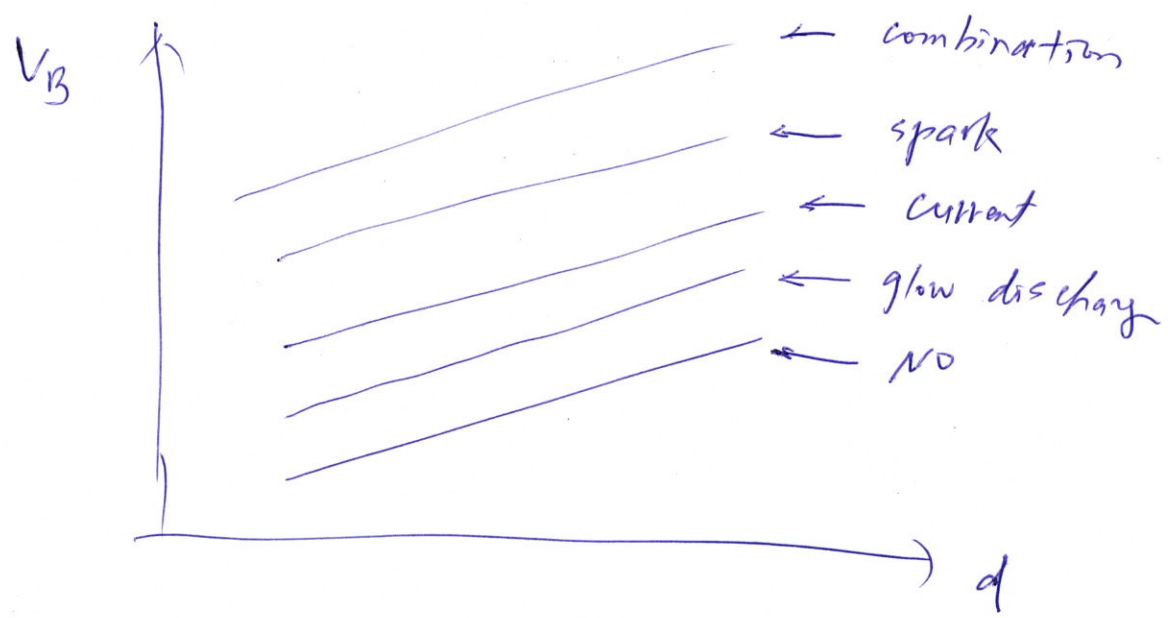
钴 钼

cobalt-tungsten

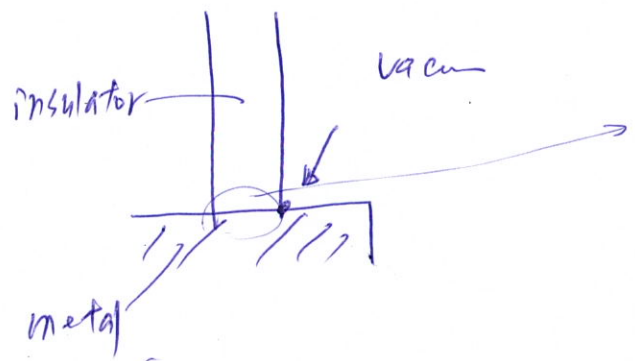
钴 钨



- ion implantation \rightarrow work hardening of the surface



3 Triple-Point Junction Modifications



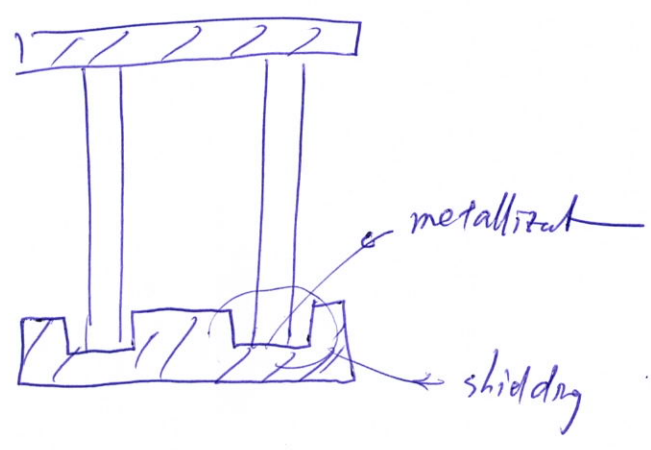
- It imperfect
- ⇒ a void or a gap results
- ⇒ E field enhancement
- ⇒ enhanced field emission

To improve:

- ① metalizing the insulator surface
- ② contact ⇒ a firm contact.

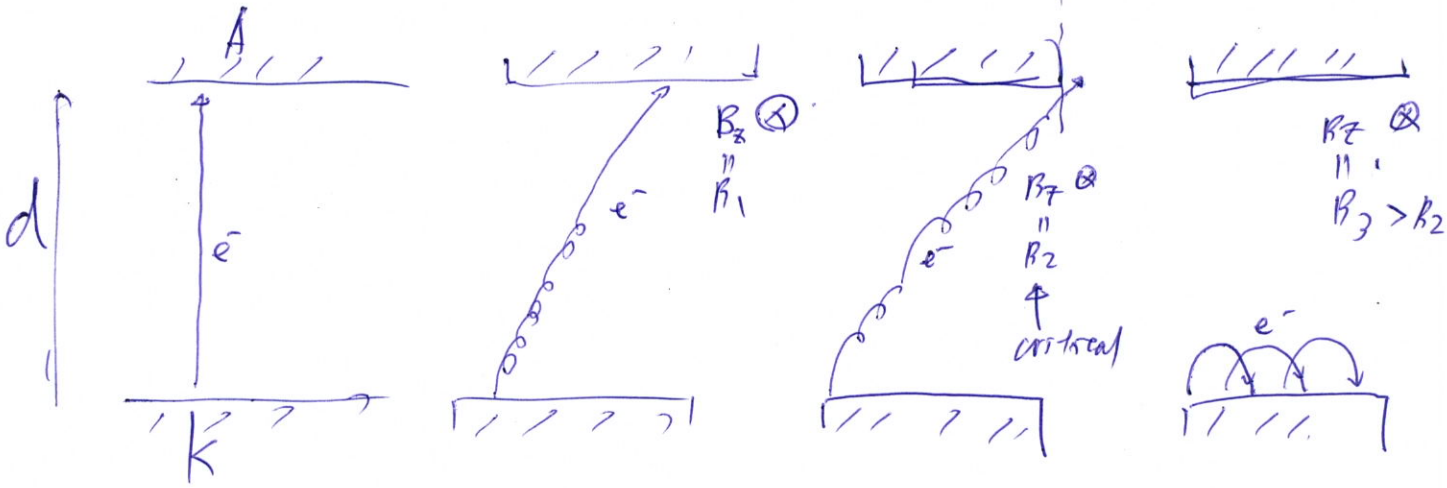
② elimination of the void and the shielding of the emitted area by $\frac{K}{L}$

Anode doesn't help



2. Vacuum magnetic insulation

my



- the crossed B field can be externally applied.

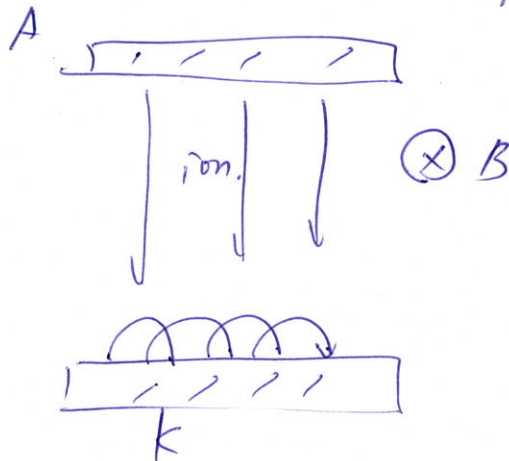
but also self-generated

⇒ magnetic insulation transmission line (MITL)

----- insulated line oscillator (MILLO)

high power
μ wave source.

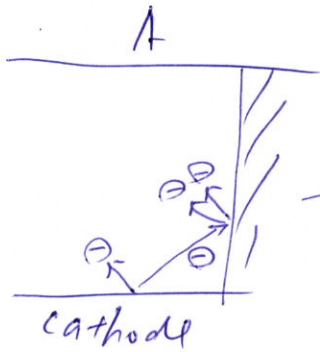
- Ion diode
 $m_i > m_e$



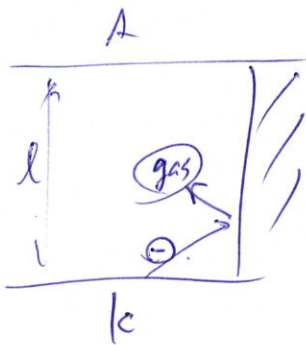
3 Surface flashover across solid in Vacuum 135

- $V_B \uparrow$ rapidly @ low p \therefore lack of ionizing collisions partners

\rightarrow surface flashover



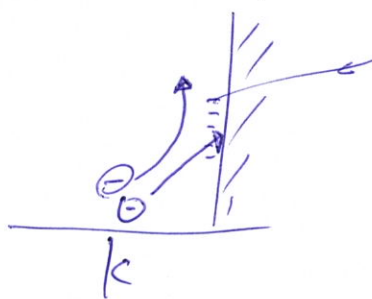
\rightarrow The dielectric surface is the source of electrons to feed the developing avalanche by a process known as 2nd e^- emission.



\rightarrow electron-stimulated desorption. e^- impacting the surface liberates gas trapped or adsorbed by the surface.

\rightarrow 2nd e^- emission from dielectric surface

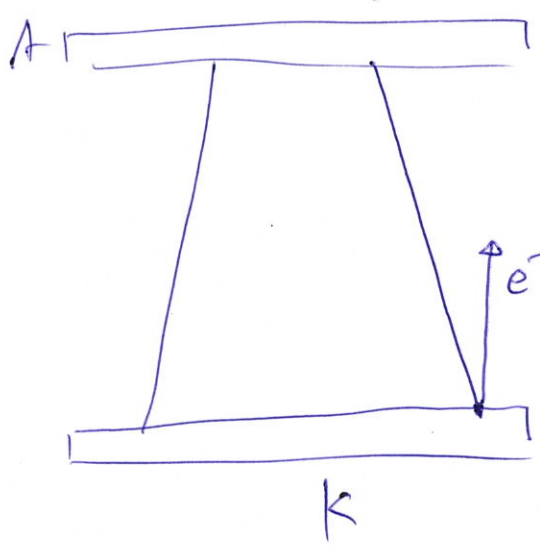
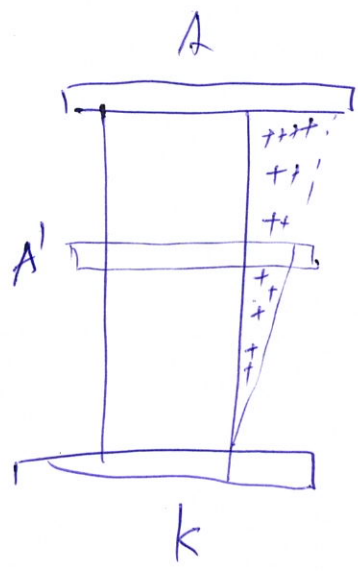
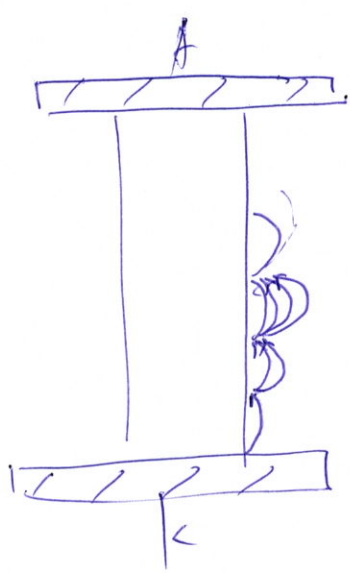
$E_{fc} > E_0 \rightarrow$ to liberate e^-



if $E_{fc} < E_0$, charge build up causing the following e^- away from the surface going more easy

$\Rightarrow E_{fc} \geq E_0 \rightarrow$ generate more e^-

$V_B \propto \sqrt{l}$



← to improve V_B'
or higher value of
 $E_0 \rightarrow$ less e^-
etc
generated